TWP EC Ca

AGENDA COMMITTEE OF THE WHOLE COMMUNITY DEVELOPMENT

Monday, October 7, 2024, 6:30 PM Corporation of The Township of Edwardsburgh Cardinal Council Chambers, Spencerville Ontario

- 1. Call to Order Chair, Chris Ward
- 2. Approval of Agenda
- 3. Disclosure of Pecuniary Interest or Conflict of Interest & the General Nature Thereof
- 4. Business Arising from Previous Committee Meeting Minutes (if any)
- 5. Delegations and Presentations
 - a. Affordable Housing Doug Poirier Total Equity Construction
 - b. Subdivision Agreement David Simpson Lockmaster's Meadow

6. Action/Information/Discussion Items

- a. Live: Land Use Planning
 - 1. Development Agreement, 27 David Street (Broniszeski)
 - 2. Subdivision Agreement, Lockmaster's Meadow (Edwardsburgh Developments Inc.)
- b. Work: Economic Development
- c. Play: Recreation
 - 1. Summer Day Camp Year End Report
 - 2. Aquatics Program Year End Report
- 7. Inquiries/Notices of Motion
- 8. Question Period
- 9. Closed Session
- 10. Adjournment



Affordable Housing

Page 1 of 465



Affordable Home Ownership in Ontario - Help is on the way

Introduction

Total Equity Construction was founded in 2021 by Doug Poirier. TEC is a designbuild general contracting company based in Greely Ontario with a mission to develop and build quality homes in the Ottawa region. TEC combines Doug's passion for construction and real estate development and investing. In 2023, TEC completed its first new build development, a 4800 square foot fourplex in Cornwall Ontario.

In Ontario, we are short on the goal of new housing starts that the government of Canada has set. At TEC, our key interest is in the development of new freehold homes and to build houses that our fellow Canadians can afford to purchase. We believe this can be achieved primarily through the collaboration of private developers and municipal government.

We are a boots on the ground developer



Small, lean business with minimal overhead WSIB insured with 2M liability coverage







The current state of affordable housing

Affordable housing initiatives are the central focus at this time as they should be. There is so much hope on the horizon. There are many positive policies and efforts being conducted to bring affordable rentals to the market. Many entities like non-profit housing providers, community housing bonds, co-operatives, charities and more are making big strides to deliver and preserve affordable housing units. On the affordable rental side there is great progress being made and on the affordable home ownership side there is also progress that should be highlighted. Ourboro is a company that co-invests in the purchase of houses to help Canadians get into the housing market by contributing to the down payment. This model of co-ownership is a very powerful way to support Canadians home ownership. CMHC has also rolled out a 30 year mortgage for first time homebuyers which is also very helpful.

We believe that there is a key piece missing in the conversation surrounding affordable housing that is the construction of new affordable freehold houses in Ontario. We believe affordable home ownership can be primarily achieved through the collaboration of private developers and municipal governments to build affordable houses.

TEC's Plan

We have a 2 bedroom starter house for \$260,000. This price is for the house only. TEC has designed a 2 bedroom bungalow that includes 1.5 bathrooms, full kitchen, dining room, living room and mechanical room. To keep the houses affordable, they will use a common well and septic system. The cost will be shared between the 4 homes and will be in addition to the price of the house. We do not have the price for this work at this point, a location would be required to be able to do the septic plan. This model is 600 square feet above grade and 600 square feet in the basement for a total of 1200 square feet of finished living space.

We also have a second model of a 2 bedroom house we can also build. We believe that the recipe for success with these houses are to build them on rural lots, where we can sell them and include a lifetime land lease of 99 years. This allows the purchaser to build equity and own their own property. In order to make these projects viable, the houses would share a septic system and a well. We have done preliminary research and have calculated that we could comfortably build 4 dwellings on a 1 acre lot. In the future we could look at having 9 dwellings on a single lot and could expand past that if it is a best use of the resources.

TEC's Plan (continued)

At this time we believe a pilot project of 4 houses on a 1 acre lot is optimal. The benefits of this approach are appealing to the home owner and the Township; affordable freehold house for the owners and multiple property tax sources for the Township. Our development would most likely need to be structured under condominium rules and collect condominium fees to maintain the septic, well, grass and snow. This would ensure that the overall maintenance of the grounds are uniform and addressed as per the schedule. Our vision to build these houses affordably will be achieved by adhering to the Ontario Building Code and using standard materials and standard design processes. The 2 bedroom bungalow model has a straightforward design meant to be cost effective and simple to build.

The contribution we are seeking from a township

To keep the homes affordable, we would need a low price on the land. The proposed land would need to be 1 acre in size with the minimum of electrical and internet services at the lot. The price of the land will be shared between the 4 homes and will be added to the price of the house.

We our doing our best to keep the price down by choosing smaller footprint for the homes and sharing a common well and septic. We are looking for a partner to work with us to keep the price as close to the \$260,000.00 as possible.

We would need a lot that is abutting a road that is maintained by the township, that has a hydro pole and internet nearby so that the costs to build will be kept to a minimum.





Drawn:	Notes:	Total Equity						
DP		Construction Inc.						



		2	21	5 '	-	10		>	2	11		5	18C			5755	63	1	57.0		1	6.72	5	22	195
								2724-1	- 66 	-		- 22	1 - 1 - 1		122 111		- 10	202 202	1000		1		8	39 	1083
S.,	÷.,	<u>.</u>	5.			5	1		5	2	12			5	3		8	3				3	8	2	1
				•		1	87 	0.85	25. 	88		10	12281	55	10	0.831	80 	1	122116	1		525	20 -	68	
	1900 - 1 552 - 1	1965 - 2293 -	46 - 3 13 - 1				28 75	27.447 - 6.521	184 195	100	1990) 1970)	- 20	280) 121	10	- 26	1989) 2003	- A.S. - 135-	98 98	oren Sect			2044 1925	90.	294 203	1981 1933
	18 - I	585	ð: -	1		2	8	1923	8	10	-23	1		5	18. 	5852. 	<u>8</u>	10	100	2		100	31	1	-51
	18 I 19 I	2754 1920 -	종 : 의 :			8	-12	1515	表示	57 742	6.83 0.25	18 19	620 120	5	示 (2)	NGAL Denis	89 20	18 12	9283 10253	8		1551	5	27 - 14	9.65 0.25
	3		ж. 36 - 1			8		Col	nti	~ ~	in	top		8	3	1000	33	3	25	8			35 25	28 12	
8		253) 1909	92 i 10 i			2	į,	Je	pu	1.0	yə	len		78	12 - 14	2525 0400	52 40	33. 14		2			2 	88 - 194	125
		2573 11251		1			12	122315 122315	/	1	120	2	1070 U 522 U		а 2	1233) 1223)	- 15	27 51	1070 1123	12		7227	22 22	22	1000 1140
		225	5	2	¥	4		-		5		-	20	5	÷.	222	5	2		ŝ		12	5	8	
	25 - 16 - 1	uala 1940	55 - W	ara Nam	833. 842	2	197 198	1977-12 1096-1	23) 24	965 714	1222	- 33 - 34	1373 1940 (* 1	22	10	NEN.	55 101	12 34	1574) 2000	23		5163	22. M	19 74	1995 1997
		221	¥.				24	1326	12	94		2	1921				Ŕ						2		
	Re	ar				1		1111	1	12		2 		1	-	257 A. 1994 B.	-	22 28		1			1	12	
	Ya	rd					ан. 38	1996) 1996)	36	100	163		200		18		100 100			8		2943	8	59 236	162
		4	2	1			3	1261		1	12	3	167		3			12				141		3	4
		1821	52 死日			8	200 208	1975-5 19962	307 1983	28		G	ree	n s	spa	ce		10 18		8		2.40	87 実		- 10 - 103
	γ.	1965	8	1			18	3645	10	76	181	(ii)	940	16	a"	1975	8	ж. ЭК	66	1		2663	w.	5	142
	8			1		į.	8		×.	8	56	ŝ.	(\hat{n})	ġ.	÷.	665				į.			8	8	56
8		182	Ř.	8.			28	3265	35	10		35	3817	8		1993	8	98	389			3361		8	. 83
100	-	100	100				3	3646	÷	54	12	8	646		92	1993	ŝ.		199			1643	1	5	148
5	5	-	5	5		3	ŝ.		2		6			Ę.	3				Ċ.				ġ.,	ŝ.	
0		001	85	8		82	34	1963	83	33	1.03	8	590	10	3	(00))	85	3		8		3965	36	38	103
62	22	-		-			12				n In .		n f			<u>.</u>	$\widetilde{\mathcal{V}}_{i}^{2}$	14	226		5	847	2	8	142
	8			8	2				4	danı	J HI J hu	dro	met	ur er i	with		ŝ.	8				6		ā.	ġ.
÷.	8	4	<u>-</u>	1	<i>K</i>		10	"di	sco	onne	ects	ma	unte	ed t	o sh	ned	$\left(i \right)$	10	(00)	90		206		0	1065
	8		ĕ.	1	1.	~	-		-	/		8	ξų.		1		Ĕ.	1	1	ž,				1	÷.
	r							988	2	12	150	2	no	ter	tia	L.w.		In	cat	ior	ġ	952	8	6	
67	8		16	8		×	30	1965	36	998	163		pu		rua		ULL	i.	Jul	1		5%0	8	3	163
		*					3		8	2	1	8		5	3			1	- /	/-			8	2	1
1963		1222		8		5	8	2253		22	155	2	898	55	15	69833 		/	/	1		259			195
	90 - 1 10 - 1		85 70	9 			94 22	3943	344 1.00	59 	183	1	140		<	-			890 2022	8		2243	W.	974 - 1971 -	100
8	Ű.		ð			8	3		8	2	9	8	20.				ġ.		0	8			3	ġ.	9
55	8	68.2	10	8		2	34	1189	35	0	.83	1	0.00	53	æ.,	192	80	8	889	87		6.89	8	58	.83
	0	~					3¥ 22	240 	100 100	54 22	192	ж ю	1991) - 224		ж е	2949) 2720-	16 10	18 20	293 2225			2000	ा स	54 22	2483 4 - 24
3			8	3		S.	3		2	9		3		2	1		£	5	19	2				9	
		1992.0					25 10	10.50	-32 	12.5 1915	- 55	- 22		27 	12 11	1000	- 22	83 	6444 4.447			1005	85 	3.8 	1.083
160 C	140 1	1.00	10.0	64 - E	1911	100	1.6	10.041	- 940	12.00	11042	- 942	10.00	100	1941	1921	1917	1.00	1.61	100	1.54	COLUMN 1	1967	1994	11.14.2

How we will build affordable houses

- Adhere to the Ontario Building Code minimum \checkmark
 - Utilize standard size construction materials
- Design a simple, efficient and repeatable structure
 - Use builder grade products 🗸
 - Implement durable and affordable products ie. (vinyl siding, asphalt shingles)
 - Maximize the number of dwellings per lot 🗸
 - Central parking lot \checkmark

Page 11 of 465



 \times Net Zero

 \times Passive House



Modular



Customizable finishes and features









Next steps

We are happy to work together with you to bring affordable housing in various forms to your township and are open to your suggestions. We believe this concept can bring density that will compliment the rural setting. Our goal is to start a long term relationship that we can create a winning situation for us as the developer and builder, you the Township and our fellow Canadian citizens. We believe that this can yield social impact and be profitable simultaneously.

If you see viability in this project as we do, we should consider a plot of land to conduct preliminary work on. Since each project is very situational, we would need to have a dedicated lot to test the soil as this would determine the feasibility of the undertaking. Let's discuss which contributions both parties are able to make to this endeavour.



Page 17 of 465

Affordable Home Ownership in Ontario

Help is on the way

Simple, repeatable process



Contact us





Doug Poirier Owner, TEC

totalequityconstruction.com

Office: 613-821-5548 Cell: 343-572-3664 doug@totalequityconstruction.com

LET'S MAKE AFFORDABLE HOME OWNERSHIP POSSBILE FOR OUR FELLOW CANADIANS



TOWNSHIP OF EDWARDSBURGH CARDINAL ACTION ITEM

Committee: Committee of the Whole - Community Development

Date: October 7, 2024

Department: Community Development

Topic: Development Agreement, 27 David Street. (Broniszeski)

Purpose: To review a draft development agreement prepared for the severed portion of severance B-38-23 at 27 David Street, to satisfy a condition of the severance decision.

Background: Application for severance B-38-23 received conditional approval from the consent granting authority on August 16, 2023. The application will create a new 0.094 ha lot with frontage on Charles Street. A hydrogeological study was submitted with the application to review water quality and quantity at the site in support of a reduced lot size in the R2 zone. An application for Minor Variance has also been submitted.

As a condition of severance approval, the applicant must enter into a development agreement with the Township to implement the recommendations of the hydrogeological study.

The hydrogeological study was prepared by Kollaard Associates in October 2022. The study determines that a well constructed on the new lot will provide sufficient water quantity for domestic use for a residential dwelling. In regards to water quality, the study finds that the water is hard by water treatment standards, the total dissolved solids may be present above the aesthetic objective in the future well; and iron and sulphides also measured high. The report provides recommendations for treatment of each concern.

The study also recommends that future well construction should conform with the recommended construction in the Thomson report from 2005 that was supported through the MOE report from 2020;

- well should be cased to a depth of at least 25 to 32 metres; AND
- the annulus of the well shall be sealed using suitable grouting and sealant for its entire length to the ground surface.

A draft development agreement is attached for Committee review.

Policy Implications: Sections 51(25) and section 53(12) of the Planning Act allow the approval authority to impose certain conditions of approval for severance decisions, including a condition that the owner enter into an agreement with the municipality. The agreement will be registered on title of the severed lot so that it is available to future owners.

Financial Considerations: The applicant has submitted the required fee to the Township for the development agreement, in accordance with the Planning Fees Bylaw 2022-40.

Recommendation: That Committee recommend that Council enter into a development agreement with the property owner, as attached, for the severed parcel of application B-38-23.

Community Development Coordinator

THE TOWNSHIP OF EDWARDSBUGH/CARDINAL DEVELOPMENT AGREEMENT

THIS AGREEMENT, made in triplicate, the ____ day of _____2024.

BETWEEN:

EDWARD BRONISZESKI AND LILA BRONISZESKI

(the "Owner")

-and-

THE CORPORATION OF THE TOWNSHIP OF EDWARDSBUGH/CARDINAL

(the "Township")

FOR LANDS DESCRIBED AS

The severed parcel of severance application B-38-23 of the United Counties of Leeds and Grenville

Part 2 of 15R12398; EDWARDSBURGH/CARDINAL

RECITALS:

1. The Owner is the owner of the lands described in Schedule "A" to this Agreement and proposes to subdivide it for the purpose of selling, conveying, or leasing it in lots.

2. The said lands are the subject matter of consent application B-38-23 which has received conditional approval from the United Counties of Leeds and Grenville Consent Granting Authority, a copy of which is annexed hereto as Schedule "B".

3. The Township, pursuant to Section 53 of the Planning Act, R.S.O. 1990, as amended, has the authority to enter into an agreement imposed as a condition of the approval of consent.

4. This agreement shall be registered at the cost of the Owner against the land to which it applies subject to the Registry Act and the Land Titles Act;

NOW THEREFORE THIS AGREEMENT WITNESSETH that in consideration of the other good and valuable consideration and the sum of One (\$1.00) Dollar of lawful money of Canada, now paid by each of the other parties hereto (the receipt whereof is hereby acknowledged) the Parties hereby covenant, promise and agree with each other as follows:

DEVELOPMENT AGREEMENT BETWEEN EDWARD AND LILA BRONISZESKI AND THE TOWNSHIP OF EDWARDSBUGH/CARDINAL

- 1. This Agreement affects the Lands described in Schedule "A" to this Agreement and shall ensure to the benefit of and be binding upon parties hereto, and their respective successors and assigns, The Owner hereby agrees to the registration of this Agreement against the title to the severed lands and retained lands, at the sole cost of the Owner.
- The Owner hereby agrees to obtain all required municipal approvals and comply with all applicable Zoning By-Laws of the Township, the Building Code Act, 1992, S.O. 1992, c.23 requirements and approvals required by applicable government authorities which may be required prior to the development of the lands.
- 3. The Owner hereby acknowledges that the lands described in Schedule "A" to this Agreement are the subject of the Hydrogeological Study, as shown in Schedule "C" to this Agreement, which was completed in order to assess the water quality and quantity for the site to allow a single family dwelling on the proposed severed lot that is to be serviced by a well and the existing municipal sewer.
- 4. The Owner hereby acknowledges and agrees that the professional recommendations and matters provided by Schedules "C" shall be provided and maintained by the Owner at the Owner's sole risk and expense.
- 5. In the event the Owner defaults in the performance of an obligation under this agreement or for reasons of public safety as determined by the Chief Building Official under the Building Code Act of Ontario or the Fire Marshall under the Fire Protection & Prevention Act of Ontario, the Township may, at the expense of the Owner, enter upon the lands and do all such matters and things as may be required to comply with any Order of the Chief Building Official or Assistant to the Fire Marshall (local Fire Chief). Such actual costs incurred by the Township plus an overhead charge of 15%, shall be deemed to be recoverable from the Owner by invoice and may be recovered in like manner as municipal taxes pursuant to the Municipal Act.
- 6. Any notice to be given hereunto shall be in writing to all other parties and either delivered personally or sent by prepaid registered mail, and in the latter case shall be deemed to have been given three (3) business days following the date upon which it was mailed. The address of the parties for the purpose hereof shall be:

to the Owner at:	to the Township at:
Edward and Lila Broniszeski	Township of Edwardsburgh/Cardinal
PO Box 5	PO Box 129
Spencerville ON K0E 1X0	Spencerville ON KOE 1XO

 The following schedules will form part of this agreement: SCHEDULE "A" – Description of the Property SCHEDULE "B" – Decision of the United Counties of Leeds and Grenville Consent Granting Authority SCHEDULE "C" –Hydrogeological Study Prepared by Kollaard Associates, October 28, 2022 SCHEDULE "D" – Site Survey 15R12398

IN WITNESS WHEREOF the parties hereto have executed this agreement.

OWNERS, EDWARD BRONISZESKI AND LILA BRONISZESKI

Owner

Owner

I/We are the registered owners of the property.

THE CORPORATION OF THE TOWNSHIP OF EDWARDSBURGH/CARDINAL

Mayor

Clerk

I/We have authority to bind the Corporation.

DATED AT Spencerville, ON this _____ day of _____, 2024

DEVELOPMENT AGREEMENT BETWEEN EDWARD AND LILA BRONISZESKI AND THE TOWNSHIP OF EDWARDSBUGH/CARDINAL

SCHEDULE "A"

DESCRIPTION OF THE PROPERTY

The severed parcel of severance application B-38-23 of the United Counties of Leeds and Grenville

Shown as Part 2 on Registered Survey 15R12398

DEVELOPMENT AGREEMENT BETWEEN EDWARD AND LILA BRONISZESKI AND THE TOWNSHIP OF EDWARDSBUGH/CARDINAL

SCHEDULE "B"

DECISION OF THE UNITED COUNTIES OF LEEDS AND GRENVILLE CONSENT GRANTING AUTHORITY



UNITED COUNTIES OF LEEDS AND GRENVILLE CONSENT GRANTING AUTHORITY

DECISION

APPLICATION B-38-23

We the undersigned members of the Consent Granting Authority of the United Counties of Leeds and Grenville; do hereby certify that the following is a decision reached by us at a hearing held at the Counties Offices, 25 Central Avenue, Brockville, Ontario on **August 16, 2023**. The said decision was reached on the application of **Edward & Lila Broniszeski** to sever a parcel of land being; Concession 6, Lot 5 of Registered Plan No. 40; **Township of Edwardsburgh Cardinal** having dimensions of approximately 32.52 metres by 29.69 metres with an area of 0.097 hectares.

DECISION: <u>GRANTED</u> providing the conditions as stated below are met.

REASONS:

Division of land is compatible with the intent and purpose of the Official Plan and meets the criteria in Section 51 (24) of the Planning Act providing conditions are met.

CONDITIONS:

- (1) That all conditions imposed in the granting of this decision be met and one (1) original paper copy and one (1) digital copy of the deposited reference plan of the subject lands, which conforms substantially with the application as submitted, and the instrument relating to the transaction (deed/transfer, Service Ontario parcel register, grant of right-of-way, etc.) be presented to the Secretary-Treasurer of the Consent Granting Authority for the Certificate of Consent no later than **August 17, 2025.**
- (2) That a copy of the deposited survey be submitted to the Township.
- (3) That the applicant obtain relief from the zoning bylaw, as necessary to address the deficient lot size for the severed and retained parcels.
- (4) That a development agreement is registered on title of the severed parcel to implement the recommendations of the hydrogeological study (Kollard Associates, October 28, 2022) to the satisfaction of the Township.
- (5) That written release of conditions 2, 3 and 4 from the Township be submitted to the Consent Granting Authority prior to endorsement of consent on the deed for the severed land.

NOTES:

- (1) The Township had no objection providing conditions 2, 3 and 4 are complied with.
- (2) South Nation Conservation had no objection.
 - SNC's review did not identify any natural hazards on the severed or retained lots.

I hereby certify this to be a true and exact copy

Cherie Mills

KWeideraar

Secretary-Treasurer

Chair

This Decision was mailed on <u>August 17, 2023</u>

The last date for appealing this decision is September 6, 2023

DEVELOPMENT AGREEMENT BETWEEN EDWARD AND LILA BRONISZESKI AND THE TOWNSHIP OF EDWARDSBUGH/CARDINAL

SCHEDULE "C"

HYDROGEOLOGICAL STUDY PREPARED BY KOLLAARD ASSOCIATES OCTOBER 28, 2022



210 Prescott Street, Unit 1 P.O. Box 189 Kemptville, Ontario K0G 1J0 Civil • Geotechnical • Structural • Environmental • Hydrogeology •

(613) 860-0923

FAX: (613) 258-0475

REPORT ON

HYDROGEOLOGICAL STUDY PROPOSED RESIDENTIAL LOT SEVERANCE 27 DAVID STREET SPENCERVILLE, ONTARIO

Submitted to:

Ed Broniszeski 27 David Street Spencerville, Ontario K0E 1X0

DATE October 28, 2022

DISTRIBUTION

1 digital copy Ed Broniszeski 1 digital copy Kollaard Associates Inc.

220996

Professional Engineers Ontario

Authorized by the Association of Professional Engineers of Ontario to offer professional engineering services. Kollaard Associates Engineers 210 Prescott Street, Unit 1 P.O. Box 189 Kemptville, Ontario K0G 1J0 Civil • Geotechnical • Structural • Environmental • Hydrogeology •

(613) 860-0923

FAX: (613) 258-0475

October 28, 2022

220996

Ed Broniszeski 27 David Street Spencerville, ON K0E 1X0

RE: HYDROGEOLOGICAL STUDY PROPOSED RESIDENTIAL LOT SEVERANCE 27 DAVID STREET SPENCERVILLE, ONTARIO

Kollaard Associates Inc. was retained by Mr. Ed Broniszeski to undertake a hydrogeological and terrain study for a proposed residential lot severance with frontage on Charles Street in Spencerville, Ontario (Key Plan, Figure 1).

It is understood that it is being proposed to sever one residential lot of 0.09 acres, which is currently vacant. The retained parcel consists of about 0.09 hectares and is occupied by a single residence. It is identified as 27 David Street. A Lot Development Plan is provided as Figure 2.

The purpose of the severance is to allow single family dwelling on the proposed severed lot that is to be serviced by a well and the existing municipal sewer. It is understood that all residential dwellings within 500 metres are serviced by sanitary sewer, with the exception of the rural properties that are located on the opposite side of the South Nation River.

This report consists of an evaluation of the water quality and quantity for the existing well on the property.

The assessment was carried out on an existing drilled well to ensure that the water quality and quantity is acceptable using the following guidelines; Ministry of the Environment, Conservation and Parks (MECP) Guideline D-5-5 and the Ontario Drinking Water Standards, Objectives and Guidelines (ODWSOG).

HYDROGEOLOGICAL STUDY

Background

A bedrock geology map for the site area indicates the bedrock at the site consists of dolostone and sandstone of the Beekmantown Group.

The surficial geology map indicates that the proposed severed lot is located within an area of glacial till. Most of the well records for the area wells indicate that there is between 0 and 2 metres of overburden, consisting of glacial till or sand and clay.

Professional Engineers Ontario

Authorized by the Association of Professional Engineers of Ontario to offer professional engineering services. A review of topographical information from the Province of Ontario online mapping indicates that the site topography is sloped towards the south of the proposed severed lot.

No well record was available for the existing drilled well at 27 David Street. The well depth was measured to be about 59.8 metres, and the casing was indicated by the owner to extend to about 30.5 metres deep. The static water level measured at the day of the test was about 7.43 metres.

The well record and Certificate of Well Compliance for the test well and area well records are provided herein as Attachment A.

Area Well Records

It is understood from information provided by the owner that the well that services the existing dwelling was installed when the municipal sanitary system was put into place. The well was constructed with recommendations from a private well and sewage system study completed by MS Thomson and Associates in 1984. A review of three other well records also installed at this time was carried out. The well records are provided (Attachment A). The depths of the wells are indicated to be between 61 and 70 metres, obtaining water from a dolomite aquifer. Test pumping rates were between 19 and 45 litres per minute. Recommended pumping rates were between 15 and 38 litres per minute. Overburden thickness was between 1.8 and 2.1 metres of sand or clay. The wells had 31.1 metres of casing. Specific capacity was between 0.3 and 0.8 litres per minute per metre of drawdown.

A review of eleven area well records constructed not due to the installation of the municipal sanitary system was also carried out. The well records are provided (Attachment A). The depths of the wells are indicated to be between 12 and 55 metres, obtaining water from a limestone aquifer. Test pumping rates for the area wells were 24 to 76 litres per minute. Recommended pumping rates were between 11 and 46 litres per minute. One well record indicated no overburden. In the other ten well records, overburden was identified as between 0.6 to 2.0 metres of till, topsoil, sand or clay. All area wells had between 4.0 to 9.5 metres of casing below the ground surface. Specific capacity for area wells is between 5 and 1050 litres per minute per metre of drawdown.

The test well is considered to be representative of the expected well yields based on other area wells, specifically those installed due to the municipal sanitary system.

Review of MECP Report

A review of the MECP Potable Well Water Quality Survey for the Village of Spencerville, dated November 6, 2020, was carried out as a part of this report. The MECP report details an investigation completed in 2020 regarding water quality and bacteria contamination in Spencerville, and focuses on a subject property at 32 David Street.

This report contains recommendations on well construction in Spencerville, based on a previous report from 1985, due to poor water quality (from shallow contamination sources) particularly with regards to bacteria and sewage impacts from the private sewage systems. The recommended well construction was that wells should be cased to depths exceeding 25 to 32 metres. The 2020 sampling by the MOE indicated that fewer of the deeper cased wells (2 of 9 wells) had adverse bacteria results compared to some 6 of 9 wells with short casing lengths where some 67% had adverse bacteria results. The MOE indicated the following based on their 2020 well water sampling results:



Well owners with wells not conforming to the recommendations provided by Thompson (1985) and with chronic adverse water quality issues could also consider obtaining the services of a licensed well contractor to replace their existing well with one that is cased into the deeper less vulnerable aquifer. It should be noted that this recommendation is not a guarantee that potable water will be obtained; however, it would be expected to reduce the vulnerability (magnitude and frequency of adverse water quality) of the water supply and those recommendations provide above should still be followed. It should also be noted that the deeper bedrock units may produce water with elevated concentrations of iron and/or sulphur and additional treatment may be required to address them.

-3-

The well that was sampled does comply with the recommendations of the Thompson report. As such, it is highly recommended that the future well servicing the severed lot should also be constructed similarly.

Water Quantity

A pumping test was carried out on October 14, 2022, on the existing drilled well at the retained lot on the subject property (27 David Street).

The testing consisted of a 6 hour duration pumping test. During the pumping test, water level measurements were made on a regular basis to monitor the drawdown of the water level in the well in response to pumping and water levels were monitored at one minute intervals using a pressure transducer. Hourly field water quality readings were recorded for the water temperature, pH, total dissolved solids (conductivity) and turbidity. After the pump was shut off, the recovery of the water level in the well was measured until about 95% recovery of static water level had been achieved or for 24 hours.

The well was pumped for about 360 minutes at a pumping rate of about 30 litres per minute. Over the course of the pumping test, the water level in the well dropped 0.31 metres in response to that rate. At the end of pumping, 100 percent recovery of the total drawdown in the static water level created during pumping was measured after about 13 minutes.

The pumping test drawdown and recovery data and plots for TW1 are provided as Attachment B. The drawdown and recovery data provided were measured with reference to the top of the well casing at the test well location.

The pumping test data for the test well was analyzed using the method of Cooper and Jacob (1946). Although the assumptions on which these equations are based are not strictly met, this method provides a reasonable estimate of the aquifer transmissivity.

Transmissivity was calculated using the following relationship:

$$T = \frac{2.3Q}{4\pi ds}$$

where

Q is the pump rate, m^3/day ds is the change in drawdown over one time log cycle, m T is the transmissivity, m^2/day

Based on the pumping test drawdown data, the transmissivity of the aquifer is estimated to be about 395 m^2 /day. Based on the recovery data from the pumping test, the transmissivity is

Civil · Geotechnical · Structural · Environmental · Hydrogeology



estimated to be about 132 m²/day. The aquifer parameters, such as transmissivity, can be determined more accurately by using a higher flow rate and a longer duration to establish hydraulic boundaries for the aquifer. The pumping rate and duration that were used were sufficient to confirm that the well yield is sufficient for the proposed use.

Based on the data obtained during the six hour pumping test, it can be concluded that the well is capable of sustaining a short term yield of at least 30 litres per minute. During the course of the pumping period, less than 1 percent of the available drawdown in the test well was utilized, based on an estimated pump depth of 56 metres and the static water level recorded the day of the pumping test (7.43 metres). The specific capacity of the well based on the pumping rate used is 81 litres per minute per metre of drawdown.

The typical residential peak demand rate is 22.5 litres per minute for a five bedroom dwelling. It is considered that the pumping rate used was sufficient to meet peak residential demands.

Based on the above noted assessment of the test well and what is known about the aquifer from adjacent wells, it is considered that future wells constructed in the same aquifer (to similar depths) on the proposed severed lots will provide sufficient water for domestic use for a residential dwelling.

Water Quality

During the pumping test, hourly field readings of pH, temperature, turbidity and total dissolved solids (conductivity) were recorded.

The results of the chemical, physical and bacteriological analyses of the water samples obtained from the test well are provided in Attachment C. A summary of the water quality measured in the field are provided as Table I, Water Quality Measurements for Test Well.

Groundwater samples were prepared and preserved in the field using appropriate techniques. Chlorine residuals were measured prior to obtaining water samples for lab submission and free chlorine was measured to be zero. The water samples were submitted to Eurofins Environmental Laboratory in Ottawa, Ontario, for the chemical, physical and bacteriological analyses listed in the MECP guideline entitled Procedure D-5-5, Technical Guideline for Private Wells: Water Supply Assessment, August 1996.

The water quality as determined from the results of the analyses is acceptable. The water meets all the Ontario Drinking Water Standards, Objectives and Guidelines (ODWSOG) health and aesthetic parameters tested for at the test well except for hardness, hydrogen sulphide, turbidity, iron and TDS. Sodium is above the medical advisory level of 20 milligrams per litre for those who require a sodium reduced diet. The sodium level is about 57 milligrams per litre. When sodium levels exceed 20 mg/l, the local Medical Officer of Health should be informed so that the information can be relayed to local physicians.

Hardness

The water is considered to be moderately hard by water treatment standards. Water with hardness above 80 to 100 milligrams per litre as $CaCO_3$ is often softened for domestic use. The hardness at the well is 417 to 420 milligrams per litre, which is considered poor but tolerable. Treatment using ion exchange water softeners is effective to reduce hardness.

Water softening by conventional sodium ion exchange may introduce relatively high concentrations of sodium into the drinking water, which may contribute a significant percentage to the daily sodium



intake for a consumer on a sodium restricted diet. Where ion exchange water softeners are used, a separate unsoftened water supply could be used for drinking and culinary purposes.

-5-

Iron

Iron was measured at a level of 2.20 to 2.28 mg/l, compared to the aesthetic objective of 0.3 mg/l. Excessive iron levels may cause brown or black discolouration of laundry and fixtures, affect the taste and colour of water, and iron precipitation in pipes and hot water tank can also promote the growth of iron bacteria. For iron levels of up to 5.0 mg/L, a manganese greensand iron filters (or other proprietary iron filter) is effective in removing iron from the water supply.

Turbidity

Turbidity at the well was initially recorded at less than 5 NTU (during the first two hours of the pumping test), which is acceptable for groundwater at the point of consumption. However, turbidity became elevated and even increased between about three six hours (8.0 and 20.6 NTU). The elevated turbidity measured in the field during the test was likely due to the iron deposits in the well casing and the agitation of the well surfaces created during the pumping test. Given the depth of well casing, there is significant well surface and the iron in the water and in the casing could contribute to the turbidity.

The lab based turbidity measurements for the three and six hour samples were 14.6 and 24.8 NTU, respectively. This is consistent with the field readings and also higher due to the presence of iron which can cause turbidity to exceed due to precipitation that occurs as the water sample changes temperatures and is exposed to air during storage and transportation prior to the laboratory sampling.

Water treated through an iron filter is expected to meet the required turbidity levels of less than 5 NTU in the treated water. It is considered that the untreated water has a turbidity level of less than 5 NTU (based on the first two hours of water tested using field equipment) and that treatment to reduce iron will also cause the turbidity to be less than 5 NTU in the treated water.

Sulphide

Sulphide was measured at levels of 0.09 and 0.12 mg/L as hydrogen sulphide, compared to the aesthetic objective of 0.05 mg/L. Excessive sulphide levels may produce black deposits on pipes and fixtures and black stains on laundered items. The sulphide can be removed using the same manganese filter that is needed for iron reduction. Proprietary filters for iron and sulphide removal as well as manganese greensand filters are effective at reducing sulphide levels of up to 1.0 and 2.5 mg/L.

Total Dissolved Solids

Total dissolved solids (TDS) were elevated above the aesthetic objective of 500 mg/l, about 607 to 610 mg/l. The Ryznar Stability Index (RSI) and Langelier Saturation Index (LSI) were calculated for both water samples. The RSI values for the water samples were 6.81 and 6.67 for the three and six hour samples, respectively. The LSI values for the water samples were 0.32 and 0.44 for the three and six hour samples, respectively. RSI values less than 6 indicate that the scale potential increases and values greater than 7 indicate that a calcium carbonate formation does not lead to a protective corrosion inhibiting film. In this case, the water is mildly scale forming and not corrosive. Positive values close to zero indicate borderline scale potential. In this case, the LSI values are positive, indicating borderline scale potential. Combined with the RSI values, it is likely that the water is slightly scale forming and is not corrosive. According to the Support Document for the Ontario Drinking Water Standards, Objectives and Guidelines (ODWSOG), the palatability of drinking water with a TDS level less than 500 mg/l is generally considered to be good. The effect of

Civil • Geotechnical • Structural • Environmental • Hydrogeology



elevated TDS levels on drinking water depends on the individual components, which are principally chlorides, sulphates, calcium, magnesium and bicarbonates. Depending on which parameters are elevated, TDS exceedances can include hardness, taste, mineral deposition or corrosion. In this case, the water samples had high hardness. Sodium and chloride are both well within the aesthetic objectives and are unlikely to significantly affect the taste of the water. Hardness generally increases the mineral deposition. However, in this case, the water is not indicated to be scale forming. Based on the above noted information, it is considered that treatment to reduce hardness will reduce the potential for scale forming as it affects TDS.

-6-

Total Coliforms

The water samples obtained after 3 and 6 hours of pumping on October 14, 2022 both had total coliforms of 4 counts/ 100 mL with E. Coli and faecal coliforms absent.

MECP Procedure D-5-5 states the following with regards to total coliforms:

While the stated ODWS for Total Coliforms is 0 counts per 100 ml of sample, it is recognized that the objective had been set as an indicator of inadequate disinfection within the distribution systems associated with water works. For private water wells not subject to approval under the OWRA, the MOEE and Health Units have historically used the limit of <5 counts per 100 ml in the absence of a chlorine residual as indicating acceptable water quality.

As the total coliforms were within the wells allowed for existing wells and E. Coli was absent, the presence of total coliforms is considered acceptable. The owner was informed and recommendations were provided to test at least quarterly for bacteria through the public health unit.

RECOMMENDATIONS

The following is recommended for the construction of the future well to service the proposed severed lot with frontage on Charles Street:

- The well construction should conform with the recommended construction in the Thomson report from 2005 that was supported through the MOE report from 2020, as follows:
 - well should be cased to a depth of at least 25 to 32 metres; AND
 - the annulus of the well shall be sealed using suitable grouting and sealant for its entire length to the ground surface.

The following should be considered for expected water quality and well construction for the future well on the severed lot.

The water is considered to be hard by water treatment standards. Water with hardness above 80 to 100 milligrams per litre as CaC0₃ is often softened for domestic use. The hardness at the well is ~420 milligrams per litre. Treatment using ion exchange water softeners is effective to reduce hardness. Water softening by conventional sodium ion exchange may introduce relatively high concentrations of sodium into the drinking water, which may contribute a significant percentage to the daily sodium intake for a consumer on a sodium restricted diet. Where ion exchange water softeners are used, a separate unsoftened water supply could be used for drinking and culinary purposes. Sodium level in the untreated water is 57 mg/L, which is above the 20 mg/l medical advisory limit and well within the aesthetic objective of 200 mg/L. When sodium levels exceed 20 mg/l, the local Medical Officer of Health should be informed so that the information can be relayed to local physicians.

Civil • Geotechnical • Structural • Environmental • Hydrogeology


 Total dissolved solids (TDS) may be present above the aesthetic objective of 500 mg/l in the future well. It is likely that the water is slightly scale forming. According to the Support Document for the Ontario Drinking Water Standards, Objectives and Guidelines (ODWSOG), the palatability of drinking water with a TDS level less than 500 mg/l is generally considered to be good. There is no treatment recommendation for TDS. Treatment to reduce hardness will reduce scale potential associated with elevated TDS.

-7-

Iron was measured at between 2.2 and 2.28 mg/L, compared to the aesthetic objective of 0.3 mg/L. Sulphide was measured at a level of 0.09 to 0.12 mg/L, compared to the aesthetic objective of 0.05 mg/L. Excess iron and sulphide levels may produce coloured deposits on pipes and fixtures and stains on laundered items. It also produces an unpleasant taste and odour. Both iron and sulphide may be reduced using manganese greensand filters or other proprietary filter at iron levels up to 5.0 mg/L and sulphide levels of up to 1.0 to 2.5 mg/L.

We trust this letter provides sufficient information for your purposes. If you have any questions concerning this letter, please do not hesitate to contact our office.

Regards,

Kollaard Associates Inc.



Colleen Vermeersch, P. Eng.

Attachments:	Table I Figure 1 Figure 2 Attachment A	Summary of Hourly Field Water Quality Key Plan Site Plan Sketch Well Records TW1 Pumping Test Data
	Attachment B Attachment C	TW1-Pumping Test Data TW1-Laboratory Water Testing Results

TABLE I

FIELD WATER QUALITY MEASUREMENTS FOR TEST WELL 1

Time Since Pumping	Temperature	pН	Turbidity	Total Dissolved	Conductivity	Free
Test Started	(°C)		(NTU)	Solids	(μS)	Chlorine
(min)				(ppm)		(ppm)
60	10.4	6.84	4.81	515	1034	0.00
120	10.8	7.18	4.61	498	996	-
180	11.3	7.35	8.05	488	966	-
240	11.8	7.43	15.0	476	950	-
300	11.4	7.60	13.2	481	960	-
360	12.1	7.58	20.6	490	978	-





Page 39 of 465



ATTACHMENT A

MECP AREA WELL RECORDS

UTM $ $	ources	Commission	Act ORD	water resou division 24 N JAN 191 ontario wa resources com	IRCES 0 0 1 0 6 965 NTER MISSION
Basin 215 drehville	Fownsł	1ip, Village, T	own or City	Edwardsbu	argh
Con. 6 Lot Part 27 I	Date co Ires:	mpleted s Sp enc	l ((day erville,	OCT ^{month} Ontario.	64 year)
Casing and Screen Record			Pumping	Test	
Inside diameter of casing 6 3/16"	Sta	tic level	20 feet	*********	
Total length of casing 13 feet	Tes	st-pumping ra	ite 3호		G.P.M.
Type of screen None	Pur	mping level	35 feet	er stillen for kan anderskaler off	
Length of screen	Du	ration of test p	oumping	l hour	
Depth to top of screen	Wa	ter clear or clo	oudy at end of	test cle s	ar
Diameter of finished hole 6"	Re	commended p	oumping rate	3	G.P.M.
	wit	h pump settin	ւց of	feet belo	w ground surface
Well Log			r	Water	r Record
Overburden and Bedrock Record		From ft.	To ft.	Depth(s) at which water(s) found	Kind of water (fresh, salty, sulphur)
Grey limestone		0	40	38	fresh
For what purpose(s) is the water to be used? House Is well on upland, in valley, or on hillside? Hillside Drilling or Boring Firm J.B. Dufresne & Co. Ltd., 1014 Maitland Ave., Address OTTAWA 5, Ont. Licence Number 1307 Name of Driller or Borer R. Leniel Address Ironside, Cuebec. Date 5 October, 1964 (Signature of Licensed Dritting for Jording Contractor) Form 7 10M-62-1152		In diagram road and	Location m below show lot line. Ind 300 300 House Brice gra	of Well distances of we icate north by TV RD TV RD Color to R to R to R to R to R to R to R to R	ll from arroy 26 21 9 4 4
OWRC COPY Page 4	1 of 4	165	•		

$\frac{ q _{R}}{ q _{R}} = \frac{ q _{R}}{ q _{R}}$ Elev. $ q _{R} = \frac{ q _{R}}{ q _{R}}$	E N The Wat	ONTA	RIO Illers Act. 1954	GROUND 24 _{SE} ONTAI RESOURCE	NATER BRANCH JO T 8 1958 RIO WATER S COMMISSION
$\begin{array}{c} \text{Basim} \left[\begin{array}{c} A \\ \end{array} \right] \\ = \\ \begin{array}{c} 0 \\ \end{array} \end{array} \right] \\ \begin{array}{c} 2 \\ \end{array} \right] \\ = \\ \begin{array}{c} 0 \\ \end{array} \\ \end{array} $	D	epartment	of Mines	_	
V	Vater	We	ll Record	E	
	11	1950	hip, Village, Town or C n Village, Town or Cit Address	ity.la.du.za.ala ty) succurrent	lsusgtuj: '
Date completed	(month)	(year)			
Pipe and Casing	Record]	Pumping Test	
Casing diameter(s)	Casing diameter (s)				
Well Log			,	Water Record	
Overburden and Bedrock Record	From ft.	To ft_	Depth (s) at which water (s) found	No. of feet water rises	Kind of water (fresh, salty, or sulphur)
hadpan	0	4	65	47	frech
For what purpose(s) is the water of MULL Is water clear or cloudy?	to be used?	and	Loc In diagram below road and lot line. // OR // // // J350 70 m	ation of Well show distances of Indicate north	f well from by arrow. SPENOEAVILLE
Form 5	-	.	<i></i>	C	55.58

Min of th	istry ne	×	Th	e Ontario Water Resour	ces Act
Ontario Env	ironment 2	406531	AIER 7 2404	967,48. 12,40,02	
COUNTY OR DISTRICT		TOWNSHIP. BOROUGH CITY. TOWN V	LLAGE	CON BLOCK IRACT SURVE	1 G & 35.11
TITCEN .		1- di vards b	urg	cont.	DATE COMPLETED
		E,	·/e #	2-18	DAY_11_ MO_9 YR 91
1 2 20 20	8-6111		Lele Levation	IN INPLICAT	
	L	G OF OVERBURDEN AND	EDROCK MATE	RIALS (SEE INSTRUCTIONS)	
GENERAL COLOUR	MOST COMMON MATERIAL	OTHER MATERIALS		GENERAL DESCRIPTION	DEPTH - FEET
Brown	Class	Sand Gray	rel	5/+	0 6
Black	Dolomite	Fracturer	ł	Hard	6 151
Greu	Sandatore	Dolomite		Hard	151 303
9				1	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
5	5.	24 - 1 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	2	2	
31 32 41 WATER FOUND ATTER	H 13 21 ER RECORD 21 KIND OF WATER 78554 30 000 PUUN FRESH 30 000 PUUN 14 SALTY 40 PUNEPALS 60 CAS FRESH 30 000 PUUN 14 SALTY 40 PUNEPALS 78757 FRESH 30 000 PUUN 14 SALTY 40 PUNEPALS 60 CAS FRESH 30 000 PUNE 24 SALTY 40 MINEPALS 60 CAS FRESH 30 000 PUNE 24 SALTY 60 CAS 50 PUNEPUR FRESH 31 000 PUNE 24 SALTY 60 CAS 50 PUNEPUR FRESH 31 000 PUNE 24 SALTY 60 CAS 50 PUNEPUR FRESH 31 000 PUNE 24 SALTY 60 CAS 50 PUNEPUR FRESH 31 000 PUNE 24 SALTY 60 CAS 50 PUNEPUR AND FRESH 31 00 PUNEPUR 34 PUNEPUR SALTY 60 CAS 50 PUNEPUREPUE FRESH 31 00 PUNEPUE 34 PUNEPUE SALTY 60 CAS 50 PUNEPUE	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	OLE RECORD CECTIM FEET CALCENT FEET CALCE		ATTERIAL AND TYPE CORD
TEST DI CARACTERIA COMPACTICA COM	WATER LEVEL END DTV PINPTNG 28-24 15 MIAUTES 28-24 15 MIAUTES 1900 7607 7	VELS DURING I BY PUMPING 30 MINUTES 45 MINUTES 66 MIN 190 FEET 190 FEET 190 11 AT WATER AT END OF TEST 190 FEET 1 CLEAR 2 BE CLU 43-45 PECOMENDED 190 FEET RATE 7		DIAGHAM BELOW SHOW DISTANCES T LINE INDICATE NORTH BY AR	ROW.
FINAL STATUS OF WELL WATER USE	1 DQ (WATER SUPPLY 2 OBSERVATION WELL 3 TEX HOLE 4 RECHARGE WELL 56 1 5 TERICATION 4 DISTRICATION 5 TERICATION 4 DISTRICATION 4 TERICATION 5 TERICATION 4 INDUSTRIAL 0 OTHER	ABANDONED INSUFFICIENT SU ABANDONED POOR QUALITY UNFINISHED DEWATERING COMMERCIAL MUNICIPAL PUBLIC SUPPLY COOLING OR AIR CONDITIONING	PPLY OF TO		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
METHOD OF CONSTRUCTIO	1 CABLE TOOL 2 ROTARY ICONVENTION 3 ROTARY INTERPRESS 4 ROTARY INTERPRESS 5 ØZ AIR PERCUSSION	BORING BORING J DIANOND DISTING DRIVING DIGGING OTHER	DRIVERE	Uillage of Spenceru	ille 101572
NAME OF WELL CO	MURACTOR L Well Dr 1083 Ple:	well contractions of the second second well rechnicity of the second sec	AN'S	SPECTION	NTE ACCENTE 1 1 1991 *****
BIGNATURE OF T	OF THE ENVIRON	SUBHISSION DATE	OFFIC		CSS.ES

R		istry			Th	e Ontario Wa	ater Resources	Act	
0	ntario	ironment 2	406532	WA				ECC	
	TOUNTY OR DISTRICT	2. CHECK 🛛 CORF	TOWNSHIP BOROUGH	CITY. TOWN. VILLAGE	<u>a</u>			Part Part	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
		- 10 12	17 16		C. ELEVATION	RC BA			₩ ₩
		MOST	G OF OVERBURD	EN AND BEDR	OCK MATE	RIALS ISEE INST	RUCTIONS	DEPT	
E	2	COMMON MATERIAL		MATERIALS		GENERAL D	DESCRIPTION	FROM	
4	Brain	Shall	Wood F	ragment		Hacke	<u>ol</u>	 	S r
Ē	Black	Dolomite	FIRCYL			Hard		6.5	231
	31	TRESH 3 DULPHUR TRESH 3 DULPHUR TRESH 3 DULPHUR SALTY 4 MINERALS TRESH 3 DULPHUR SALTY 4 MINERALS TRESH 3 DULPHUR SALTY 4 MINERALS TRESH 3 DULPHUR SALTY 4 GOAS TRESH 3 DULPHUR SALTY 4 GOAS TRESH 3 DULPHUR SALTY 4 GOAS TRESH 3 DULPHUR SALTY 4 MINERALS TRESH 3 DULPHUR SALTY 4 MINERALS SALTY 4		1 1 1 1 1 1 1 1 1 1 1 1 1 2 OPEN HOLE 1 1 CATASS 1 1 CATASS 1 2 (1 2 (1 3 - 188 (2 4 (2	J L L J L L J L L J L L J L L D D D D I D D I D D J D D J D D J D D J D	E STAC SP OF STAC	L L <th>DIAMTER 34-34 DIAMTER 34-34 DIAMTER 34-34 DEFINITO FOR DIFFERENT DEFINITO DIFFERENT DEFINITO DIFFERENT DEFINITO DIFFERENT DEFINITO DEFINIT</th> <th></th>	DIAMTER 34-34 DIAMTER 34-34 DIAMTER 34-34 DEFINITO FOR DIFFERENT DEFINITO DIFFERENT DEFINITO DIFFERENT DEFINITO DIFFERENT DEFINITO DEFINIT	
PUMPING TEST	STATIC LEVEL 15-21 15-21 15-21 1-21 10-210	E BAILER WATER LEVEL 25 END OF BATER LE DUPING WATER LE DUPING State DUPING State DUPING State DUPING State BI-41 IS MINUTES BI-41 PUNP INTAKE S OFM C PTYPE RECOMMENDED PLDEEP SETTING	VELS DURING 30 MINUTES 30 MINUTES 43 M	13-56 O 17-56 Mouns O 17-56 PUMPING ← RECOVERY	Source	DIAGRAM BELOW S T LINE INDICAT INDICAT	How DISTANCES OF V	VELL FROM READ /	an d
	FINAL STATUS OF WELL	A I D WATER SUPPLY 2 OBSERVATION WELL 3 TEST HOLE 4 RECHARGE WELL	ABAN DONED IN ABAN DONED IN ABAN DONED PO UNFINISHED DEWATERING	SUFFICIENT SUPPLY FOR QUALITY	$ _{n_{j}}$		Villag	e te	5
	ss WATER USE	54 I Image: Content of Contento	COMMERCIAL MUNICIPAL PUBLIC SUPPLY COOLING OR AIR CO +	NDITIONING Not used			Spencer	o:lle	
co	METHOD OF ONSTRUCTIO	CABLE TOOL CABLE TOOL CABLE TOOL CABLE TOOL CABLE TOOL CABLE TOOL CONTANY (COVENT) CABLE TOOL CABLE TOOL CONTANY (COVENT) CABLE TOOL CONTANY (COVENT) CABLE TOOL CONTANY (COVENT) CONTANY CONTANY (COVENT) CONTANY	6 BORING ONALI 7 DIAMON 8 JETTING 9 DRIVING 0 DRIVING	ар 5 5 G Потнев	DRILLERS REM	(ounty F	Ra 44	N 113	8957
ONTRACTOR	ADD ESS ADD ESS Bok MALL OF WELLE Todd	A WeILDR: RS Presco TEPHNICIAN ZEQUSON	Iling &	ELL TECHNICIAN'S	DATA SOURCE O DATE OF IN U M MEMARKS	58 CONTAA 1897ECT ION	B 7 7 A	PR 2 9 199	32 *** **
ļ	MINISTR	OF THE ENVIRON	DAY21 W	0 4 yr.94	OFFI			CSS.1	ES 11/86) FORM 9

	11.	Far and sbu	in a lon Bio	CK. TRACT AVEY ETC	
	- JACA	rontret			
GENERAL COLOUR	MOST	OG OF OVERBURDEN AND BED	ROCK MATERIALS		DEPTH · FEET
Black	TopSail	t.	Solt		
Brown Grey	Story	Stones	+ Pac Hard	Real	7 200
	e.				
	3				, <u>, , , , , , , , , , , , , , , , , , </u>
31		Image: 1 mining the second		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
AT - FEET	KIND OF WATER FRESH 3 DSULPHUR ¹⁴ SALTY 6 DAKERALS FRESH 3 DSULPHUR ¹⁹	HS:00 DAM HKCHES HCHES			INCHES FEET
15 ⁴ ² ¹ ² 20 ⁷ ² ² ²	SALTY 4 DIMERALS GAS GAS FRESH 3 DSULPHUR 24 SALTY 4 DIMERALS 6 GAS GAS 5 7 FRESH 3 DSULPHUR 24 SALTY 6 GAS 25 SALTY 6 GAS 27 SALTY 6 GAS 27 SALTY 6 GAS 27	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 105 20-13 1 ROM 1 ROM	O ¹⁴⁻¹⁷ 22-23	TYPE LEAD PACKER ETC.
2 D	SALTY 6 GAS	UTO A COPEN HOLE	1 2 2 d a		
	2 □ BAILER WATER LEVEL END OF PUMPING 22-24 15 MINUTES 3100 24-28	Э сри 15-16 ЗО 11-10 ионяз Доляз Доляз 100 учець роцяна 2 Доляз 1 ЗО мілицтез 45 Мілицтез 60 1 ЗО мілицтез 45 Мілицтез 60 1 1 20-35-3 ЗО мілицтез 45 Мілицтез 45 1 10 32-34	IN DIAGRAM BELOW S LOT LINE INDICAT	HOW DISTANCES OF WELL	FROM ROAD D
Z O FEET		ET AT WAILER AT END OF TEST AT	101 Hourson	entre 5	+=+
C SHALLOW 50-33 FINΔ1	PUMP SETTING	10 FEET RATE GPM		1. 9	a 4
STATUS OF WELL	2 DOBSERVATION WELL 3 D TEST HOLE 4 D RECHARGE WELL 56 , BL DOMESTIC 7 STOCK	ABANDUNED POOR QUALITY UNFINISHED DEWATERING		N .	in to
WATER USE	3 IRRIGATION 4 INDUSTRIAL 0 OTHER	7			Dere le
	2 ROTARY (CONVENTI	€ □ BORING ONAL) 7 □ DIAMOND ■ □ JETTING ■ □ DRIVING			> \0
METHOD OF CONSTRUCTIO	N 4 D ROTARY (AIR) 5 AIR PERCUSSION		DRILLERS REMARKS		105183

🗑 Ontario	Ministry of Well the Environment	^{Tag N} ∕, ≜, 038 €	ielow)	Regulation 903 Ontar	Well Record
Instructions for Completin	ng Form	A038	362		page of
For use in the Province All Sections must be con Questions regarding con All metre measurement Please print clearly in blu Well Owner's Information	of Ontario only. This doct mpleted in full to avoid del apleting this application ca is shall be reported to 1/ e or black ink only.	ument is a permanent I ays in processing. Furt n be directed to the Wi 10 th of a metre.	egal document. F her instructions an ater Well Manage	Clease retain for future refer dexplanations are available ment Coordinator at 416-2: Ministry Use Only ON ↓	rence. on the back of this form. 35-6203.
C - Q d C RR#/Street Number/Name GPS Reading NAD 8 3 (8) Cor 8 3 (8) C	Street Spend Street Spend HEGG4944	$c \neq n \stackrel{n}{\leftarrow} \frac{e}{c \neq v} $	VarAS DU r mVillage se/Model Mod	S Site/Compartment e of Operation: Undifferentiated	/Block/Tract etc. ted X Averaged
-og of Overburden and Be General Colour Most common	edrock Materials (see in material Other	nstructions)	Gener	al Description	Depth Metres
Mawn Ton Se	iL Hart F	G 7	Genera		From To
Tay Limest	lane take				1.8 C. C G. C 44.8
Hole Diameter	Co	Instruction Record		Test of We	ell Yield
$\begin{array}{c c} \hline From & To & Centimetres \\ \hline O & \hline U_{L} & \hline O & 25, cc \\ \hline \end{array}$	Inside diam Material centimetres	Wall Dept thickness centimetres Fron	h Metres	Pumping test method Drav Time/V Pump intakenet ar- (metres)	Vater Level Metres min Metres
Water Record	S.24 Steel Fibregla Plastic Concrel Galvanized	1355 te 0.48 0	6.6	Pumping rate - (litres/min) 44 4 Duration of pumping 2	1 3, 01 3, 4 2 -
m Fresh Sulphur Gas Sally Minerals	Steelibregia PlasticConcret Galvanized SteelFibregia	1955 16 1955		Final water level end 3 of pumping netres Recommended pump 4 type.	3, 9 3 ~ 3, 9 4 ~
Gas Sinv Minerals	Plastic Concret	Screen		Recommended pump 5 depth	5 1 10 1
After test of well yield, water was	diam Steel Fibregla diam Plastic Concret	Slot No.		(litres/min) 15 If flowing give rate - 20 (litres/min) 25 If pumping discontin- ued, give reason. 30	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
Chlorinated Yes No	Open hole	o Casing or Screen			- 40
Plugging and Se	aling Record	ular space 🔲 Abandonme	ent	Location of Well	60
Depth set at - Metres Material and type From To	e (bentonite slurry, neat cement slu	urry) etc. Volume Placed (cubic metres)	In diagram belo Indicate north b	w show distances of well from road y arrow.	
				Vacante	FI
Cable Tool Cable Tool Rotary (conventional) Rotary (conventional) Rotary (reverse) Rotary	Iethod of Construction air) Diamond sussion Jetting Driving Driving	I Digging		- Lon	notics IV
Domestic Industria Stock Comme Irrigation Municip	Water Use al Public Si rcial Not used al Cooling	upply Other	RA Audit No	Date Well	Completed
Water Supply Recharge we Observation well Abandoned, Test Hole Abandoned,	Final Status of Well IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	ed Abandoned, (Othing	er) Was the well or package deliver	38136 wner's information ed? Yes No	2006 08 03
Well Conversion of Well Conversion of Well Conversion of Well Contractor	tractor/Technician Informa	Well Contractor's Licence No GSGS	Data Source	Ministry Use Only Contractor Date of Inst	6565 pection YYYY MM DD
Venue of Well Technician (last name, f Janue of Well Technician (Contractor Signature of Technician/Contractor	rst name)	Wall Technician's Licence N C ~ / Y Y Date Submitted	o. Remarks	τ Δυψb Well Recor	rd Number
0506E (09/03)	Contractor's Copy	Ministry's Copy	Owner's Copy	Cette formule	est disponible en français

🕅 Ontario	Ministry of the Environment	Well Tag	er below)	Regulation 903 Ontai	Well Record
Instructions for Complet	ing Form	Ã05	2125		page of
 For use in the Province All Sections must be co Questions regarding co All metre measuremer Please print clearly in b Well Owner's Information 	e of Ontario only. This ompleted in full to avoid ompleting this application the shall be reported use or black ink only.	document is a perma d delays in processing on can be directed to to 1/10 th of a metre.	Inent legal document, p. Further instructions a b the Water Well Help	Please retain for future refe nd explanations are available Desk (Toll Free) at 1-888-3 Ministry Use Only CON	rence. on the back of this form. 396-9355.
Wen Owner's Information	51. Sten		d <i>WardSOUrs</i>	Site/Compartment	Block/Tract etc.
GPS Reading NAD ZO 813/2	SF Speric 045661414	$\frac{2}{9}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{5}$ $\frac{1}{6}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}$	Pencerville nit Make/Model Mo E (I = X	de of Operation: Undifferentia	ted 🕅 Averaged
General Colour Most commo	n material	Other Materials	Gong	ral Description	Depth Metres
BLA TAS			Gene		From To
Tay (imester	E Blac	paling h palin	te		1.2 6.6 6.6 54.5
Hole Diameter]	Construction Dec	d		
Depth Metres Diameter	Inoide		Donih	Purpoing test methods	N Down Recovery
From To Centimetres	diam Materia	al thickness	Depth Metres	Time V	Vater Level Time Water Level
1 6.6 25.40	centimetres	centimetres	From To	Rump intake sat at low	Metres min Metres
6 4.e.p 7=040		Casing		(metres) 40 Level	4.6 4.9
	Steel F	ibreglass		Pumping rate - 1	1
Water Record	IS,24 Balvanized	concrete G. 48	0 6.6	Duration of pumping 2 (13246
Water found Kind of Water		ibreglass		hrs + min	
m Fresh Suphur		oncrete	а. С	Final water level end 3 (4. 9 3 4. 5
Gas Salty Minerals	Galvanized			Recommended pump	- 1/1.5
I m Eresh Sulphur	Steel F	ibreglass		Shallow F Deep	- 4 4 C
Gas Salty Minerals		oncrete		Recommended pump 5	- 5
Eresh Sulphur		Screen		Recommended pump 10	· · · · · · · · · · · · · · · · · · ·
Gas Salty Minerals	Outside Steel	ibreglass Slot No		rate. (litres/min) 15	10 -
After test of well visited water was	diam Plastic CC	oncrete		If flowing give rate - 20	<u> </u>
Clear and sediment free	Galvanized			If pumping discontin- 20	25 ~
Other, specify		No Casing or Scree	n	ued, give reason. 40	- 40 -
	Open hole			50	- 50 -
- Ales Bile					<u> </u>
Plugging and S	ealing Record	Annular space Aba	Placed	Location of Well	
From To Material and ty	pe (penionite slurry, neat cem	ent siumy) etc. (cubic n	netres) Indicate north	by arrow.	e / I
V 6.6 US	ich Grou	17 1		11.15/1	SIL
		Bac	541 /	Moth	METERS
			<u> </u>	1 1/2	Λ
			/	f-1	F1
	Method of Construction	l	/		
Cable Tool	(air) Dia	mond D	igging		I
Rotary (conventional) Air per Rotary (reverse) Boring	cussion Jet	ting C	ther N	Delit in	
	Water Use			(power	1 >>
Stock Comm	ercial IN0	t used —	RO	- / `	
Irrigation Municip	Final Status of Woll	oling & air conditioning	Audit No.	55705 Date Well C	A YAYAA MAL DO A
Water Supply Recharge w	rell Unit, insufficient supply Dev	inished Abandone watering	ed, (Olher) Was the well of package delive	owner's information red? Yes No	2007 0700
Well Cor	tractor/Technician Infe	ormation		Ministry Use Only	
Name of Well Contractor	Dallac	Well Contractor's Lice	ence No. Data Source	Contractor	
Bopiness Address (street name, num	per, city etc.)	636)	Date Rebeiver		ection yyyy has an
KK 3 Vort	2 August	9	JEXTENDO		DD
Name of Well Technician (last name,	(Irst name)	Well Technician's Lic	ençe No. Remarks	Well Record	d Number
Signature of Technician/Contractor		Date Submitted	MAN DO		
X Your	4	2010	106		
USUGE (08/2006)		Distriction	1.7 of 165	Cette formule	est disponible en francais

Page 4% 01/465

μņ nç

🕅 Ontario	Ministry of Well the Environment		er below)	Regulation 903 Ontario	Well Record
Instructions for Completin	ng Form	405272	6		page of
 For use in the Province All Sections must be con 	of Ontario only. This doc mpleted in full to avoid del	ument is a permanent leg lays in processing. Further	al document. P instructions and	- lease retain for future refere d explanations are available or	nce. 1 the back of this form.
 Questions regarding cor All metre measuremen 	mpleting this application of ts shall be reported to 1,	an be directed to the Wa /10 th of a metre.	ter Well Help D	Desk (Toll Free) at 1-888-39	16-9355.
 Please print clearly in blu Well Owner's Information 	ue or black ink only.	nformation MUN		Ministry Use Only	
well owner s mormanon	and Location of Weith				
CA (haile 5)7 BB#/Street Number/Name	rect Spence	rv. 11 e Golwan	ds burs	Site/Compartment/B	Lock/Tract ata
6A Charle St GPS Pooding NAD 700	rect Spence	11- Spen	CErvill	<	
	456598 496	51226 ETL		Differentiated, s	specify
General Colour Most common	material Other	Materials	Genera	I Description	Depth Metres
Brown Tap Soi	1				0 1.2
Gray Limeste	ne Black	Prinite			1.2 4.6
62ay Lineste	177 Blach	Dolimite			6, 6 38,7
Hole Diameter	C	onstruction Record		Test of Well	Yield
Depth Metres Diameter From To Centimetres	Inside diam Material	Wall Depth	Metres	Pumping test method Draw I	Down Recovery
0 6.6 25.40	centimetres	centimetres From	То	Pump intake set at a Static	Aetres min Metres
	Steel Eibreel	Casing		(metres) 40 Level	16 51
		ne 12,48 0	6.6	(litres/min) 44	- 7.0
Water Record	Steel Fibreal	ass	_	hrs + min	· / 2 4· 5
m Fresh Sulphur		te		Final water level end 3 L4	, 8 3 4, 4
	Galvanized	ass		Recommended pump 4	G 4 ~
Gas Salty Minerals		te		Recommended pump 5 5	; (5 -
m Fresh Sulphur	Gaivanized	Screen		Recommended pump 10	- 10 -
Gas Sally Migerals	Outside Steel Fibregi	ass Slot No.		rate. (litres/min) 15	<u> </u>
After test of well yield, water was	Plastic Concre	le		O (litres/min) 25	- 25 -
Olher, specify	N	o Casing or Screen		ued, give reason. 40	- 30
Chlorinated KYes 🗌 No	Open hole			50	<u> 50 60 60 </u>
Plugging and Se	aling Record	nular space 🔲 Abandonment		Location of Well	
Depth set at - Metres From To Material and typ	be (bentonite slurry, neat cement sl	urry) etc. Volume Placed (cubic metres)	In diagram below Indicate north by	show distances of well from road, arrow.	lot line, and building.
1 6.4 Ch	1 ch Geou	+ 2	N	Siles we	14.8
		<u> </u>	ì	Noit	· motors
				1	Λ
M	lethod of Construction				7
Cable Tool	air) Diamond	Digging			
Rotary (reverse)		Other			
Domestic Industria	Water Use	upply 🗍 Other	A	(Onlowa)	
Stock Commer Irrigation Municipa	rcial Not used al Cooling	air conditioning	Audit No	Date Well Co	mpleted
At Water Supply	Final Status of Well	ad Abandonad (Othor)	Mas the well ow	55703	20010100
Observation well Abandoned,	insufficient supply Dewater	ing	package delivered		2007 0100
Well Cont	tractor/Technician Informa	ation	Data Source	Ministry Use Only	
Daves uz //	Prilling	6 5 6 5 5 5 Cence No.	Data Source	Contractor	
High Street name, number	Augusta		Date Redetver	Y2000 MM DD Date of Inspec	tion yyyy MM DD
Name of Well Technictan (last name, fi	irst name)	Well Technician's Licence No.	Remarks	Well Record N	Number
Signatore of Technician/Contractor		Date Submitted	T.		
0506E (08/2006)		Page 48 of	465	Cette formule es	t disponible en français

Po	ntario	Ministry of the Environm	ent	Well Tag		1165	Regulation	903 0	We	II R	ecord
Measuren	ents recorded in:	Metric	🗌 Imperial			1100	Regulator		Page_		of
Well Owr	ner's Informati	ion									
First Name Concerned Mailing Add	107: Onterio Kwood Bri Iross (Street Num) Toterr	Last Nam Conce Contractor Soor/Namo) Conce	e / Organizatio Constru NRd W	n uction h eat C	s Iunicipality Dxforch Hills	E-mail Address Province ON	Postal Code	7 <u>0</u> 7		Well (by We 5 Av	Constructed II Owner area codel 4335
Address of	ation Well Location (Str	eet Number/Na	me)	I	ownship		Lot	-	Concession	L	······
12 Cede	y SH trict/Municipality	, E	6 Crels	LOEST E	Edwardob	wig .		Provin	38	Postal	Gode
Gre	nuille				Spencery	ille		Ont	ario	KOi	ENXO
UTM Coord NAD	8 3 1 8 4	ting ちんすにユ	Northing	1786	Print 2 cm Plan	on Number	-41	Other			
Overburde	en and Bedrock	Materials/Aba	ndonment Se	aling Reco	rd (see instructions on the	back of this form)				Der	sh Inviti
General C	alour Mas	t Common Mate	erial	Oth	er Materials	Ger	eral Description			From	
Brow	in C	lay				С Ц	CTT			p a i	20110
Grey	hard I	mestore	-			11	and		0	11	24.64
							Develop of M				
Depth Se	et at (m/t)	Type of	Sealant Used		Volume Placed	After test of well yel	d water was	D	aw Down	F	ecovery
From	To	(Materia	and Type)		(m ² /R ²)	Clear and sand	i free	Time (min)	Water Level (m/fi)	Time (min)	Water Level (m/it)
6.90	φ Cer	nent Kies	Same 61	outed	e 16	If pumping discontin	ued, give reason:	Static Level	5.04		5.15
								1	5,07	1	5.13
						Pump intake set at	(mvft)	2	5.09	2	5,12
Mot	hod of Construc	rtion		Well Us	P	Pumping rate (Vitim	I GPMJ	3	5.10	3	5.11
Cable To		Diamond [Public	Comme	rcia: 🗌 Not used	Dorahou of pumpin	25	4	5.10	4	5,10
Ka Retary (Retary (Conventional) [] . Reverse) [] [Jetting Driving	kDomestic] Livestock	U Municip	sl 🗌 Dewatering le 🗌 Monitoring	$\int hrs + O$	min	5	5.11	5	5.09
Boring	[] I	Digging C] Irrigation] Industrial	Cooling	& Air Conditioning	Final water level end	i of pumping (avit)	10	5.12	10	5.08
Cther, s	oecify] Other, specify			If flowing give rate	(l/min / GPM)	15	5.12	15	5.04
inside	Construct	tion Record -	Casing Dept	h (<i>m/ft</i>)	Status of Well	Recommended put	mp death (m/ft)	20	5.13	20	
Diameter (cm/in)	(Galvanized, Fibri Concrete, Plastic,	agiass. Thuckra Steel) (anvir	BS From	То	Replacement Well Test Hole	21.3	34	25	5.14	25	
25.40	GORAHA	lo	Ø	625	Recharge Well	(Vmin / GPM)	mp rate	30	5.14	30	
15.88	Steel	-49	30	6.25	Dewatering Well Observation and/or	Well production (Vic	nin 7 GPM)	40	5.14	40	
15:00	Anna Hal	0	1.25	2419	Monitoring Hole	Disinfactor(2		50	5.15	50	
1000	opennor	<u> </u>	0.00	0 1101	(Construction)	X Yes No		60	5.15	60	*
	Constru	ction Record -	Screen		- Insufficient Supply Abandoned, Poor		Map of W	ell Lo	cation		2,613
Diameter (cm/in)	Material (Plastic, Galvanized	d, Steel) Sict N	0. From	h (<i>m/ll)</i> To	Water Quality	Please provide a m	sh nerow roriowing	msouc	cons on the t	erck.	
Lavery					specify		Count	NP	15#21		
					Other, specify			40	<u> </u>	T	
	Wa	iter Details	19.332030	Prost F	lole Diameter	A A					t.
Water four	nd at Depth Kind :	of Water Ere	sh 🕅 Untester	5 Dep From	th (<i>m/lt</i>) Diameter To (<i>cm/in</i>)						E.
Water four	n/ff) Gas OI nd at Depth Kind (her, specify of Water: Fre	sh Untester	ø	6.25 25,40			7		;	F D
21.031	n/lt) Gas Ot	her, specify		625	24,69 15,55)	7	.	r d
Water tour (f)	nd at Depth Kind (n/lt) Gas 00	ner, specify	sh Untested	1 Martine of	0.01.0.0			1	P		E G
Sal The we	Well Co	ntractor and V	Vell Technici	an Informa	tion			I	19	1	5
Business N	ame of Well Contr	D- lliv	0	We	All Contractor's Licence No. $4 R + 7$			1	HSTR	18	
Business A	ddress (Street Nur	mber/Name)	ig	M.	unicipality	Comments:			301	10	
Province	SOX 108 Postal C	Dade Busi	ness E-mail Ad	dress	NESCOTT						
ON	KOE	OTI				Well owner's Date	e Package Deliver	ed	Minis	try Us	e Only
Bus Telephi (~12k	one No. (inc. area co G a 5 Ll Q. C	Name of W	ell Technician	Last Name.	First Name)	delivered	10010	96	Audit No.	10	4993
Well Technic	sian's Licence Mar IS	gnature of Tech	mician and/or C	ontractor Da	te Submitted	Ves Date	a Work Completed	5. F	MAR Z	4 4	u il
C906E (12.20	CTD (Toda	Per-	0	Page 49 of	465	01001	al	Reperced (o [∽] raler	tar Ontano 2007
					in a second						

Ontario	Ministry of the Environment	Well Ta	g No. (†	no	1166	Regulation	1 903 C	We Intario Wate	II R er Res	ecord
Measurements recorded	in: 😥 Metric 🔄 Ir	nperial	1	00	1100			Page_		of
Well Owner's Inform	ation				E		10			
Aling Address (Street Nu	Brothers (mhen/Name)	constru	etiwo Municipality		E-mail Address Province	Postal Code	7-25	Telephone N	Well (by We n mo	Constructed ell Owner area oppei al o o C
Well Location	S Ranch Rd	i west	DXtord M	1115	010	KOG I	10.0	6130	2.0	4000
Address of Well Location ()	Street Number/Name)	-	Fownship	4		Lol		Concession	6	
County/District/Municipalit	adax Str	eer (CULCIC Sity/Tawn/Vitlage	e e	بر الم م		Provin	ce.	Posta	Code
UTM Coordinates Zone, E	Q astric Nor	thing	Spenc Junicipal Plan a	er v Ind Subic	A Number		Onta	ario \	KO	EIXO
NAD 8 3 1 8 4	1564604	9653017	Partac	m Pla	an 15R -10	1430				
Overburden and Bedroo	ck Materials/Abandor	nment Sealing Reco	ord (see instruction or Materials	ons on the	back of this form)	eral Description			De;	ath (<i>m/R</i>)
Brancia (~\~				50	-C-t-			X	FOIL
Grey	instand				H	and			F0.	- 24.69
- y	- (]) Societ C Sublime									
										1
		t 								
										-
The second secon				-	Contraction of the second	D				
Depth Sel at (m/ft)	Annular S Type of Seal	ant Used	Volume Pla	aced	After test of well yield	Results of Wi	Dr	aw Down	F	lecovery
From To	(Material and	t Type)	(m ¹ /ft ²)		Clear and sand	free	Time (nwn)	Water Level (m/t)	Time (min)	Water i.evel (m/ft)
6.35 4 6	ement Pressi	me Grouted	016		If pumping discontinu	ued, give reason:	Static Level	5.27		5.335
							1	5.29	1	5.31
					Pump intake set at	(m/ft)	2	5.29	2	5.30
					Pumping rate (limin	/ GPMI	3	5.295	3	5.245
Method of Constr	Dramond Pub	lic Comme	ae arcial ∏No	t used	68.	25	4	5.30	4	5.29
K Retary (Conventional)	Jetting 🐱 Dom	nestic 🗌 Municip stock 🗍 Test Ho	al Do	watering	Duration of pumpin	g min	5	5.30	5	5.29
Boring	Digging Digging	ation Cooling	& Air Conditionin	iĝ Antorioĝ	Final water level end	of pumping (avii)	10	5.31	10	5.285
Chier, specify		istrial er, specify			If flowing give rate (35 Vmin / GPMI	15	5.32	15	5.28
Constr	uction Record - Casi	ing	Status of	Well			20	5.32	20	5.275
Diameter Open Hole OR Diameter (Galvanized, Fi	Matenai Wall breglass Thickness	From To	Replaceme	ply int Well	Recommended pur	np depth (<i>m/it)</i> 24	25	532	25	5.17
AT US A L		A LOS	Test Hole Recharge \	Nell	Recommended pur	np rate	30	5.200	30	5101
05.40 opent	lole	4 6.05	Dewatering	Well	45	.5	40	5.33	40	
15.88 Steel	840	\$ 6.25	Monitoring H	fole	Well production (Un	tin / GPM)	50	5.32	50	-
15.55 Open H	ole	6.92 34.60	(Construction	on)	Disinfected?		60	5 325	60	1
Const	ruction Record - Scree	n saele a state	Insufficient	supply		Map of W	ell Loo	cation		
Canside Mataria	at Slot No	Depth (m/ft)	Water Qual	a, ⊭ocr lity	Please provide a ma	ip below following	instruct	ions on the b	ack.	
(cm/m) (Plastic, Galvan)	zed steel)	From To	specify	a, other,			C	ounty	24	191
		· · · · · · · · · · · · · · · · · · ·	Other. spec	cify		A				
Concernant of the second se						4	N			to
Water found at Depth Kind	Vater Details	Untested Dep	tole Diameter th (m/ft) D	hameter						24
13.72(mv11) Gas	Other, specify	From	To	(cm/in)			Ē		-	- in
Water found at Depth Kind	d of Water:Fresh 🍺 Other_scecify	QUntested P	6.92 9	5.40			I.	-> 0 4 -=	5.48	• 10
Water found at Depth Kind	d of Water Fresh	Untested 6.00	24.69 1	5,55			16	0110		W
(m/ft) Gas	Other, specify						1			
Business Name of Well Cor	ontractor and well in tractor	i echnician informa	tion all Contractor's Lio	ence No.			1			
Splash W	ell Drilli	ing 1	F87	7	Communic	Martin Martin Strate Strategy and	I			
POBOX 10	83	- A	resco	TT	COMMERCIE					
Province Posta	Code Business	E-mail Address			Might growthe P	Paskers D. :		107		- 0-1
Bus Telephone No. (inc. area	code) Name of Well Te	echnician (Last Name.	First Name)		information package	Chackage Deliver	07	Minis Audit No	I O	a O O A
61392548	85 Fergu	pontode	L.		delivered Date	Work Completed	DTD	Z,	LU	4994
T:478	Signature of Technician	andror Contractor Da	te Submitted	DAL	A Tes	1001	21	MAR	22	2010
05055 (12/2007)	(-Y	0-0	rage 5	S Copy	405		~ *	© Gueen s	Photor	Inr Ontario (2007

Ontario Ministry of the Environment	Well Tag No. (Place Sticker an Tag#: A	ndlor Print Below) 133708 Regulatio	NO n 903 Ontario Wat Page	ell Record
Address of Well Location (Street Number/Name)	Township	Lot	Concession	
Cectar Street	City/Town/Village	ingh 1 St	Province	Postal Code
UTM Coordinates Zone, Easting, Northing	Spencer Municipal Plan and Suble	UIUL Number	Ontario	KOELKO
NAD 8 3 1 8 4 565 711 4365	189 Plan 40)		
Overburden and Bedrock Materials/Abandonment Se General Colour Most Common Material	Conter Materials	back of this form) General Description	n	Depth (m/ft)
Red Sand Fill		Soft		¢ 5'
Brown Sandy Clay		Padied		51661
Grey Limestone		Broken Sof	t lo	'6" 25'
Grey Limestone		Hard	Ĉ	101
Annular Space		Results of W	ell Yield Testing	Received and
Depth Set at (mlft) Type of Sealant Used From To (Material and Type)	Volume Placed (m³/ft³)	Clear and sand free	Time Water Level	Time Water Level
31 Ø Cement Pressions	Granted 20,31	If pumping discontinued, give reason:	Static I Q	
			1 15	1 14
		Pump intake set at (m/ft)	2 18	2 10.7
		Pumping rate (Ilmin-/ GPM)	3 19.7	3 9.4
Method of Construction Cable Tool Diamond Public	Well Use	90	4 2017	4 8.8
Rotary (Conventional) Jetting Domestic Rotary (Reverse) Driving Livestock	Municipal Dewatering Test Hole Monitoring	$\underline{\qquad}$ hrs + $\underline{\bigcirc}$ min	5 2114	5 8,5
Boring Digging Irrigation	Cooling & Air Conditioning	Final water level end of pumping (m/ft	10 22,6	10 81
Other, specify Other, specify		If flowing give rate (Ilmin GPM)	15 22.9	15 8
Construction Record - Casing Inside Open Hole OR Material Wall Dept	Status of Well h (m/ft)	Recommended pump depth (m/ft)	20 23.1	20 7,9
Diameter (Galvanized, Fibreglass, (cmlin) Concrete, Plastic, Steel) (cmlin) From	To Replacement Well	80'	25 23.2	25 7,9
10" OpenHole \$	31 CRecharge Well	(Ilmin / GPM)	30 23,3	30 7,8
6/4" Steel 0188 \$	31' Observation and/or	Well production (Ilmin / GPM)	40 23.4	40
618" Open Hole 31'		Disinfected?	50 23.4	50
	Abandoned, Insufficient Supply	Yes No 160	60 3.4	60
Construction Record - Screen Outside Material Depti	Abandoned, Poor (m/ft) Water Quality	Map of W Please provide a map below following	fell Location g instructions on the b	ack. 🛛 .
Diameter (cmlin) (Plastic, Galvanized, Steel) Slot No. From	To Abandoned, olher, specify	C	-+0	I#DI W
- -			Dunlyk	$a \alpha \mu$
		t t		
Water Details	Hole Diameter Depth (m/ft) Diameter	v		
15' (mlft) Gas Other, specify	From To (cmlin)	5		
Water found at Depth Kind of Water: Fresh Montested	φ 31 10		an a share the state	
Water found at Depth Kind of Water: Fresh Untested	31 101 618	13 U		
(m/tt)Gas Other, specify	n Information			
Business Name of Well Contractor	Well Contractor's Licence No.	v k→0		
Jusiness Address (Street Number/Name)	Municipality	Comments:		(:
POBOX LOB3	PURSCOTT	160 chlorine o	altor 4:	eldTent
OW 40EVTO	1633	Well owner's Date Package Deliver		try Use Only
Bus.Telephone No. (inc. area code) Name of Well Technician (I	Last Name, First Name)	package delivered 20130H	18 Audit No.	27004
Well Technician's Licence No. Signature of Technician and/or Co	ontractor Date Submitted	Date Work Completed	L 2	57094
1 1 1 0 Jadd	Ministry's Copy	<u>⊔™</u> ₽01304	() Received	202019

Ministry's Copy Page 51 of 465

1000 TW1-WELL DRAWDOWN VS. TIME-KOLLAARD FILE 220996 Q = 43.2 m³/day (30 LPM) T = 2.3Q / 4pi(ds) ds = 0.02 m T = 395.3 m²/day 100 TIME LAPSED (minutes) ds = 0.02 m10 Pump Rate adjusted C. I 0.0 0.6 -0.1 0.5 0.7 0.1 0.3 0.4 0.2 (zenterne) HT9AD NWODWAAD

Page 52 of 465

ime Lapsed	Abs Pres	Temp	Water Level	Drawdowr
(minutes)	(kPa)	(°C)	(m)	(m)
1	397.747	9.275	-7.412	-0.01
2	391.342	9.275	-8.065	0.65
3	393.618	9.275	-7.833	0.42
4	394.658	9.275	-7.727	0.32
5	393.405	9.176	-7.855	0.30
7	394.12	9.176	-7.782	0.37
8	394.38	9.176	-7.755	0.34
9	394.38	9.176	-7.755	0.34
10	394.478	9.176	-7.755	0.35
12	394.363	9.077	-7.757	0.35
13	394.363	9.077	-7.757	0.35
14	394.265	9.077	-7.767	0.36
15	394.038	9.077	-7.79	0.38
10	394.005	9.077	-7.793	0.39
18	394.005	9.077	-7.793	0.38
19	394.135	9.077	-7.78	0.37
20	394.233	9.077	-7.77	0.36
21	394.395	9.077	-7.754	0.34
22	394.493	9.077	-7.744	0.33
24	394.46	9.077	-7.747	0.33
25	394.493	9.077	-7.744	0.33
26	394.525	9.077	-7.74	0.33
27	394.33	9.077	-7.76	0.35
28	394.428	9.077	-7.75	0.34
29	394.363	9.077	-7.757	0.35
31	394.363	9.077	-7.757	0.35
32	394.363	9.077	-7.757	0.35
33	394.395	9.077	-7.754	0.34
34	394.525	9.077	-7.74	0.33
35	394.428	9.077	-7.75	0.34
30	394.395	9.077	-7.754	0.34
38	394.493	9.077	-7.744	0.33
39	394.59	9.077	-7.734	0.32
40	394.59	9.077	-7.734	0.32
41	394.688	9.077	-7.724	0.31
42	394.655	9.077	-7.727	0.32
43	394.33	9.077	-7.76	0.35
45	394.33	9.077	-7.76	0.35
46	394.428	9.077	-7.75	0.34
47	394.558	9.077	-7.737	0.33
48	394.558	9.077	-/./3/	0.33
49 50	394.655	9.077	-7.727	0.32
51	394.623	9.077	-7.73	0.32
52	394.688	9.077	-7.724	0.31
53	394.655	9.077	-7.727	0.32
54	394.655	9.077	-7.727	0.32
55 56	394.558	9.077	-7.727	0.33
57	394.688	9.077	-7.724	0.31
58	394.655	9.077	-7.727	0.32
59	394.655	9.077	-7.727	0.32
60	394.655	9.077	-7.727	0.32
67	394.688	9.077	-7.724	0.31
63	394.623	9.077	-7.73	0.32
64	394.493	9.077	-7.744	0.33
65	394.428	9.077	-7.75	0.34
66	394.493	9.077	-7.744	0.33
67	394.558	9.077	-7.737	0.33
69	394.59	9.077	-7.73	0.32
70	394.655	9.077	-7.727	0.32
71	394.655	9.077	-7.727	0.32
72	394.72	9.077	-7.721	0.31
73	394.59	9.077	-7.734	0.32
74 75	394.623	9.077	-7.73	0.32
76	394.688	9.077	-7.724	0.32
77	394.688	9.077	-7.724	0.31
78	394.688	9.077	-7.724	0.31
79	394.72	9.077	-7.721	0.31
80	394.753	9.077	-7.717	0.31
87	394.688	9.077	-7.724	0.31
83	394.655	9.077	-7.727	0.52
84	394.655	9.077	-7.727	0.32
85	394.623	9.077	-7.73	0.32
	204 752	0.077	-7.717	0.31
86	334.733	5.077		

89	394.72	9.077	-7.721	0.31
90	394.753	9.077	-7.717	0.31
91	394.72	9.077	-7.721	0.31
97	394 655	9.077	-7 727	0.32
02	204 77	9.077	7 721	0.31
04	204 795	9.077	7 714	0.30
05	204 72	9.077	-7.714	0.30
95	394.72	9.077	-7.721	0.31
96	394.72	9.077	-7.721	0.51
97	394.753	9.077	-/./1/	0.31
98	394.785	9.077	-7.714	0.30
99	394.785	9.077	-7.714	0.30
100	394.785	9.077	-7.714	0.30
101	394.655	9.077	-7.727	0.32
102	394.688	9.077	-7.724	0.31
103	394.72	9.077	-7.721	0.31
104	394.753	9.077	-7.717	0.31
105	394.753	9.077	-7.717	0.31
106	394.785	9.077	-7.714	0.30
107	394.85	9.077	-7.707	0.30
108	394,785	9.077	-7.714	0.30
109	394,818	9.077	-7.711	0.30
110	394,785	9.077	-7.714	0.30
111	39/ 72	9.077	-7 721	0.31
117	204 655	D.077	7.721	0.32
112	394.033	9.077	-7.727	0.32
115	394.033	9.077	-7.727	0.32
114	394.72	9.077	-7.721	0.31
115	394.72	9.077	-7.721	0.31
116	394.818	9.077	-7.711	0.30
117	394.785	9.077	-7.714	0.30
118	394.818	9.077	-7.711	0.30
119	394.785	9.077	-7.714	0.30
120	394.72	9.077	-7.721	0.31
121	394.818	9.077	-7.711	0.30
122	394.818	9.077	-7.711	0.30
123	394.85	9.077	-7.707	0.30
124	394.883	9.077	-7.704	0.29
125	394.85	9.077	-7.707	0.30
126	394.883	9.077	-7.704	0.29
127	394,948	9.077	-7.697	0.29
128	394.85	9.077	-7.707	0.30
129	394 785	9.077	-7.714	0.30
120	394.85	9.077	-7 707	0.30
121	304.049	9.077	7.697	0.30
131	304.940	0.077	7.704	0.25
132	394.885	9.077	-7.704	0.29
133	394.85	9.077	-7.707	0.30
134	394.818	9.077	-7.711	0.30
135	394.85	9.077	-7.707	0.30
136	394.818	9.077	-7./11	0.30
137	394.85	9.077	-7.707	0.30
138	394.753	9.077	-7.717	0.31
139	394.785	9.077	-7.714	0.30
140	394.85	9.077	-7.707	0.30
141	394.818	9.077	-7.711	0.30
142	394.818	9.077	-7.711	0.30
143	394.818	9.077	-7.711	0.30
144	394.85	9.077	-7.707	0.30
145	394.85	9.077	-7.707	0.30
146	394.85	9.077	-7.707	0.30
147	394.948	9.077	-7.697	0.29
148	394.818	9.077	-7.711	0.30
149	394,818	9.077	-7.711	0.30
150	394,915	9.077	-7.701	0.29
151	394.85	9.077	-7 707	0.30
157	394.915	9.077	-7 701	0.30
152	204 992	0.077	7.701	0.25
155	394.003	9.077	-7.704	0.29
154	394.865	9.077	-7.704	0.29
122	304.785	9.077	-7.714	0.30
156	394.753	9.077	-7.717	0.31
15/	394./53	9.077	-7./1/	0.31
158	394.72	9.077	-7.721	0.31
159	394.72	9.077	-7.721	0.31
160	394.753	9.077	-7.717	0.31
161	394.818	9.077	-7.711	0.30
162	394.818	9.077	-7.711	0.30
163	394.688	9.077	-7.724	0.31
164	394.753	9.077	-7.717	0.31
165	394.785	9.077	-7.714	0.30
166	394.85	9.077	-7.707	0.30
167	394.753	9.077	-7.717	0.31
168	394.753	9.077	-7.717	0.31
169	394.623	9.077	-7.73	0.32
170	394.688	9.077	-7.724	0.31
171	394.72	9.077	-7.721	0.31
177	394 753	9,077	-7,717	0.31
173	394.85	9.077	-7.707	0.30
174	394 819	9.077	-7 711	0.30
175	39/ 85	9 077	-7 707	0.30
175	39/ 015	9,077	-7 701	0.50
177	394.015	9.077	.7 701	0.25
170	334.915	9.077	-7.701	0.29
178	394.785	9.0//	-7./14	0.30
1/9	394.818	9.077	-7.711	0.30
180	394.85	9.077	-7.707	0.30
181	394.883	9.077	-7.704	0.29
182	394.883	9.077	-7.704	0.29
183	394.883	9.077	-7.704	0.29

184	394.85	9.077	-7.707	0.30
185	394.85	9.077	-7.707	0.30
186	394.85	9.077	-7.707	0.30
197	20/ 0/8	9.077	-7 697	0.29
107	304.040	0.077	7.007	0.20
188	394.865	9.077	-7.704	0.25
189	394.915	9.077	-7.701	0.29
190	394.785	9.077	-7.714	0.30
191	394.85	9.077	-7.707	0.30
192	394.753	9.077	-7.717	0.31
193	394.818	9.077	-7.711	0.30
194	394.72	9.077	-7.721	0.31
195	394.883	9.077	-7.704	0.29
196	394.818	9.077	-7.711	0.30
197	394 883	9.077	-7 704	0.29
109	204 015	9.077	7.701	0.29
198	334.313	9.077	7.701	0.25
199	394.883	9.077	-7.704	0.29
200	394.915	9.077	-7.701	0.29
201	394.818	9.077	-7.711	0.30
202	394.818	9.077	-7.711	0.30
203	394.85	9.077	-7.707	0.30
204	394.85	9.077	-7.707	0.30
205	394.785	9.077	-7.714	0.30
206	394.753	9.077	-7.717	0.31
207	394 753	9.077	-7.717	0.31
208	394 753	9.077	.7 717	0.31
208	394.733	9.077	7.714	0.31
209	394.785	9.077	-7.714	0.30
210	394.688	9.077	-7.724	0.51
211	394.753	9.077	-/./1/	0.31
212	394.753	9.077	-7.717	0.31
213	394.818	9.077	-7.711	0.30
214	394.785	9.077	-7.714	0.30
215	394.785	9.077	-7.714	0.30
216	394.655	9.077	-7.727	0.32
217	394.59	9.077	-7.734	0.32
218	394,525	9.077	-7.74	0.33
210	394.523	9.077	.7.73	0.32
215	204.655	9.077	7.75	0.32
220	394.033	9.077	-7.727	0.32
221	394.72	9.077	-7.721	0.51
222	394.72	9.077	-7.721	0.31
223	394.753	9.077	-7.717	0.31
224	394.785	9.077	-7.714	0.30
225	394.753	9.077	-7.717	0.31
226	394.818	9.077	-7.711	0.30
227	394.655	9.077	-7.727	0.32
228	394.785	9.077	-7.714	0.30
229	394,753	9.077	-7.717	0.31
230	394 753	9.077	-7 717	0.31
230	304 785	9.077	-7 714	0.30
231	304.705	0.077	7 711	0.30
232	394.010	9.077	7.711	0.30
233	394.818	9.077	-7.711	0.50
234	394.818	9.077	-7.711	0.30
235	394.883	9.077	-7.704	0.29
236	394.72	9.077	-7.721	0.31
237	394.72	9.077	-7.721	0.31
238	394.785	9.077	-7.714	0.30
239	394.85	9.077	-7.707	0.30
240	394,785	9.077	-7.714	0.30
241	394.818	9.077	-7.711	0.30
242	394.85	9.077	-7 707	0.30
242	304.05	9.077	-7 707	0.30
245	304.893	0.077	7 704	0.30
244	394.865	9.077	-7.704	0.25
245	394.785	9.077	-7.714	0.50
246	394.753	9.077	-7.717	0.31
247	394.85	9.077	-7.707	0.30
248	394.85	9.077	-7.707	0.30
249	394.85	9.077	-7.707	0.30
250	394.818	9.077	-7.711	0.30
251	394.948	9.077	-7.697	0.29
252	394.818	9.077	-7.711	0.30
253	394.883	9.077	-7.704	0.29
254	394.85	9.077	-7.707	0.30
255	394.688	9.077	-7.724	0.31
256	394,72	9.077	-7.721	0.31
257	394 753	9,077	-7,717	0.31
259	394 819	9.077	-7 711	0.30
200	204.010	5.077	7 714	0.30
259	394./85	9.077	-7.714	0.30
260	394.85	9.077	-7.707	0.30
261	394.85	9.0/7	-7.707	0.30
262	394.85	9.077	-7.707	0.30
263	394.85	9.077	-7.707	0.30
264	394.72	9.077	-7.721	0.31
265	394.72	9.077	-7.721	0.31
266	394.818	9.077	-7.711	0.30
267	394.72	9.077	-7.721	0.31
268	394.46	9.077	-7.747	0.34
269	394,558	9.077	-7.737	0.33
270	394 72	9,077	-7 721	0.31
270	394.919	9.077	-7 711	0.30
271	394.618	5.0//	7 711	0.50
2/2	394.818	9.077	-7./11	0.30
273	394.72	9.077	-7.721	0.31
274	394.72	9.077	-7.721	0.31
275	394.818	9.077	-7.711	0.30
276	394.818	9.077	-7.711	0.30
277	394.85	9.077	-7.707	0.30
278	394.785	9.077	-7.714	0.30

1	279	394.883	9.077	-7.704	0.29
	280	394 818	9.077	-7.711	0.30
	200	204 95	9.077	-7 707	0.30
	201	394.85	5.077	7.707	0.30
	282	394.85	9.077	-7.707	0.50
	283	394.785	9.077	-7.714	0.30
	284	394.818	9.077	-7.711	0.30
	285	394.818	9.077	-7.711	0.30
	286	394.883	9.077	-7,704	0.29
	287	304.85	9.077	7 707	0.30
	207	204.007	0.077	7.704	0.30
	288	394.885	9.077	-7.704	0.23
	289	394.85	9.077	-7.707	0.30
	290	394.915	9.077	-7.701	0.29
	291	394.883	9.077	-7.704	0.29
	292	394.72	9.077	-7.721	0.31
	293	394.818	9.077	-7.711	0.30
	204	204.85	0.077	7 707	0.30
	204	304.05	0.077	7,707	0.30
	295	594.72	9.077	-7.721	0.31
	296	394.558	9.077	-1.131	0.33
	297	394.558	9.077	-7.737	0.33
	298	394.818	9.077	-7.711	0.30
	299	394.818	9.077	-7.711	0.30
	300	394,493	9.077	-7,744	0.33
	301	30/ /03	9.077	-7 744	0.33
	303	304.455	0.077	7.744	0.32
	502	334.033	9.077	-7.727	0.32
	303	394.688	9.077	-7.724	0.51
	304	394.655	9.077	-7.727	0.32
	305	394.525	9.077	-7.74	0.33
	306	394.623	9.077	-7.73	0.32
	307	394.72	9.077	-7.721	0.31
	308	394.85	9.077	-7.707	0.30
	300	39/ 59	9.077	-7 734	0 37
	310	304.55	9.077	.7 734	0.32
	310	394.59	9.077	-7.734	0.32
	311	394.655	9.077	-1.121	0.32
	312	394.753	9.077	-7.717	0.31
	313	394.818	9.077	-7.711	0.30
	314	394.883	9.077	-7.704	0.29
	315	394.85	9.077	-7.707	0.30
	316	394.883	9.077	-7.704	0.29
	317	394.915	9.077	-7.701	0.29
	318	394.85	9.077	-7.707	0.30
	319	394.818	9.077	-7.711	0.30
	320	396 378	9.077	-7.551	0.14
	321	396 541	9.077	-7 535	0.12
	321	206 606	9.077	7.535	0.12
	322	390.000	9.077	7.520	0.12
	323	396.476	9.077	-7.541	0.13
	324	396.541	9.077	-7.535	0.12
	325	396.833	9.077	-7.505	0.09
	326	396.638	9.077	-7.525	0.11
	327	396.671	9.077	-7.522	0.11
	328	396.703	9.077	-7.518	0.11
	329	396.573	9.077	-7.532	0.12
	330	396.703	9.077	-7.518	0.11
	331	396.736	9.077	-7.515	0.10
	332	396 736	9,077	-7,515	0.10
	322	396 736	9.077	-7.515	0.10
	224	306 769	9.077	.7 517	0.10
	534	390.708	9.077	7.512	0.10
	535	390.0/1	9.077	-7.522	0.10
	336	396.736	9.077	-7.515	0.10
	337	396.768	9.077	-7.512	0.10
	338	396.768	9.077	-7.512	0.10
	339	396.768	9.077	-7.512	0.10
	340	396.801	9.077	-7.508	0.10
	341	396.606	9.077	-7.528	0.12
	342	396.541	9.077	-7.535	0.12
	343	396,703	9.077	-7.518	0.11
	344	396.606	9.077	-7.528	0.12
	345	396.671	9,077	-7.522	0.11
	346	396 736	9.077	-7.515	0.10
	247	306 736	9.077	-7 515	0.10
	547	350.750	9.077	7 513	0.10
	348	396.768	9.077	-7.512	0.10
	349	396.736	9.077	-7.515	0.10
	350	396.768	9.077	-7.512	0.10
	351	396.736	9.077	-7.515	0.10
	352	396.606	9.077	-7.528	0.12
	353	396.541	9.077	-7.535	0.12
	354	396.606	9.077	-7.528	0.12
	355	396.736	9.077	-7.515	0.10
	356	396.768	9.077	-7.512	0.10
	357	396.801	9.077	-7.508	0.10
	358	396 801	9,077	-7.508	0.10
	350	396 933	9.077	-7 505	0.09
	350	396,033	9.077	-7 505	0.09
		330.033	3.0//	-7.00	0.05

TW1- WELL RECOVERY VS. TIME - KOLLAARD FILE 220996



Page 57 of 465

Kollaard File 220996 RECOVERY DATA TW-1

ť'	t/ť	Abs Pres	Temp	Water Level	Drawdown	Recovery
		(kPa)	(°C)	(m)	(m)	(%)
1	361	397.061	9.077	-7.482	0.07	25%
2	181.0	397.158	9.077	-7.472	0.06	35%
3	121.0	397.321	9.077	-7.455	0.04	54%
4	91.0	397.516	9.077	-7.435	0.02	75%
5	73.0	397.516	9.077	-7.435	0.02	75%
6	61.0	397.581	9.077	-7.429	0.02	82%
7	52.4	397.516	9.077	-7.435	0.02	75%
8	46.0	397.646	9.077	-7.422	0.01	89%
9	41.0	397.581	9.077	-7.429	0.02	82%
10	37.0	397.646	9.077	-7.422	0.01	89%
11	33.7	397.581	9.077	-7.429	0.02	82%
12	31.0	397.581	9.077	-7.429	0.02	82%
13	28.7	397.776	9.077	-7.409	0.00	103%



ATTACHMENT C

WATER QUALITY RESULTS

	Report Number: 1988079 Date Submitted: 2022-10-14 Date Reported: 2022-10-21 Project: 220996 COC #: 901489		sport, please do not hesitate to call (613-727-5692).				ccreditation to ISO/IEC 17025 for tests which appear on the scope of	ration, and Parks (MECP) for specific tests in drinking water (license	Rural Affairs for specific tests in agricultural soils.	urposes only. Guideline values listed on this report are provided for uired. Unless otherwise stated, measurement uncertainty is not taken
Certificate of Analysis	20	Page 1 of 7	samples. If you have any questions regarding this re			anada Inc. (Ottawa, Ontario) unless otherwise indicated.	is accredited by CALA, Canadian Association for Laboratory Ac <u>ala.ca/</u> .	is licensed by the Ontario Ministry of the Environment, Conserv	$\scriptstyle\rm is$ accredited by the Ontario Ministry of Agriculture, Food, and F	been provided by the client and is presented for informational puends consulting the official provincial or federal guideline as requdances.
rofins	Environment Testin Kollaard Associates Inc. 210 Prescott St., Box 189 Kemptville, ON KoG 1J0 Ms. Colleen Vermeersch	e to: Kollaard Associates Inc.	Colleen Vermeersch: e find attached the analytical results for your s Comments:	Emma-Dawn Ferguson 2022.10.21 15:58:23 -04'00'	ROVAL: Emma-Dawn Ferguson, Chemist	alysis is completed at Eurofins Environment Testing Car	ns Environment Testing Canada Inc. (Ottawa, Ontario) ditation. The scope is available at: <u>https://directory.ca</u>	ns Environment Testing Canada Inc. (Ottawa, Ontario) . A copy of the license is available upon request.	ns Environment Testing Canada Inc. (Ottawa, Ontario)	a note: Field data, where presented on the report, has b of use (informational purposes) only. Eurofins recomme count when determining guideline or regulatory exceed
🐝 eurofins	Client: Kollaard Associates Inc. 210 Prescott St., Box 189 Kemptville, ON K0G 1J0 Attention: Ms. Colleen Vermeersch PO#:	Invoice to: Kollaard Associates Inc.	Dear Colleen Vermeersch: Please find attached the analytical ree Report Comments:	Emma-Dawn Fergu 2022.10.21 15:58:2 -04'00'	APROVAL: Emma-Dawn Ferguso	All analysis is completed at Eurofins Environ	Eurofins Environment Testing Canada Inc. ((accreditation. The scope is available at: <u>http</u>		Eurofins Environment Testing Canada Inc. ((#2318). A copy of the license is available up	Eurofins Environment Testing Canada Inc. ((#2318). A copy of the license is available up Eurofins Environment Testing Canada Inc. ((

🐝 eurofins

Certificate of Analysis

Report Number: Date Submitted: Date Reported: Project: COC #: Environment Testing

210 Prescott St., Box 189

Kemptville, ON

K0G 1J0

Kollaard Associates Inc.

Client:

Ms. Colleen Vermeersch

Attention:

:#0d

Kollaard Associates Inc.

Invoice to:

2022-10-14 2022-10-21 1988079

220996 901489

1656461 Water	2022-10-14 TW1-6 hrs		0.159	0.508	1.0
1656460 Water	2022-10-14 TW1-3 hrs		0.153	0.260	1.0
Lab I.D. Sample Matrix	Sample Type Sampling Date Sample I.D.	Guideline			
		Units	mg/L	mg/L	mg/L
		MRL	0.020	0.100	0.1
		Analyte	N-NH3	Total Kjeldahl Nitrogen	Tannin & Lignin
		Group	Nutrients	1	Subcontract

* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

Guideline = ODWSOG

146 Colonnade Rd. Unit 8, Ottawa, ON K2E 7Y1

Page 3 of 7

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range

į	eurotins
6 0	

Certificate of Analysis

•

2022-10-14 2022-10-21 1988079

Report Number: Date Submitted: Date Reported: Project: COC #:

220996 901489

Environment Testing

Kollaard Associates Inc. Kemptville, ON K0G 1J0 Attention: PO#: Client:

210 Prescott St., Box 189 Ms. Colleen Vermeersch Kollaard Associates Inc.

Invoice to:

QC Summary

Α	nalyte	Blank	QC % Rec	QC Limits
Run No 431422 Method AMBCOLM1	Analysis/Extraction Date 20	22-10-16 A	ialyst LV	
Escherichia Coli				
Heterotrophic Pla	ate Count			
Total Coliforms				
Run No 431424 Method C SM2130B	Analysis/Extraction Date 20	22-10-15 A	alyst CK	
Turbidity		<0.1 NTU	100	70-130
Run No 431472 Method EPA 200.8	Analysis/Extraction Date 20	22-10-17 A	alyst SD	
Iron		<0.03 mg/L	107	80-120
Manganese		<0.01 mg/L	104	80-120
Run No 431474 Method C SM4500-S:	Analysis/Extraction Date 20 2-D	22-10-17 A	alyst ACG	
S2-		<0.01 mg/L	101	80-120
Run No 431497 Method SM 4110	Analysis/Extraction Date 20	22-10-18 A	nalyst AaN	
N-NO2		<0.10 mg/L	98	90-110
N-NO3		<0.10 mg/L	68	90-110

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

* = Guideline Exceedence

Guideline = ODWSOG

146 Colonnade Rd. Unit 8, Ottawa, ON K2E 7Y1

Page 4 of 7

	anera .
eurofins	
ସ୍ଥ୍ୟୁତ ବ୍ରତ୍ତ ବ୍ରତ୍ତ	

Certificate of Analysis

Environment Testing

Kollaard Associates Inc. Kemptville, ON K0G 1J0 Attention: Client: PO#:

210 Prescott St., Box 189 Ms. Colleen Vermeersch Kollaard Associates Inc.

Invoice to:

2022-10-21 220996 2022-10-14 1988079 901489 Report Number: Date Submitted: Date Reported: Project: COC #:

QC Summary

Analyte	Blank	QC % Rec	QC Limits
S04	<1 mg/L	95	90-110
Run No 431504 Analysis/Extraction Date 20 Method C SM2120C	22-10-18 Ana	lyst ACG	
Colour (True)	<2 TCU	100	90-110
Run No 431520 Analysis/Extraction Date 20 Method M SM3120B-3500C	22-10-18 Ana	lyst Z S	
Calcium	<1 mg/L	104	90-110
Potassium	<1 mg/L	110	87-113
Magnesium	<1 mg/L	102	76-124
Sodium	<1 mg/L	107	82-118
Run No 431556 Analysis/Extraction Date 20 Method SM 4110	22-10-19 Ana	Iyst AaN	
Chloride	<5 mg/L		90-110
Run No 431558 Analysis/Extraction Date 20 Method SM2320,2510,4500H/F	22-10-18 Ana	lyst ACG	
Alkalinity (CaCO3)	<5 mg/L	98	90-110
Conductivity	<5 uS/cm	100	90-110
Ľ	<0.10 mg/L	104	90-110
H		66	90-110

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range

146 Colonnade Rd. Unit 8, Ottawa, ON K2E 7Y1

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

* = Guideline Exceedence

Guideline = ODWSOG

Page 5 of 7

to eurofins

Environment Testing

Client: Kollaard Associates Inc. 210 Prescott St., Box 189 Kemptville, ON K0G 1J0 Ms. Colleen Vermeersch PO#:

Kollaard Associates Inc.

Invoice to:

Certificate of Analysis

 Report Number:
 1988079

 Date Submitted:
 2022-10-14

 Date Reported:
 2022-10-21

 Project:
 220996

 COC #:
 901489

QC Summary

Analyte	Blank	QC % Rec	QC Limits
Run No 431595 Analysis/Extraction Date 2 Method EPA 350.1	022-10-19 Ana	lyst SKH	
N-NH3	<0.020 mg/L	111	80-120
Run No 431627 Analysis/Extraction Date 2 Method C SM5310C	022-10-18 Ana	lyst ACG	
DOC	<0.5 mg/L	102	84-116
Run No 431628 Analysis/Extraction Date 2 Method EPA 351.2	022-10-19 Ana	lyst ML	
Total Kjeldahl Nitrogen	<0.100 mg/L	110	70-130
Run No 431652 Analysis/Extraction Date 2 Method C SM2340B	022-10-20 Ana	lyst AET	
Hardness as CaCO3			
Ion Balance			
TDS (COND - CALC)			
Run No 431683 Analysis/Extraction Date 2 Method SUBCONTRACT-A	022-10-19 Ana	lyst AET	
Tannin & Lignin	<0.10 mg/L	102	
Run No 431738 Analysis/Extraction Date 2 Method SM5530D/EPA420.2	022-10-21 Ana	lyst IP	

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

* = Guideline Exceedence

Guideline = ODWSOG

146 Colonnade Rd. Unit 8, Ottawa, ON K2E 7Y1

Page 6 of 7

	t and the second
ţ	urotins
6	

Environment Testing

210 Prescott St., Box 189

Kemptville, ON K0G 1J0

Kollaard Associates Inc.

Client:

Ms. Colleen Vermeersch

Attention:

PO#:

Kollaard Associates Inc.

Invoice to:

Certificate of Analysis

2022-10-14 2022-10-21 1988079 220996 901489 Report Number: Date Submitted: Date Reported: Project: COC #:

QC Summary

Analyte	Blank	QC % Rec	QC Limits
Phenois	<0.001 mg/L	104	50-120

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

Guideline = ODWSOG

* = Guideline Exceedence

146 Colonnade Rd. Unit 8, Ottawa, ON K2E 7Y1

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range

Ryznar Stability Index

$RSI = 2(pH_s) - pH$

RSI << 6 → the scale tendency increases as the index decreases RSI >> 7 → the calcium carbonate formation probably does not lead to a protective corrosion inhibitor film RSI >> 8 → mild steel corrosion becomes an increasing problem

Langelier Saturation Index

$LSI = pH - pH_s$

If LSI is negative \rightarrow no potential to scale, the water will dissolve CaCO₃

If LSI is positive \rightarrow scale can form and CaCO₃ precipitation may occur

If LSI is close to zero \rightarrow borderline scale potential, water quality or temperature change or evaporation could change the index

where pH measured from sample

pH_s = pH at saturation in calcite or calcium carbonate

$$pH_{s} = (9.3 + A + B) - (C + D)$$

$$A = \frac{\log_{10}[TDS] - 1}{10}$$

$$B = -13.12 \times \log_{10}(^{\circ}C + 273) + 34.55$$

$$C = \log_{10}[Ca^{2+}asCaCO_{3}] - 0.4$$

$$D = \log_{10}[alkalinityasCaCO_{3}]$$

pH hardness [mg/l as $CaCo_3$] Alkalinity [mg/l as $CaCo_3$] total dissolved solids [mg/l] temperature (°C) $\rightarrow \rightarrow$ RSI

 $\rightarrow \rightarrow$ LSI

TW1-3hr	TW1-6hr
7.45	7.55
417	420
304	307
607	610
11.3	12.1
6.81	6.67
0.32	0.44

DEVELOPMENT AGREEMENT BETWEEN EDWARD AND LILA BRONISZESKI AND THE TOWNSHIP OF EDWARDSBUGH/CARDINAL

SCHEDULE "D"

SITE SURVEY 15R12398

Page 67 of 465



(PER REGISTERED PLAN 40)

		S	CHEDUL	E		
	3	PART LOT ALL OF 5	PLAN	PIN	AREA	-
		PART OF BRUCE STREET PART OF 5, NORTH	40	ALL OF 68141-0313(LT)	0.099 ha	PLAN 15R-12398
		2 SIDE CHARLES STREET PART OF BRUCE STREET			0.094 ha	Received and deposited
						February 8th 2024
						Mary Beth Quellette
						Penresentative for the
						Land Registrar for the Land Titles Division of Grenville (No.15)
					LOT 5	F SURVEY OF
J STREET					SOUTH S PART NORTH S PART REGIST FORMER TOWNSH COUNTY SCALF:	SIDE OF DAVID STREET, OF LOT 5 SIDE OF CHARLES STREET OF BRUCE STREET TERED PLAN 40 LY THE VILLAGE OF SPENCERVILLE HIP OF EDWARDSBURGH/CARDINAL OF GRENVILLE 1:200
	1				0 1 2 3	4 5 10 15
					THE INTEND IN WIDTH B A SCALE C	DED PLOT SIZE OF THIS PLAN IS 914MM BY 457MM IN HEIGHT WHEN PLOTTED AT DF 1:200
		(PER REOS/ER			BEARING BEARINGS A POINTS A A ZONE 18, N FOR BEARIN APPLIED:	S NOTES ARE UTM GRID, DERIVED FROM OBSERVED REFERENCE IND B, BY REAL TIME NETWORK OBSERVATIONS, UTM AD83(CSRS)(2010). IG COMPARISONS, THE FOLLOWING ROTATIONS WERE P2 - 00°24'00" CLOCKWISE P3 - 00°22'50" CLOCKWISE P5 - 00°21'45" CLOCKWISE P6, P7 - 00°24'30" CLOCKWISE
	STREET				DISTANC DISTANCES CONVERTED DISTANCES MULTIPLYINC	CE NOTES — METRIC and coordinates are in metres and can be to feet by dividing by 0.3048. are ground and can be converted to grid by g by the combined scale factor of 0.9996128.
					SURVEY(1 certify t	OR'S CERTIFICATE
	0865				1. THIS SUR WITH THE TITLES AG	RVEY AND PLAN ARE CORRECT AND IN ACCORDANCE SURVEYS ACT, THE SURVEYORS ACT, THE LAND CT AND THE REGULATIONS MADE UNDER THEM.
					2. THE SUR	VEY WAS COMPLETED ON JANUARY 17, 2024.
	LEGE □ ■	LINU DENOTES PLANTED MONUM DENOTES FOUND MONUMFI	1ENT NT		FEBR	RUARY 6, 2024
	SIB SSIB IB CM	DENOTES STANDARD IRON DENOTES SHORT STANDAR DENOTES IRON BAR DENOTES CONCRETE MONU DENOTES CUIT CROSS	bar d iron e jment	BAR	DATE THIS PLAN SUBMISSIO	V RONT M. JASON, O.L.S. N OF SURVEY RELATES TO AOLS PLAN ON FORM NUMBER V-68543
1	CP PB IP	DENOTES CONCRETE PIN DENOTES PLASTIC BAR DENOTES IRON PIPF		F	OBSERVED REFE	INTEGRATION DATA ERENCE POINTS DERIVED FROM GPS OBSERVATIONS USING A REAL
VIT ACC		DENOTES IRON PIPE DENOTES ROUND DENOTES WITNESS DENOTES ACCEPTED	TIME NETWORK AND ARE REFERRED TO UTM ZONE 18 (75' WEST LONGITUDE) NAD83(CSRS)(2010).			
/ /	MEAS INST x-x	DENOTES MEASURED DENOTES INSTRUMENT DENOTES FENCE		-	POINT II	D NORTHING EASTING 4965357.02 456464.34
	P1 P2 P3	DENOTES REGISTERED PLA DENOTES PLAN 15R–9233 DENOTES PLAN 15R–9446	N 40	-	B CAUTION: COORDINATES (CANNOT, IN THEMSELVES, BE USED TO RE-ESTABLISH CORNERS OR BOUNDARIES SHOWN ON THIS PLAN
	P4 P5 P6	DENOTES PLAN 15R-1222 DENOTES PLAN 15R-6224 DENOTES PLAN OF SURVE	6 Y BY (14	.25)		
	P7	DATED OCTOBER DENOTES PLAN OF SURVE DATED JUNE 3	14, 199 Y BY (16 1993	2 41)	-	-{Â}→IBW
	FN1 FN2	DENOTES FIELD NOTES BY DATED JANUARY DENOTES FIELD NOTES BY	RON M. 9, 1996 RON M	JASON O.L.S.		SURVEYORS
	ALL R	DATED APRIL 16	, 2019 REE WITH	CITED PLANS	IBV	WSURVEYORS.COM 1.800.667.0696
	UNLES	S OTHERWISE NOTED.			FILE NAME: A-	KU UKAWN BY: BM CHECKED BY: RJ PLOT DATE: * 045746-V2 copies available at LandSurveyRecords.com



TOWNSHIP OF EDWARDSBURGH CARDINAL ACTION ITEM

Committee: Committee of the Whole – Community Development

Date: October 7, 2024

Department: Community Development

Topic: Subdivision Agreement, Lockmaster Meadow Subdivision (Edwardsburgh Developments Inc.)

Purpose: To review a draft subdivision agreement.

Background: The subject lands, referred to as the Lockmaster Meadow Subdivision, are approximately 11.1 ha in land area, located on the west side of Shanly Road (County Road No. 22) and south of the CN Railway within the Village of Cardinal. The lands are currently undeveloped and are surrounded by rural properties towards the north and west and residential properties to the east and south.



Excerpt of Draft Plan of Subdivision S-1; February 6, 2024

The draft plan includes 95 lots for single detached dwellings, one stormwater/open space block, one block for parkland purposes, a block for a future road to the west, one block for a pumping station, and a treed earth berm instead of the barrier to mitigate noise from the railway. The subdivision includes three new public streets and will be accessed from two new street entrances on Shanly Road. All residential lots will be developed on full municipal services.

The draft plan approval includes 62 conditions to be cleared by the developer. The conditions are made by the Counties through recommendations from the Township and other agencies. The conditions relate to topics such as parkland dedication, zoning, servicing, water and sewer works, stormwater management, fish habitat, noise attenuation, landscaping and streetscaping, roads, traffic, and services such as hydro and gas.

Condition 7 of draft plan approval requires that the Owner enter into a subdivision agreement between the Owner and the Township to the satisfaction of the Township. A draft agreement is attached to this report. It has been reviewed by our lawyer and insurer and their recommendations have been incorporated. The Owner has received a copy of the draft agreement and staff have requested an updated development schedule.

Detailed designs and reports have been provided to the Township and have been reviewed by staff and peer reviewers on our behalf. The detailed designs and reports are included in the subdivision agreement, which requires the subdivision works to be completed in accordance with the designs.

The Township is asked to provide notice to the Counties that conditions 2 to 58 of draft approval have been satisfied. Some of these conditions relate to requirements of other agencies. The Township has received written notice from South Nation Conservation and Canada Post that they are satisfied with the designs and wording in the subdivision agreement. Staff have asked the developer to provide confirmation from Hydro One and Enbridge that their conditions are satisfied before we provide this clearance to the Counties.

Policy Implications: The Planning Act allows a municipality to enter into a subdivision agreement and enforce the provisions against the owner and subsequent owners. The agreement will be registered against the lands so that it is available to future owners.

Section 53(26) of the *Planning Act*, R.S.O., 1990, Chapter P.13.

A municipality or approval authority, or both, may enter into agreements imposed as a condition to the approval of a plan of subdivision and the agreements may be registered against the land to which it applies and the municipality or the approval authority, as the case may be, is entitled to enforce the provisions of it against the owner and, subject to the Registry Act and the Land Titles Act, any and all subsequent owners of the land. 1994, c. 23, s. 30.

The United Counties of Leeds and Grenville is the approval authority for plans of subdivision. Final approval is given when all conditions of draft approval have been met. Once final approval has been granted, the plan of subdivision is registered and lots may be sold individually.

Strategic Plan Implications: The subdivision agreement is supported by the Township's Strategic Plan. The agreement ensures that infrastructure will be

constructed to support a thriving, resilient and well-connected community, while supporting growth and economic development by increasing housing availability.

Financial Considerations: The Owner addressed Council on July 22, requesting that the Township consider reduced or alternative financial securities. An estimated cost of \$3,965,054.74 (including HST) for the subdivision works were provided by the developer and included in Schedule D.

The agreement includes financial requirements in section 23, further detailed in Schedule E to include a deposit of \$2 million, plus 2 lots to be held as securities to guarantee the construction and installation of the Works withing the agreement. In the event that some Works or some part of the Works are constructed by a Municipal Official pursuant to this Agreement, or in the event that the Owner fails to pay the cost of any of the Works, or in the event of other default of this Agreement, the Municipality may draw upon the securities to correct any defect prior to assuming the Works in accordance with this Agreement.

Recommendation: That Committee recommend that Council enter into a subdivision agreement with Edwardsburgh Developments Inc., as attached, once a development schedule has been received and approved by staff.

Community Development Coordinator


Applicant:Edwardsburgh Developments Inc.File:07-T-10005 (Lockmaster's Meadow)Municipality:Township of Edwardsburgh CardinalLocation:Lot 7, Con. 1, County Road 22

Date of Original Decision: April 24, 2013 Date of Revised Decision: February 24, 2022 Date of Notice: February 25, 2022 Last Date of Appeal: March 17, 2022 Lapsing Date: February 25, 2025

Conditions of Draft Approval

- 1. That this approval applies to the Draft Plan of Subdivision in Lot 7, Concession 1, Township of Edwardsburgh Cardinal, County of Grenville, prepared by Advance Engineering dated December 7, 2021 which shows a total of 95 residential lots, Block A for open space, a safety fence, a stormwater retention pond, noise attenuation barrier and safety barrier, Block B for a sanitary pumping station, Blocks C, D, and Da for 0.3 m reserves, Block E for future road purposes, Block F for parkland, Block G for future road purposes and Block H for a walkway and utility corridor.
- 2. That a minimum of 10 metres from both sides of the centre line of the Streets shown on the draft plan shall be shown and dedicated as public highways on the final plan.
- 3. That Block E and Block G, as shown on the draft plan, shall be conveyed to and held in trust, by the Township of Edwardsburgh Cardinal until the extension of the road allowance.
- 4. That Block A, as shown on the draft plan, shall be conveyed to the Township of Edwardsburgh Cardinal subject to the terms and conditions of the Township.
- 5. That the streets shall be named to the satisfaction of the Township.
- 6. The subdivision shall be built in two phases. Phase 1 consists of Block A including the safety fence, stormwater management pond, noise barrier and safety barrier, Street A, Street B south-east of Street A, a total of fifty-nine (59) residential lots, being lots 9-37, 57-61 and 71-95, including Blocks C, D and Da as 0.3 m reserves, Block E as a future roadway block, Block F as parkland dedication, and Block H as a walkway and utility corridor, as shown on the draft plan. Phase 2 consists of Street C, the remainder of Street B, the remaining thirty-six (36) units, being lots 1-8, 38-56 and 62-70, Block B for a sanitary pumping station and Block G as a future roadway connection.
- 7. That the Owner enter into a subdivision agreement between the Owner and the Township to the satisfaction of the Township and that the Owner covenants and agrees that the executed subdivision agreement between the Owner and the Municipality shall be registered against the lands to which it applies once the plan of subdivision has been registered. It is noted that the subdivision agreement



will be prepared when the final design plans (i.e. servicing, stormwater management, road design, berm design, etc.) have been reviewed and accepted and/or are in the final stages of review and acceptance by the Township.

<u>Parkland</u>

- 8. That Block F, as shown on the draft plan, shall be conveyed to the Township of Edwardsburgh Cardinal as part of Parkland Dedication subject to the terms and conditions of the Township.
- 9. That the developer, as part of Parkland Dedication, convey a cash-in-lieu payment to the Township.
- 10. All Owner obligations associated with Block F must be completed in Phase 1 to the satisfaction of the Township of Edwardsburgh Cardinal.
- 11. It is the responsibility of the Owner to fill with clean earth fill, compact and level Block F accordingly, providing for positive surface drainage to the satisfaction of the Township of Edwardsburgh Cardinal.
- 12. The Owner shall grade areas of parkland where necessary to the satisfaction of the Township of Edwardsburgh Cardinal, so as to provide a uniform surface, free of debris, necessary to establish a safe clean and maintainable surface. Block F shall be graded in accordance with the approved Grading Plan for the Plan of Subdivision. No storage of building materials, including granular or topsoil will be permitted on Block F.

<u>Zoning</u>

13. That prior to final approval by the Counties, the Counties is to be advised by the Township of Edwardsburgh Cardinal that this proposed subdivision conforms to the zoning by-law in effect and that any zoning issues identified are appropriately satisfied through an amendment to the Township Zoning By-Law. It is noted that the Township is currently preparing a new Zoning By-Law. To clear this condition, a plan noting lot area and lot frontage for each proposed lot will be required based on the definitions of the Zoning By-law in effect at the time of final approval.

Servicing - General

- 14. That the Owner agrees in writing to satisfy all the requirements, financial and otherwise, of the Township of Edwardsburgh Cardinal concerning the provision of roads, installation of services, drainage and other relevant features (such as lighting, etc.).
- 15. That such easements as may be required for utility or drainage purposes shall be granted to the appropriate authority.



- 16. The Owner acknowledges their responsibility to obtain all of the required approvals for the pumping station to be constructed on Block B.
- 17. Notwithstanding what may be illustrated on the approved draft plan, that the final subdivision agreement plans show and subdivision agreement contain a clause whereby the Owner agrees to provide two lifts of asphalt, concrete curbs and gutters, in accordance with OPSS, on Streets A, B and C to the satisfaction of the Township of Edwardsburgh Cardinal.
- 18. That the plans show and subdivision agreement contain a clause whereby the Owner agrees to provide underground electrical servicing to the satisfaction of the Township of Edwardsburgh Cardinal.
- 19. That the subdivision agreement include terms satisfactory to the Township indicating Block H, as shown on the draft plan, shall be conveyed to the Township upon Township acceptance of the underground services, walkway, landscaping and fencing.

Water and Sewer Works

- 20. The Owner shall submit detailed municipal servicing plans, prepared by a Civil Engineer licensed in the Province of Ontario, to the Township of Edwardsburgh Cardinal and the United Counties of Leeds and Grenville (Counties'). All water and sewer works to be located on the County Road right-of-way shall be subject to approval from the Counties' Roads Department at the time of detailed design.
- 21. The Owner acknowledges and agrees that building permits will not be issued for the development of individual Lots in Phase 2 until the pumping station has been installed and placed in service to the satisfaction of the Township of Edwardsburgh Cardinal.
- 22. The Owner shall design and construct all necessary watermains and the details of services and meters to the satisfaction of the Township of Edwardsburgh Cardinal. The Owner acknowledges that the servicing plan shall include a watermain stub to Block E and Block G. The Owner shall pay all related costs, including the cost of connection, inspection and sterilization by Township personnel, as well as the supply and installation of water meters by the Township.
- 23. Upon completion of the installation of all watermains, hydrants and water services, the Owner shall provide the Township with mylar(s) of the "as-built" plan(s), certified under seal by a Professional Engineer, showing the location of the watermains, hydrants and services. Electronic files are also required in order for them to be added to the Township GIS system. The United Counties require digital files in .dwg and pdf format.



Stormwater Management

- 24. That prior to final plan approval, the Owner shall prepare a final stormwater site management plan and lot grade and drainage plan which shall be consistent with the report entitled "Preliminary Stormwater Management Report" prepared by Eastern Engineering Group Inc. signed July 13, 2010. The final stormwater site management plan shall address the South Nation Conservation review comments dated October 12, 2010. The Plan shall describe how stormwater management is to be implemented in accordance with the current Stormwater Management Best Management Practices and should address both water quality and quantity concerns. Models, assumptions and calculations of pre-and post-development runoff are to be included in this submission. The final report shall be prepared to the satisfaction of the Township of Edwardsburgh Cardinal, South Nation Conservation and the United Counties of Leeds and Grenville. Consideration shall be had to condition 41.
- 25. Post-development stormwater flows at the County Road culvert shall equal pre-development flows.
- 26. That prior to final plan approval, the Owner shall prepare and submit a Sediment and Erosion Control Plan, appropriate to the site conditions, prior to undertaking any site alterations (filling, grading, removal of vegetation, etc.) and indicate how it is to be implemented during all phases of the site preparation and construction in accordance with the current Best Management Practices for Erosion and Sediment Control to the satisfaction of the Township of Edwardsburgh Cardinal and South Nation Conservation.
- 27. That the Subdivision Agreement contain a clause whereby the Owner agrees that upon completion of all stormwater works, to provide certification to the Township of Edwardsburgh Cardinal and South Nation Conservation, through a professional engineer, that all measures have been implemented in conformity with the approved stormwater site management plan.
- 28. That the Subdivision Agreement contains a clause whereby prior to the commencement of construction of any phase of the subdivision (roads, utilities and off-site works, etc.), the Owner agrees to:
 - a. have a professional engineer prepare an erosion and sediment control plan appropriate for site conditions in accordance with the current best management practices;
 - b. have this plan reviewed and approved by the Township of Edwardsburgh Cardinal and South Nation Conservation;
 - c. monitor the effectiveness of and maintain the erosion and sedimentation control works as necessary, and;
 - d. provide certification to the Township of Edwardsburgh Cardinal and South Nation Conservation through a professional engineer that the plan has been implemented.



Fisheries

- 29. The Owner acknowledges that the unnamed watercourse is considered either direct or indirect Fish Habitat as per Section 35 of the *Fisheries Act*.
- 30. The Owner shall establish a 30 metre "no touch/no development" setback of the unnamed watercourse, on both sides, measured from the top of the average annual highwater mark. The final approved plan of subdivision shall clearly show this setback. The berm required under condition 32.a. shall be located outside of this 30 metre setback. Any deviation from this setback shall be to the satisfaction of the Township of Edwardsburgh Cardinal and South Nation Conservation.
- 31. The subdivision agreement with the Township will indicate that in accordance with Section 35 of the *Fisheries Act*, the Harmful Alteration, Disruption or Destruction (HADD) of fish habitat is prohibited. The impacts that any such works may have on a fish habitat, whether directly adjacent to the site or downstream, may require approval of the Department of Fisheries and Oceans Canada.

Noise Attenuation and Warnings

- 32. That the subdivision agreement between the Owner and the Township contain the following provisions with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the Owner agrees to install a noise barrier for Phase 1 in accordance with subsection a. below and further that for Phase 2 for lots 1, 46-52 and 66-70 inclusive that the noise attenuation and warning requirements be in accordance with subsections b. to d. inclusive:
 - a. A treed earth berm for noise attenuation purposes shall be constructed as part of Phase 1. Notwithstanding what may be illustrated in the approved draft plan, the berm shall be designed and constructed to the satisfaction of the Township of Edwardsburgh Cardinal. No portion of the noise attenuation berm shall be located on the County Road right-of-way.

Note: This berm may be designed in such a way as to also meet condition 37.

- b. All units shall be equipped with forced air heating with central air conditioning.
- c. That Warning Clause Type D, in accordance with the following, shall be included on all Lease and Purchase and Sale Agreements.

Type D: "This dwelling has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the Municipality's and the Ministry of Environment's noise criteria."



- d. Bedroom windows facing north will require a minimum Sound Transmission Class (STC), being outdoor noise levels minus the targeted indoor noise level, of 26. Living room windows facing north will require a minimum STC of 21. Exterior wall components of north facades will require a minimum STC of 45, which will be achieved with brick cladding or an acoustical equivalent according to NRC test data. Detailed STC calculations will be completed prior to building permit application for each unit type and submitted to the Township with the building permit application.
- 33. That the subdivision agreement between the Owner and the Township contain provisions with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the owner agrees for Phase 2 for Lots 46-52 inclusive that Warning Clause Type A, as follows, will be included in all Lease and Purchase and Sale Agreements. This provision is in addition to those noise attenuation and warning requirements detailed in condition 32:

Type A: "Purchasers/tenants are advised that sound levels due to increasing rail traffic may occasionally interfere with some outdoor activities as the sound levels may exceed the sound level limits of the Township and the Ministry of the Environment, Conservation and Parks."

- 34. That the subdivision agreement between the Owner and the Township contain the following provision with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the Owner agrees where structural mitigation measures are required the Owner shall provide, prior to final building inspection, certification to the Township of Edwardsburgh Cardinal, through a Professional Engineer, that the noise control measures have been implemented in accordance with the approved study.
- 35. That the subdivision agreement between the Owner and the Township contain provisions with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the Owner agrees for all lots that rooftop HVAC equipment shall be prohibited.
- 36. The Owners acknowledges and agrees that building permits will not be issued for the development of individual lots in Phase 2 until the treed earth berm has been constructed to the satisfaction of the Township of Edwardsburgh Cardinal.

<u>CN Rail</u>

For Phase 1, conditions 37 and 42 shall apply:

37. A safety berm parallel to the railway rights-of-way with returns at the ends shall be installed between any publically accessible open space lands and the railway. The berm shall be 2.5 metres above



grade at the property line, with side slopes not steeper than 2.5 to 1. The location may be moved and height of the berm may be reduced proportionally to the distance separating the designated open space area from the north property line. Past the 120m setback from the property line there will be no requirements for a berm. For example, if the park area accessible to the public is to be located at 60 metres from the CN right of way, the required berm should be 1.25 metres tall. The safety berm and its characteristics and the limits of the park area accessible to the public shall be appropriately illustrated on the plan.

Note: This berm may be designed in such a way as to also meet condition 32.

For Phase 2, conditions 38 to 44 shall apply:

- 38. The Owner shall install and maintain a chain link fence of minimum 1.83 metre height along the mutual property line (being the north-west lot line of Block A). The safety fence and its characteristics must be illustrated in the plan.
- 39. Since the development is partially located within 300 metres of the CN main line, the Owner shall engage a consultant to undertake an analysis of noise. Subject to the review of the noise report, the Railway may consider other measures recommended by an approved Noise Consultant. CN will review the Noise report and will determine if mitigation measures will be required to be implemented by the Owner.
- 40. The following clause should be inserted in all development agreements, offers to purchase, and agreements of Purchase and Sale or Lease of each dwelling unit within 300 m of the railway right-of-way:

"Warning: Canadian National Railway Company or its assigns or successors in interest has or have a rights-of-way within 300 metres from the land the subject hereof. There may be alterations to or expansions of the railway facilities on such rights-of-way in the future including the possibility that the railway or its assigns or successors as aforesaid may expand its operations, which expansion may affect the living environment of the residents in the vicinity, notwithstanding the inclusion of any noise and vibration attenuating measures in the design of the development and individual dwelling(s). CNR will not be responsible for any complaints or claims arising from use of such facilities and/or operations on, over or under the aforesaid rights-of-way."

41. Any proposed alterations to the existing drainage pattern affecting railway property must receive prior concurrence from the Railway and be substantiated by a drainage report to the satisfaction of the Railway. The drainage plan indicates that all storm waters from the developments will be



directed to a pond and then into an existing ditch flowing away from CN property. However, CN will require a technical memo prepared by the project engineer explaining the design concept and confirming that all storm waters will be directed away from the CN right of way.

- 42. The Owner shall through restrictive covenants to be registered on title and all agreements of purchase and sale or lease provide notice to the public that the safety berm, fencing and noise isolation measures implemented are not to be tampered with or altered and further that the Owner shall have sole responsibility for and shall maintain these measures to the satisfaction of CN.
- 43. The Owner shall enter into an Agreement with CN stipulating how CN's concerns will be resolved and will pay CN's reasonable costs in preparing and negotiating the agreement.
- 44. The Owner shall be required to grant CN an environmental easement for operational noise and vibration emissions, registered against the subject property in favour of CN (within 300 metres from CN right of way).

Landscaping/Streetscaping

45. The Owner agrees to provide additional planting where necessary to provide a buffer between the existing properties and Lots 13-20 inclusive on the draft plan of subdivision, to the satisfaction of the Township of Edwardsburgh Cardinal.

Street Lighting

- 46. The Owner shall design and construct all necessary street lighting, interior and exterior to the subdivision, to the satisfaction of the Township of Edwardsburgh Cardinal. The Owner shall pay all related costs, including the cost of connection and inspection by Township personnel and/or the hydro authority.
- 47. The Owner agrees to provide streetlights on Street A and C, where the streets intersect with the Counties Road. Lighting shall be designed and installed under the guidance, requirements and to the satisfaction of the Counties. The Owner shall pay all related costs.

Grass Cutting, Ditch Maintenance and Schools

48. That the subdivision agreement between the Owner and the municipality and the Offers of Purchase and Sale Agreements and Deeds contain the following provisions with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the Owner agrees:



- a. That the general maintenance and upkeep of all ditches and drains within the subdivision be the responsibility of the property owner.
- b. That grass cutting along the roadside within the subdivision be the responsibility of the property owner.
- 49. That the subdivision agreement between the Owner and the Township contain a provision that Agreements of Purchase and Sale indicate that it will not be possible to guarantee which school children residing in this subdivision may attend, and that transportation will be provided in accordance with the policy of the governing school board.

County Road Access and Widening

- 50. The Owner covenants and agrees that the subdivision agreement will contain clauses whereby the Owner covenants and agrees:
 - a. that they will design and construct the intersection of all roads within the Plan of Subdivision that intersect the County Road to the satisfaction of the United Counties of Leeds and Grenville.
 - b. to pay all expenses including those for drawing preparation, utility relocations, fees, security, road work, construction supervision, engineering and administrative costs for the modification of any intersection.
 - c. to obtain an entrance permit and/or enter into an agreement with the United Counties of Leeds and Grenville, to the satisfaction of the United Counties of Leeds and Grenville respecting the conditions of accessing the Counties road/road allowance prior to undertaking any work within the Counties road allowance.
 - d. to transfer Blocks C, D and Da to the United Counties of Leeds and Grenville at the Owner's cost for the purpose of a reserve to restrict access onto the Counties road. The lands shall be free of any encumbrances.
- 51. Road widening shall be deeded to the United Counties of Leeds and Grenville along the lot frontage which abuts County Road 22 as per Section 6.2.2 (d) of the Counties Official Plan. The road allowance should be 26.2 metres. Should sufficient allowance exist, a letter from a surveyor would meet the Counties' needs. Should the allowance not meet minimum desired right-of-way, an appropriate dedication (1/2 the desired allowance width, measured from the centerline of the current road) will be required to be incorporated into the final plan. All lands transferred for road purposes shall be free and clear from any encumbrances.



Hydro Installations

- 52. The Owner shall request a connection cost assessment from Hydro One and from Rideau St. Lawrence Distribution Inc. Should the cost assessment result in Hydro One supporting a Service Area Amendment, the Owner shall arrange for Rideau St. Lawrence Distribution Inc. to be the Hydro Electric Commission (i.e., provider).
- 53. The Owner shall arrange with the relevant Hydro Electric Commission for the installation of such services to the subdivision and for the provision of easements with respect to such installations. The Owner shall pay any cost involved in relocating any existing services required by the construction of works in the subdivision.
- 54. That prior to final plan approval by the Counties, the Owner shall enter into a Servicing Agreement with the relevant Hydro Electric Commission.

Enbridge Gas

- 55. That the subdivision agreement between the Owner and the Township contain the following to the satisfaction of the Township:
 - a. The developer is responsible for preparing a composite utility plan that allows for the safe installation of all utilities, including required separation between utilities;
 - b. Streets are to be constructed in accordance with composite utility plans previously submitted and approved by all utilities;
 - c. The developer shall grade all streets to final elevation prior to the installation of the gas lines and provide Enbridge Gas Distribution Inc. with the necessary field survey information for the installation of the gas lines; and
 - d. It is understood that the natural gas distribution system will be installed within the proposed road allowance. In the event this is not possible, easements will be provided at no cost to Enbridge Gas Distribution Inc.

Canada Post

56. The Owner shall consult with Canada Post to determine the locations of lay-bys for postal boxes outside of the County road allowance. The location of lay-bys, as agreed between the Owner and Canada Post, will be subject to the final approval of the Township.



Subdivision Agreement

57. That the subdivision agreement between the Owner and the Township contain wording acceptable to South Nation Conservation.

Traffic Impact Study

58. That prior to final approval by the Counties', the Owner shall submit a Traffic Impact Study addressing the impact of traffic from this development. The Traffic Impact Study shall be written to the satisfaction of the Township of Edwardsburgh Cardinal.

Clearance of Conditions

- 59. That prior to registration of the final plan, the United Counties of Leeds and Grenville is to be advised by the Township of Edwardsburgh Cardinal that Conditions 2-58, inclusive, have been satisfied.
- 60. That prior to registration of the final plan, the United Counties of Leeds and Grenville is to be advised by South Nation Conservation that Conditions 24, 26-28 inclusive, 30 and 57 have been satisfied.
- 61. That prior to registration of the final plan, the United Counties of Leeds and Grenville is to be advised by CN Rail that Conditions 37-44 have been satisfied.
- 62. That prior to final approval, the United Counties' subdivision approval authority is to be advised by the United Counties' Public Works Department that Conditions 20, 24, 25, 47, 50 and 51 have been satisfied.

NOTES TO DRAFT APPROVAL

- 1. It is the applicant's responsibility to fulfill the conditions of draft approval and to ensure that the required clearance letters are forwarded by the appropriate agencies to the United Counties of Leeds and Grenville and copied to the Township of Edwardsburgh Cardinal guoting File No. **07-T-10005**.
- 2. It is suggested that the Township register the subdivision agreement as provided by Section 51(26) of the Planning Act, R.S.O. 1990 against the land to which it applies, as notice to prospective purchasers.
- 3. All measurements in subdivision final plans must be presented in metric units.



- 4. If final approval is not given by the lapsing date, and no extensions have been granted pursuant to Section 51(33), then draft approval shall lapse pursuant to Section 51(32) of the *Planning Act*.
- 5. It is the responsibility of the Owner to request an extension of the draft plan approval. A request for extension should be made at least 60 days before the draft plan approval lapses. No extension can be given after the lapsing date. The request should include the reasons for requesting the extension, progress/status and the applicable fees.

Clearances Are Required From the Following Agencies

Township of Edwardsburgh Cardinal 18 Centre Street, P.O. Box 129 Spencerville, ON, K0E 1X0

South Nation Conservation 38 Victoria Street, P.O. Box 29 Finch, ON, KOC 1K0

Director of Public Works United Counties of Leeds and Grenville 25 Central Ave. W., Suite 100 Brockville, ON, K6V 4N6

CN Business Development and Real estate 1 Administration Road Concord, ON, L4K 1B9 c/o WSP proximity@cn.ca T : 1-438-459-9190 1600, René-Lévesque Ouest, 11e étage

1600, René-Lévesque Ouest, 11e éta Montreal (Quebec) H3H 1P9 CANADA



A GUIDE TO THE APPROVAL PROCESS FOR PLANS OF SUBDIVISION

NOTE:	This guide has been prepared for information purposes only. Please refer to the Planning Act of Ontario for the complete legislative requirements for plans of subdivision.			
Approval Authority	1.	The Corporation of the United Counties of Leeds and Grenville is the approval authority for plans of subdivision in the municipalities that make up the United Counties. This authority was assigned to The United Counties of Leeds and Grenville in September 1998 by the Province of Ontario.		
What is a plan of subdivision?	2.	A registered plan of subdivision is a legal document that shows, (1) the exact surveyed boundaries and dimensions of lots on which houses or buildings are to be built; (2) the location, width and names of streets; and (3) the sites of any schools or parks. A registered plan of subdivision creates new, separate parcels of land and it can be used legally for the sale of lots.		
What is the process?	3.	Refer to the Subdivision Process Flow Chart for an overview of the basic subdivision process.		
Who makes the decision?	4.	The Manager of Planning Services makes the decision on whether to approve or refuse an application, and on what conditions to attach to any draft approval with input from the municipality and circulated agencies. A Committee of Council reviews any disputed application and may render the decision. Where an application is not disputed, the authority to approve the application is delegated to the Manager of Planning Services.		
Consultation	5.	The Planning Act sets out a number of public bodies such as the local municipality, conservation authorities, utility companies, the school boards, etc., that are to be consulted regarding a proposed plan of subdivision. Also, a public meeting to receive comments on a proposed plan of subdivision must be held, normally by the affected local municipality by request of the Counties.		
Evaluation	6.	 The Counties evaluates the merits of the proposed plan of subdivision against criteria such as: whether the subdivision is premature (e.g. if municipal services such as water, sewer or roads are not available); conformity with the Counties Official Plan and the local official plan; compliance with the zoning by-law; compatibility with adjacent uses of land; suitability of the land for the proposed purpose including size and shape of lots; adequacy of access and sewer and water services; protection from flooding and conservation of natural resources; consistency with the Provincial Policy Statement. 		
Draft Approval	7.	The Counties considers the application, the comments received and the results of its evaluation. If an application is draft approved, there will be conditions to be met in order to obtain final approval. The conditions may include but are not limited to a parkland dedication, a rezoning, and a subdivision agreement between the proponent and the local municipality. When a notice of decision is given, a 20-day appeal period follows for certain parties.		
		Draft approval amounts to approval in principle of the subdivision, subject to the proponent meeting all conditions of draft approval.		

Appeals	8.	 The <u>applicant</u> may make a motion to the Ontario Land Tribunal (OLT) for directions: (i) within 30 days of receiving a notice of an incomplete application from the approval authority [Planning Act, Section 51(19.2)]; (ii) any time after 30 days of submitting an application, if the approval authority has not provided a notice of complete or incomplete application [Planning Act, Section 51(19.3)]. The <u>applicant</u> may appeal to the OLT, if the approval authority fails to make a decision within 120 days of receipt of a complete application [Planning Act, Section 51(34)]. Further appeal opportunities to the OLT, as listed below, exist for certain parties, as listed below: <i>Appeal Opportunities</i> Not later than 20 days after notice of a decision on draft approval, the following may be appealed: the decision, the lapsing provisions or any of the conditions [Planning Act, Section 51(39)]: Any time before final approval of the plan of subdivision, any conditions may be appealed [Planning Act, Section 51(43)] Any changes of conditions [Planning Act, Section 51(48)] <i>Appeal Parties</i> a public body who made oral submissions at a public meeting or written submissions prior to a decision being made by the approval authority; a person listed in subsection 48.3 of the Planning Act (generally persons representing utility companies, propane handlers, railway or telecommunication infrastructure; the Minister; the municipality in which the proposed plan of subdivision is located.
		Appeals must be filed with the United Counties of Leeds and Grenville and must include the fee required by the Ontario Land Tribunal. Currently the fee is \$1,100.00. An Appellant may request a reduction of the filing fee to \$400, if the Appellant is a private citizen or eligible community group. The request for a reduction in the fee must be made at the time of filing the appeal using the appropriate form.
When to Register the Plan?	9.	Final approval is given when all conditions of draft approval have been met. The plan may then be registered in the Registry Office. Considerable time may pass between draft approval and registration of a plan. However, the Counties has the power to provide that draft approval will lapse after three years, and the power to give extensions to draft approval.
When to sell lots?	10.	Lots may be sold after the plan of subdivision is registered. Note that the Planning Act does allow lots to be <u>offered</u> for sale after draft approval.
Timing for services	11.	The subdivision agreement between the applicant/owner and the local municipality will establish the municipality's requirements for when the various services are to be provided.

United Counties of Leeds and Grenville Subdivision Process Flowchart



Note: This is the basic subdivision process, not all steps are included.

OLT Appeal can occur at various points in the process and are not noted.

February 2024

SUBDIVISON AGREEMENT

THIS AGREEMENT made on the _____day of _____, 2024

BETWEEN:

EDWARDSBURGH DEVELOPMENT INC.

("the **OWNER**")

-and-

THE CORPORATION OF THE TOWNSHIP OF EDWARDSBURGH/CARDINAL

("the **MUNICIPALITY**")

WHEREAS the Owner is the registered owner of land ("the Lands") described in Schedule "A" and has applied to the Municipality pursuant to the *Planning Act*, for approval to subdivide and develop the Lands in accordance with a plan of subdivision (the "Plan of Division") to be registered with respect to the Lands.

AND WHEREAS approval of the Plan of Subdivision has been given on the condition that the Owner enters into this Agreement with the Municipality in accordance with section 51(26) of the *Planning Act*, RSO 1990, c. P. 13, as amended.

AND WHEREAS subsection 51(26) of the *Planning Act* permits the registration of this Agreement against the Lands to which it applies and provides that the Municipality may enforce the terms and conditions of this Agreement against the Owner and any subsequent owner of the Lands.

AND WHEREAS the subdivision shall be built in two (2) phases.

NOW THEREFORE THIS AGREEMENT WITNESSETH that in consideration of the Municipality approving the registration of the Plan of Subdivision, the covenants hereinafter expressed and for other good and valuable consideration the receipt and sufficiency of which is hereby acknowledged, the parties hereto covenant and agree as follows:

1. **DEFINITIONS**:

1.1 In this Agreement:

- (a) "Maintain" includes replace and repair.
- (b) **"Owner**" means Edwardsburgh Development Inc. and any assignor or successor and includes an individual, partnership, corporation or other entity, and any agent or contractor of the foregoing carrying out Works for the Owner.
- (c) "Plan", "Plan of Subdivision" or "Subdivision" means the proposed Plan of Subdivision submitted to the United Counties of Leeds and Grenville by the Owner for approval on July 21, 2021, and includes the lands described in Schedule "A" and shown in Schedule "I."
- (d) **"Municipality**" or "**Municipal**" means the Corporation of the Township of Edwardsburgh/Cardinal.
- (e) "Municipal Official" is any employee, contractor, or agent, that has been expressly designated by the Corporation of the Township of Edwardsburgh/Cardinal (and only those so expressly designated) for the purposes of this Agreement. A Municipal Official shall also include any employee, contractor or agent of the United Counties of Leeds and Grenville for matters impacting the new road intersections with the County Road and anything within the County Road allowance.
- (f) **"Works**" includes those services and other Works listed in Schedule "B" of this Agreement.
- (g) **"O.P.S.S."** means "Ontario Provincial Specifications, Standards and Drawings".
- (h) **"MECP**" means the Ministry of the Environment, Conservation and Parks.
- (i) **"Lands**" means the real property described in Schedule "A" and shown on the Plan of Subdivision attached hereto as Schedule "B."
- (j) **"Consulting Engineer**" means Advance Engineering and any firm of engineers retained by the Owner and approved by the Municipality.
- (k) **"Engineer**" means Greer Galloway Consulting Engineers or such other firm of engineers as may be retained by the Municipality for any purpose relating to this agreement.

- (I) **"County**" or **"United Counties**" means the United Counties of Leeds and Grenville.
- (m) "Sanitary CLI-ECA" means the Municipal sewage management collection system CLI ECA Number 155-W601 issued on July 27th, 2022 to the Township of Edwardsburgh/Cardinal.
- (n) "Storm CLI-ECA" means the Municipal stormwater management collection system CLI ECA Number 155-S701 issued on July 27th, 2022 to the Township of Edwardsburgh/Cardinal.
- (o) **"Municipal Drinking Water Licence"** or **"MDWL"** means Cardinal Water System, Licence Number: 155-102, Issue Number: 4, Dated October 22, 2021.
- (p) **"Certificate of Assumption"** means a certificate issued by the Municipal Official in accordance with section 20 of this agreement in the form attached hereto as Schedule "S."

2. SCHEDULES

2.1 The following schedules attached hereto are incorporated into this Agreement by reference and are deemed to be an integral part thereof:

a.	SCHEDULE "A"	DESCRIPTION OF THE LANDS
b.	SCHEDULE "B"	PLAN OF SUBDIVISION Approved copy of the Plan (S-1)
C.	SCHEDULE "C"	WORKS TO BE PROVIDED BY THE OWNER
d.	SCHEDULE "D"	ESTIMATED COSTS OF THE WORK Cost Estimate
e.	SCHEDULE "E"	FINANCIAL REQUIREMENTS
f.	SCHEDULE "F"	DESIGN CRITERIA AND SPECIFICATIONS Notes and Specifications (N-1) Details (D-1 to D-5 inclusive)
g.	SCHEDULE "G"	LOT GRADING AND DRAINAGE Grading & Drainage Plan (GR-1 to GR-3 inclusive) Earthwork Plan (EW-1) Geotechnical Report
h.	SCHEDULE "H"	STORMWATER MANAGEMENT

3

		& EROSION AND SEDIMENT CONTROL Stormwater Management Plan Erosion & Sediment Control Plan (ES-1) Pond Plan (PND) Sormceptor EF Sizing Report
i.	SCHEDULE "I"	SERVICING PLANS AND PUMPING STATION Site Servicing Report General Plan of Services (GSP-1, GSP-2) Plan & Profile Street A, B, C, Pathway (PP-1 to 6 inclusive) Wastewater Pumping Station & Forcemain Design Report Pumping Station Plans (PS-1 to 4 inclusive, A1, M1, E1)
j.	SCHEDULE "J"	STREET SIGNAGE AND LIGHTING Traffic Signage Plan (SIG-1) Photometric Plan (PH-1)
k.	SCHEDULE "K"	LANDSCAPING Landscaping Plan (LS-1)
I.	SCHEDULE "L"	COMPOSITE UTILITY PLAN Composite Utility Plan (CUP-1 to 3 inclusive) Utility Crossings (CR-1, CR-3) Hydro One Plan Enbridge Plan
m.	SCHEDULE "M"	NOISE ASSESSMENT Rail Noise Assessment
n.	SCHEDULE "N"	EASEMENTS AND LAND DEDICATIONS
0.	SCHEDULE "O"	PARKLAND DEVELOPMENT SPECIFICATIONS
р.	SCHEDULE "P"	ENGINEERING CONSULTANT(S)
q.	SCHEDULE "Q"	UNITED COUNTIES OF LEEDS AND GRENVILLE CONDITIONS
r.	SCHEDULE "R"	WORK SCHEDULE Schedule of Works
s.	SCHEDULE "S"	CERTIFICATE OF ASSUMPTION

3. LANDS

3.1 The lands to which this Agreement shall apply are the lands described in Schedule "A" annexed hereto and shown on the Plan of Subdivision annexed hereto as Schedule "B".

4. SCOPE OF THE WORK

- 4.1 The Owner covenants and agrees to construct and install all of the Works, more particularly set out in Schedule "C" hereto annexed, in compliance with the Work Schedule set out in Schedule "R." The said Works shall be completed at the expense of the Owner in a good and workmanlike manner and to the satisfaction of the Municipal Official.
- 4.2 The Owner shall comply with, and implement any and all reports, as updated and modified, such updates and modifications having been approved by the Municipal Official, that were supplied in support of the Owner's application for approval of the Subdivision.

5. PROSECUTION OF THE WORK

- 5.1 The Work shall proceed in a good and workmanlike manner, and to the satisfaction of the Municipal Official. If, in the opinion of the Municipal Official, the Owner is not prosecuting or causing to be prosecuted the Works required in connection with this Agreement within the specified time, or is improperly performing the Works, or should the Owner neglect or abandon any of the Works before completion, or unreasonably delay same so that the conditions of this Agreement are being violated, carelessly executed, or performed in bad faith, or should the Owner neglect or fail to renew or again perform such work as may be rejected by the Municipal Official as being or having become defective or unsuitable, or should the Owner fail to carry out any maintenance required under this Agreement, or should the Owner in any manner, in the opinion of the Municipal Official, make default in the performance of any of the terms of this Agreement, then in any such case, the Municipal Official shall promptly notify the Owner and its surety, in writing, of such default, failure, delay or neglect, and if such notification be without satisfactory answer for ten (10) calendar days after such notice, then in that case the Municipal Official shall thereupon have full authority and power to purchase such materials, tools, and machinery and to employ such workmen as in his/her opinion shall be required for the proper completion of the said work at the cost and expense of the Owner. In cases of emergency, in the opinion of the Municipal Official, such work may be done without notice. The cost of such work shall be calculated by the Municipal Official whose decision shall be final. It is understood and agreed that such costs shall be subject to an additional management fee of TWENTY-FIVE PERCENT (25%) of the labour and material value including HST or any other taxes thereon.
- 5.2 All of the Works shall be installed strictly in accordance with the specifications approved by the Municipal Official and as specified in this Agreement. The Owner

shall obtain all such permits as may be required to carry out the Works from the Municipality and/or the Province of Ontario.

- 5.3 The Owner further covenants and agrees that it is responsible for the design and supervision of construction of the roads, drains, water & sewer services in the Subdivision, but such design and supervision shall be subject to the approval of the Municipal Official. The Owner shall employ competent engineers currently registered by the Association of the Professional Engineers of Ontario, and who are expressly approved by the Municipal Official:
 - (a) To design;
 - (b) To prepare the necessary specifications for the Works;
 - (c) To obtain the necessary approvals for the Works in conjunction with the Municipality;
 - (d) To supervise the construction of the Works;
 - (e) To maintain all records or construction relating to the Works;
 - (f) To prepare and furnish all plans and drawings of the Works;
 - (g) To prepare and deliver "as-built" drawings for the Works prior to final acceptance by the Municipality;
 - (h) To complete any additional work as may be required by the Municipal Official.

The Owner shall furnish, at its own cost, all plans, specifications, calculations, contours or other information pertaining to the Works, which may be required by the Municipal Official so that he/she is able to properly, as determined in his/her sole discretion, review the design and supervision of the Works. No contract shall be awarded, and no work commenced or continued without prior written approval of the design and supervision of the Works by the Municipal Official, which approval shall not be unreasonably withheld. If for any reason the Owner commences work prior to obtaining Municipal approval, such approval may be granted retroactively but only where all required inspections can be completed. The Municipality shall be under no obligation to inspect or approve Works commenced without approval, and the Owner shall take all such steps as may be requested by the Municipality to facilitate any inspections.

5.4 It is understood and agreed that examination and acceptance of drawings, specifications and contract documents by the Municipal Official does not relieve the Owner of its obligations to carry out all Works required under this Agreement strictly in accordance with standard engineering requirements.

- 5.5 The Owner shall be responsible for payment of all professional and quasiprofessional fees and disbursements reasonably incurred by the Municipality in the determination of the nature and extent of the Works to be supplied and installed under and pursuant to this Agreement, in the negotiation and settlement of this Agreement and the enforcement hereof and in the performance by the Municipality of its rights and obligations hereunder or in connection with the preparation and enactment of relevant land use by-laws, and such fees shall include, without necessarily being limited to, engineering, planning and legal fees and costs. The parties understand that fees incurred may increase in the event of unforeseen circumstances. However, the obligation of the Owner shall remain limited to reasonable fees in the circumstances. The Owner agrees to reimburse the Municipality for reasonable costs incurred by a Municipal Official for inspections, reviews, etc. throughout the construction of the Works. The hourly rates charged for professional services will be provided by the Municipality upon the Owner's request. All fees payable by the Owner to the Municipality shall be paid within TEN (10) days of invoice.
- 5.6 The Owner agrees to submit to the Municipal Official, if requested, copies of all executed contracts relating to the construction of the Works.
- 5.7 The Municipal Official shall have the right, at all times, to inspect the installation of the Works. If at any time the Municipal Official is of the opinion that the Works are not being carried out in accordance with approved plans and specifications or in accordance with good engineering practices, he/she may stop all or any part of the work until it has been placed in satisfactory condition.
- 5.8 The Municipal Official may have any qualitative or quantitative tests made of any materials which have been or are proposed to be used in the construction of any of the Works required by this Agreement, or may require soil tests to be carried out, and the cost of such tests shall be paid by the Owner within TEN (10) days of the account being rendered by the Municipality.

6. ROADS

- 6.1 All roads in the Subdivision shall be constructed to the satisfaction of the Municipal Official and, in particular, the Owner shall provide two (2) lifts of asphalt, concrete curbs and gutters in accordance with OPSS on streets A, B, and C as shown on the Plan attached hereto at Schedule "B" and in accordance with the specifications shown in Schedule "F" and profiles in Schedule "I".
- 6.2 No paving of any street or section thereof shall be commenced until all underground Works, save and except for natural gas, have been installed, tested and approved by the Municipal Official; with CCTV work completed.

- 6.3 Where work is performed on existing roads outside the Subdivision, such roads shall be reinstated to the satisfaction of the Municipal Official.
- 6.4 Following the installation of the base course of asphalt, the Municipality shall carry out required maintenance of the roads in the Subdivision at the Owner's expense until assumed. Maintenance shall not, in any way be construed as assumption or granting of final approval or assumption of liability.
- 6.5 Following the installation of the base course of asphalt, the Municipality shall plow the roads within the Subdivision at the Municipality's expense. The Owner shall be responsible for damage sustained by Municipal snow removal equipment during snow removal operations until assumed. Municipal snow removal operations shall not, in any way, be construed as assumption or granting of final approval or assumption of liability.
- 6.6 Upon assumption by the Municipality of the underground services, walkways, landscaping, and fencing, the Owner shall convey Block H as shown on the Plan to the Municipality.

7. SANITARY SEWER WORKS

- 7.1 The Owner agrees to construct a sanitary sewer system which system shall include house connections from the sanitary sewers to the street line to service the lands in the Subdivision according to the design specifications set out in Schedules "F" and "I" of this Agreement. The Owner further agrees to Maintain such sewers, including the clearing of any blockage, until they are assumed by the Municipality. The construction and installation of all such sewers shall be in accordance with MECP and Sanitary CLI-ECA design standards. The said sewers shall be constructed to an outlet according to designs approved by the Municipal Official and the MECP. A CCTV shall be submitted by the Owner to the Municipal Official.
- 7.2 The Owner shall construct a pumping station on Block B as shown on the Plan and report attached at Schedule "I."
- 7.3 The Owner acknowledges and agrees that building permits will not be issued for the development of individual Lots in Phase 2 until the pumping station has been installed and placed in service to the satisfaction of the Municipality.

8. WATERMAINS

8.1 The Owner agrees to construct a water main system as provided for in Schedule "F" hereof and as provided for in the general plan of services located at Schedule "I", which system shall include hydrants, valves, valve boxes and house water service connections from the water main to the street line to service all lots in the Subdivision and according to MECP and Municipal Drinking Water Licence ("MDWL") design standards. The Owner shall provide the Municipality with copies of all MECP approvals and complete all required forms under the MDWL.

- 8.2 The Owner shall sub-contract and pay all related costs for tracer wire, swabbing, hydrostatic testing and disinfection of water mains. The Municipality must be on site to observe, confirm and document that all activities comply with the 2020 MECP Disinfection Procedure. The Owner must provide at a minimum, 72 hours' notice to the Municipality prior to the commencement of commissioning activities. The Municipality is responsible for the collection and submission of all microbiological samples prior to commissioning of the water mains. Only certified operators employed with the Municipality can operate water main valves during and post connection into the drinking water system. The Owner will be provided water meters and transponders by the Municipality. The Owner will be invoiced and shall pay the costs of the water meters and transponders. The Owner shall contract and pay the costs to install the water meters.
- 8.3 Upon completion of the installation of all watermains, hydrants, and water services, the Owner shall provide the Municipality with mylar(s) of the "as-built" plan(s), certified under seal by a professional engineer, showing the location of the watermains, hydrants and services. Electronic files shall also be submitted to the Municipality and the United Counties of Leeds and Grenville.

9. STORMWATER MANAGEMENT

- 9.1 The Owner shall implement all aspects of the stormwater site management plan set out in Schedule "H" attached hereto.
- 9.2 The stormwater site management, lot grade and drainage plan shall be prepared to the satisfaction of the Municipality, the South Nation Conservation Authority and the United Counties of Leeds and Grenville.
- 9.3 The Owner agrees that upon completion of all stormwater management Works, it shall provide the Municipal Official and the South Nation Conservation Authority with certification from a professional engineer that all measures have been implemented in conformity with the approved stormwater site management, lot grade and drainage plan.
- 9.4 Prior to the commencement of construction of any phase of the Subdivision (roads, utilities and off-site works, etc.), the Owner agrees to:
 - (a) have a professional engineer prepare an erosion and sediment control plan appropriate for site conditions in accordance with the current best management practices;
 - (b) have this plan reviewed and approved by the Municipality and the South Nation Conservation Authority;

- (c) monitor the effectiveness of and maintain the erosion and sedimentation control works as necessary, and;
- (d) provide certification to the Municipality and the South Nation Conservation through a professional engineer that the plan has been implemented and continuously maintained.

10. GRADING

- 10.1 The Owner shall implement all aspects of the Grade Control Plan set out in Schedule "G." It is agreed between the parties hereto that the Grade Control Plan may be amended from time to time by the Owner with the prior written approval of the Municipal Official and such approval shall not be withheld except for sound engineering reasons. The Owner shall be responsible for registering on the title of all lots affected the amended Grade Control Plan. The Owner shall be responsible for rough grading of the lands such that the material excavated for the foundation of all buildings shall be equal to the material required to complete the lot grading in accordance with the approved Lot Grading Plan.
- 10.2 The Owner agrees to submit a "Rough Lot Grading" Certificate prepared by the Consulting Engineer or Ontario Land Surveyor that certifies that the rough lot grading matches the requirements set out herein prior to the issuance of building permits. The Owner further agrees to establish ground elevation at foundation wall, consistent with the Grade Control Plan prior to foundation excavation. In all cases, the Owner will maintain, at its own expense, sufficient interim drainage and outlets to provide adequate drainage until pavement has been constructed and accepted by the Municipality. This will include the installation and removal of culverts when required by the Municipal Official or the Consulting Engineer.

11. HOUSE CONNECTIONS

- 11.1 All portions of water, storm sewer, sump pump and sanitary sewer connections from water and sewer mains, to the limit of the roads, shall be installed according to the specifications set out in Schedule "F" attached hereto and forming part of this Agreement, and shall be subject to the approval of the Municipal Official. Any connections which will involve the tunnelling or cutting of the traveled or graded portion of any road shall be made before constructing the granular base course of the roads. All connections made through any drainage ditch shall be made in such a manner that the ditch is restored to the designed grade and cross-section.
- 11.2 No person, except the Municipal Official, shall open or close any valve in the street mains or abuse or interfere with them in any manner. No hydrants may be used by the Owner or any other person for water needed during construction.

12. FISHERIES:

- 12.1 The Owner acknowledges that the unnamed watercourse is considered either direct or indirect Fish Habitat as per Section 35 of the *Fisheries Act*.
- 12.2 The Owner shall establish a 30 metre "no touch/no development" setback of the unnamed watercourse, on both sides as shown on the Plan attached at Schedule "B."
- 12.3 Subject to the requirements of Schedule "H," the Owner agrees not to interfere in any way with any existing drain or water course, without written permission from the South Nation Conservation Authority. The Owner agrees that granting such permission shall not relieve the Owner of responsibility for any damage caused by such interference and the Owner shall indemnify the Municipality in relation to any claims against the Municipality relating to such damage, provided that the Municipality shall give the Owner, at the Owner's sole cost, the opportunity to defend any such claim.

13. NOISE ATTENUATION:

- 13.1 the Owner agrees to install a noise barrier for Phase 1 in accordance with subsection (a) below and further that for Phase 2 for lots 1 and 46-52 inclusive that the noise attenuation and warning requirements be in accordance with subsections (b) to (d) inclusive:
 - (a) A treed earth berm for noise attenuation purposes shall be constructed as part of Phase 1 and constructed to the satisfaction of the Municipality.
 - (b) All residential units shall be equipped with forced air heating with central air conditioning.
 - (c) That Warning Clause Type C, in accordance with the following, shall be included on all Lease and Purchase and Sale Agreements.

Type C: "This dwelling unit has been designed with the provision for adding central air conditioning at the occupant's discretion. Installation of central air conditioning by the occupant in low and medium density developments will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment, Conservation and Parks."

(d) Bedroom and living room windows and exterior doors on the north, east and west facades of lots 1 and 47-52, and the north and west facades of lot 46 will require a minimum Sound Transmission Class (STC), being outdoor noise levels minus the targeted indoor noise level, of 30 or higher. Exterior wall components of north, east and west facades of lots 1 and 47-52, and the north and west façade of lot 46 will require a minimum STC of 45, which will be achieved with brick cladding or an acoustical equivalent according to NRC test data. Detailed STC calculations will be completed prior to building permit application for each unit type and submitted to the Township with the building permit application.

13.2 the Owner agrees for Phase 2 for Lots 1 and 47-52 inclusive that Warning Clause Type B, as follows, will be included in all Lease and Purchase and Sale Agreements. This provision is in addition to those noise attenuation and warning requirements detailed in section 13.1 of this Agreement:

Type B: "Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units, sound levels due to increasing road traffic (rail traffic) (air traffic) may on occasions interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment, Conservation and Parks."

- 13.3 The Owner agrees that where structural noise mitigation measures are required in residential units, it shall provide, prior to final building inspection, certification to the Municipality, through a professional engineer, that the noise control measures have been implemented.
- 13.4 Rooftop HVAC equipment shall not be installed on any units located in the Subdivision.
- 13.5 The Owner acknowledges and agrees that building permits will not be issued for the development of individual lots in Phase 2 until the treed earth berm has been constructed to the satisfaction of the Municipality in accordance with clause 13.1(a).

14. CN RAIL:

- 14.1 The Owner shall construct and maintain a safety berm (Phase 1) parallel to the CN railway and a chain link fence (Phase 2) in accordance with the Plan located at Schedule "K."
- 14.2 The following clause should be inserted in all development agreements, offers to purchase, and agreements of Purchase and Sale or Lease for each dwelling unit within 300m of the railway right-of-way:

"Warning: Canadian National Railway Company or its assigns or successors in interest has or have a right-of-way within 300 metres from the land the subject hereof. There may be alterations to or expansions of the railway facilities on such rights-of-way in the future including the possibility that the railway or its assigns or successors as aforesaid may expand its operations, which expansion may affect the living environment of the residents in the vicinity, notwithstanding the inclusion of any noise and vibration attenuating measures in the design of the development and individual dwelling(s). CNR will not be responsible for any complaints or claims arising from use of such facilities and/or operations on, over or under the aforesaid rights-of-way."

- 14.3 An environmental easement for operational noise and vibration emissions, registered against the subject property shall be granted in favour of CN.
- 14.4 The Owner shall enter into an Agreement with CN stipulating how CN's concerns will be resolved.

15. LANDSCAPING

- 15.1 The Owner shall install landscaping in accordance with Schedule "K".
- 15.2 All sodded areas shall be maintained by regular grass cutting and shall be graded and sodded to allow for normal grass cutting operations in order to present and maintain a neat, clean, and orderly appearance. The Subject Lands shall always be compliant with the Municipality's Clean Yards By-law.
- 15.3 The Owner shall replace at its sole expense any growth landscaping which dies within one (1) year of assumption or two (2) years of planting, whichever is the greater.
- 15.4 The Owner agrees to insert the following language in all Lease and Purchase and Sale Agreements for lots in the Subdivision:
 - (a) The general maintenance and upkeep of all ditches and drains within the subdivision are the responsibility of the property owner (buyer);
 - (b) Grass cutting along the roadside within the subdivision is the responsibility of the owner (buyer).

16. SCHOOLS

- 16.1 The Owner agrees to insert the following language in all Lease and Purchase and Sale Agreements for lots in the Subdivision:
 - (a) "The vendor makes no representation or warranties regarding which school children residing in this subdivision may attend, or that transportation will be provided by the school board."

17. STREET NAMES and SIGNAGE

17.1 The Owner covenants and agrees that all streets shown on the Plan of Subdivision shall be named as provided in Schedule "J". The Owner shall pay for and the Municipality, or the Owner acting on the instructions of the Municipality, shall supply and erect the street name signs, and civic address signs. Additionally, the Owner covenants and agrees to supply and erect any other signs that may be required in the Subdivision such as but not limited to dead end, no exit, speed restrictions, or curve. The Municipality shall invoice the Owner for the cost of the supply and installation of such signs, unless such signs are ordered and installed by the Owner in accordance with the directions of the Municipality.

18. STREET LIGHTING

- 18.1 The Owner agrees to install street lighting as provided for in Schedule "L" in accordance with the specifications set out in Schedule "L" and forming part of this Agreement.
- 18.2 The Owner shall arrange with Hydro One and the local cable, gas and telephone companies for the underground installation of services to the Subdivision and for the provision of required easements with respect to such installations.

19. ENBRIDGE GAS

- 19.1 The Owner shall install all utilities, including gas lines, in accordance with the Composite Utility Plan located at Schedule "L."
- 19.2 The Owner shall grade all streets to final elevation prior to the installation of any gas lines and provide Enbridge Gas Distribution Inc. with the necessary field survey information for the installation of the gas lines. As far as possible, the natural gas distribution system will be located in the road allowance. In the event that this is not possible, the Owner will provide easements at no cost to Enbridge Gas Distribution Inc.
- 19.3 The Owner shall pay any costs involved in installing or relocating any services, including hydro, cable, gas and telephone required by the construction of the Works in the Subdivision.

20. ACCEPTANCE OF WORKS

- 20.1 The Owner covenants to Maintain all Works installed pursuant to this Agreement for a period of ONE (1) year after preliminary approval thereof by the Municipal Official provided that preliminary approval shall not be unreasonably withheld.
- 20.2 The Owner covenants to restore any faulty workmanship or materials or any damage done by the Owner or persons claiming title from the Owner during construction of Works or buildings on the land relating to any services and Works required to be installed pursuant to this Agreement.

- 20.3 The Owner shall not apply to the Municipality for a Certificate of Assumption until at least one (1) year after the final lift of asphalt has been placed.
- 20.4 Before applying for a Certificate of Assumption for the Works or any part thereof, the Owner shall supply the Municipality with a statutory declaration that all accounts for work and materials have been paid, except normal guarantee holdbacks for accounts the Owner has paid to contractors, suppliers, etc., and that there are no claims for liens or otherwise in connection with such work done or materials supplied for or on behalf of the Owner.
- 20.5 The performance by the Owner for its obligations under this Agreement, to the satisfaction of the Municipal Official, shall be a condition precedent to the acceptance of the said Works by the Municipality.
- 20.6 When the Municipal Official is satisfied that the Works set out in this Agreement, or any part thereof, and any other or additional Works which may have been required by the Municipal Official, have been executed in accordance with this Agreement including the schedules attached hereto, and is also satisfied that all Municipal accounts have been paid and maintenance requirements met, he/she will forthwith present a report to the Council of the Municipality stating that the work or any part thereof has been completed satisfactorily and the roads are in the required condition to be assumed by the Municipality. Acceptance of any of the Works or part thereof shall be evidenced by a Certificate of Assumption issued by the Municipal Official.
- 20.7 Upon the acceptance resolution being passed by Council and the issuance of a Certificate of Assumption, ownership of the Works shall vest in the Municipality and the Owner shall have no claim or rights thereto, other than those accruing to it as Owner of the land abutting on streets on which the Works were installed.
- 20.8 The Owner covenants and agrees that it shall not dump nor permit to be dumped any fill or debris on, or will promptly remove any fill from, any public lands without the written consent of the Municipal Official.
- 20.9 The Owner agrees to Maintain the Lands in a condition acceptable to the Municipality. Lots which are or become unsightly to the public shall be cleaned up by the Owner; otherwise, such steps may be taken by a Municipal Official as necessary to restore the lots using the security provided in this Agreement.

21. BUILDING PERMITS

21.1 Building permits may be issued by the Chief Building Official, subject to other requirements of the Municipality, to construct structures on lots within the Subdivision when:

- (a) The Municipal Official has issued a letter indicating preliminary acceptance of the storm water management system, sanitary sewer system and watermains;
- (b) The Plan of Subdivision, easements and land dedications have been registered;
- (c) The base course of asphalt has received preliminary approval from the Municipal Official.

22. INITIAL PERMITS FOR MODEL HOMES

22.1 Provided that the Owner is not in default of any terms hereunder, and notwithstanding section 21 of this agreement, the Owner shall be allowed for temporary building permits to commence construction of up to four (4) model homes, but shall not convey any lot, nor allow any model homes to be occupied until the requirements of section 21 of this agreement have been met to the satisfaction of the Municipal Official.

23. FINANCIAL REQUIREMENTS

- 23.1 The Owner shall deposit with the Municipality a sufficient sum in cash or a letter of credit in accordance with the financial requirements of this Agreement as set out in Schedule "E" attached hereto and forming part of this Agreement to guarantee the construction and installation of the Works and to ensure that the Municipality is not liable for hold backs and costs under the *Construction Act*, R.S.O. 1990, c. C. 30 in respect of the Works and this Agreement. In the event that some Works or some part of the Works are constructed by a Municipal Official pursuant to this Agreement, or in the event that the Owner fails to pay the cost of any of the Works, or in the event of other default of this Agreement, the Municipality may draw upon the cash or Letter of Credit for the amount of its estimate of the cost to correct any defect prior to assuming the Works in accordance with this Agreement.
- 23.2 If the Owner provides cash or equivalent, the Municipality shall place the deposit in an interest-bearing account, and interest shall accrue to the Owner. The Municipality makes no guarantees or representations as to the interest rates that may be available at the time the funds are deposited.
- 23.3 The Owner shall provide engineering supervision and administration for all work required and/or contemplated by this Agreement. The Municipality shall provide such additional engineering review and inspection, as deemed necessary, and the costs of such review and inspection shall be paid for by the Owner. The Owner shall reimburse the Municipality for reasonable costs incurred by Municipal staff for these services throughout the construction of the development.

- 23.4 Upon the issuance of a Certificate of Assumption in accordance with section 20 of this agreement by the Municipal Official, the Owner shall be entitled to have released, by the Municipality to the Owner, all cash, principal and interest being held by it under this Agreement.
- 23.5 The Owner agrees that the Municipality may enforce, as the Owner's attorney, any performance bond given by any contractor to the Owner under any agreement for the construction of any Works, provided that this shall not constitute an assignment of such performance bond. Where the Municipality deems that there has been default by such contractor, the Municipality shall notify the Owner and the Owner shall proceed to enforce its bond within FOURTEEN (14) days or within such further time as the Municipality may allow, failing which the Municipality may proceed to enforce such bond as the Owner's attorney and at the Owner's expense.
- 23.6 The Owner acknowledges that up to \$20,000.00 of the cash or letter of credit required by this agreement may also be used by the Municipality to secure works or services required by the United Counties of Leeds and Grenville.

24. LAND DEDICATIONS AND EASEMENTS

24.1 At no cost to the Municipality, the Owner shall obtain and grant, transfer and convey unto the Municipality the easements and lands described in Schedule "N" attached hereto and forming part of this Agreement and any other drainage or environmental easements which may be required. The deeds for lands and easements shall be delivered to the Municipal solicitor by the Owner immediately following registration of the Plan. The cost of the registration shall be paid by the Owner. The Municipality shall cooperate with the Owner in acquiring easements outside the Subdivision. The Owner further covenants and agrees to convey all required easements as may be required for electrical services, internet, gas, telephone and cablevision facilities to the satisfaction of the appropriate authority. The Owner shall also enter into separate agreements, if required, with the suppliers of any utility or service. The Owner shall provide a copy of the Reference Plan showing all easements upon registration of the Plan.

25. INSURANCE

25.1 The Owner shall provide the following insurance on or before the execution of this Agreement. The insurance policy shall be with AM Best Rated A or better insurers and acceptable to the Municipality. Should any policies be changed, lapsed or cancelled, notification in writing shall be provided to the Municipality and/or the United Counties of Leeds and Grenville at least 30 days prior to the effective date.

(a) Commercial Liability Insurance

Commercial General Liability insurance issued in the amount of not less than \$10,000,000 per occurrence and in aggregate for any alleged and/or negligent acts by the Owners and those parties which the Owner is legally liable with respect to their obligations under this Agreement. Such insurance shall include but not limited to bodily injury, property damage, products and completed operations, broad form owners & contractors protective, contingent employer's liability, contractual liability, cross and several liability. The policy shall include shoring, blasting, excavating, underpinning, demolition, pile driving, caisson work and work below ground including tunnelling and grading. This policy shall be primary and noncontributory.

The policy shall provide coverage against claims for all damage or injury including death to any person or persons, or for damages to any property of the Municipality, the United Counties of Leeds and Grenville, or any other public or private property resulting from or arising out of any alleged and/or negligent act on the part of the Owner, their officers, employees, contractors, sub-contractors or those parties which they are legally responsible arising from the construction, installation or maintenance of any Work to be performed upon public rights-of-way pursuant to this Agreement. The policy shall include products and completed operations coverage for 24 months and shall be maintained in full force until final acceptance of the Work by the Municipality and/or the United Counties of Leeds and Grenville.

The Owner shall provide evidence of WSIB prior to commencement of work and during the duration of the project.

The policy shall add the Municipality, the United Counties of Leeds and Grenville, and their agents as Additional Insured.

Any Deductible shall be the sole responsibility of the Owner and the Municipality and/or the United Counties of Leeds and Grenville shall bear no responsibility for the deductible.

(b) Automobile Liability Insurance

Automobile Liability Insurance with respect to owned or leased vehicles used directly or indirectly in the performance of the Works covering liability for bodily injury, death and damage to property with a limit of not less than \$5,000,000 inclusive for each and every loss.

Prior to commencement of work, the Owner shall furnish to the Municipality with a certificate of insurance evidencing the above noted insurance. The Municipality reserves the right to request certified copies of the policies confirming the aforementioned insurance. The insurance policy will be in a form and with a company which are, in all respects, acceptable to the Municipality.

Approval of the insurance shall not relieve or decrease the liability of the Owner hereunder.

(c) Professional Liability Insurance

Should the Work involve professional design, the Owner shall ensure that any Professionals hired shall carry Professional Liability Insurance in the amount not less than \$5,000,000.00 providing coverage for acts, errors and omissions arising from their professional services performed under this Agreement. The policy SIR/deductible shall not exceed \$100,000.00 per claim and if the policy has an aggregate limit, the amount of the aggregate shall be double the required per claim limit. The policy shall be renewed for 3 years after contract termination. A certificate of insurance evidencing renewal is to be provided each and every year. The Municipality has the right to request that an Extended Reporting Endorsement be purchased by the Owner at the Owner's sole expense.

(d) Environmental Liability Insurance

At the discretion of the Municipality, the Owner may be required to purchase an Environmental Policy to cover injury to or physical damage to tangible property including loss of use of tangible property, or the prevention, control, repair, cleanup or restoration of environmental impairment of lands, the atmosphere or any water course or body of water on a sudden and accidental basis and on a gradual release. The policy shall include bodily injury, including sickness, disease, shock, mental anguish, and mental injury. The policy is to be renewed for 3 years after project completion and a Certificate of Insurance evidencing renewal shall be filed with the Municipality. The Municipality has the right to request that an Extended Reporting Endorsement be purchased by the Owner at the Owner's sole expense.

(e) Indemnification

The Owner shall defend, indemnify and save harmless the Municipality, its elected officials, officers, employees, contractors and agents from and against any and all claims of any nature, actions, causes of action, losses, expenses, fines, debts, costs (including legal costs), interest or damages of every nature and kind whatsoever, including but not limited to bodily injury, sickness, disease or death or to damage to or destruction of tangible property including loss of revenue or incurred expense resulting from disruption of service, arising out of or allegedly attributable to the negligence, acts, errors, omissions, misfeasance, nonfeasance, fraud or willful misconduct of the owner, its directors, officers, employees,

contractors, subcontractors, and those parties whom they are legally responsible in law with or in any way related to the delivery or performance of this Agreement. This indemnity shall be in addition to and not in lieu of any insurance to be provided by the Owner in accordance with this Agreement and shall survive this Agreement.

The Owner agrees to defend, indemnify and save harmless the Municipality, its elected officials, officers, employees, and agents from and against any and all claims of any nature, actions, causes of action, losses, expenses, fines, debts, costs (including legal costs), interest or damages of every nature and kind whatsoever arising out of or related to the Owners status with WSIB. This indemnity shall be in addition to and not in lieu of any proof of WSIB status and compliance to be provided by the Owner in accordance with this Agreement, and shall survive this Agreement.

26. USE OF WORKS

- 26.1 The Owner agrees that the Works referred to herein may be used by the Municipality for the purpose for which such Works are designed and such use shall not be deemed an acceptance of the Works by the Municipality nor shall such use in any way relieve the Owner of its obligations with respect to the construction and maintenance of such Works.
- 26.2 The Owner hereby grants the Municipality, its employees, agents or designates, the right and licence to enter the Lands at any time or from time to time for the purpose of making emergency repairs to any of the said Works. Such entry and repair shall not be deemed an acceptance of any of the Works by the Municipality nor an assumption by the Municipality of any liability in connection therewith nor a release from the Owner of any of its obligations under this Agreement.

27. ZONING AND BUILDING RESTRICTIONS

- 27.1 The Municipality shall regulate, by by-law, the zoning and building standards within the boundaries of the Lands. It is understood and agreed that nothing in this Agreement shall relieve the Owner of the obligation to comply, at all times, including during construction, with relevant zoning and building bylaws, as well as all Federal and Provincial legislation including the *Ontario Building Code*.
- 27.2 The Owner hereby agrees that this Agreement shall be registered on title to the Lots and Blocks contained in the Plan of Subdivision at the expense of the Owner.

28. INTEREST

28.1 Interest shall be paid at the current fixed rate, as set from time to time, and shall be payable by the Owner to Municipality on all sums of money payable to the Municipality herein which are not paid and received on the due date calculated from such due date.

29. SUBDIVIDING LOTS

29.1 The Owner covenants and agrees that it shall not subdivide any lot on the Plan of Subdivision except with the prior approval of United Counties of Leeds and Grenville, and in accordance with proper planning principles.

30. NOTICES

- 30.1 Any notice, report, direction, request or other documentation required or permitted to be given to either party hereto shall be in writing and shall be given by personal service, telex, telegram, telecopier or by envelope, to be addressed as follows:
 - (a) To EDWARDSBURGH DEVELOPMENTS INC. C/O JANSEN LAW PO BOX 820 215 VAN BUREN STREET KEMPTVILLE ON KOG 1J0
 (b) To THE CORPORATION OF THE TOWNSHIP OF
 - To THE CORPORATION OF THE TOWNSHIP OF EDWARDSBURGH/CARDINAL PO BOX 129 18 CENTRE STREET SPENCERVILLE, ON K0E 1X0 TEL: (613) 658-3055
- 30.2 Any party may by notice in writing, advise the other parties hereto, of a new address for notice, which shall then be used by the party to whom it is addressed.
- 30.3 Any notice, report, direction, request or other document delivered personally, by telex, by facsimile, by telegram, by telecopier in accordance herewith shall be deemed to have been received by and given to the addressee on the day of delivery or transmission. Any notice, report, direction, request or other document mailed as aforesaid shall be deemed to have been received by and given to the addressee on the third (3rd) business day following the date of mailing, provided that for such purposes no day during which there shall be a strike or other occurrence which shall interfere with normal mail service shall be considered a business day.

31. SUBSEQUENT PARTIES

31.1 This Agreement and everything contained herein shall ensure to the benefit of and be binding upon the parties hereto and their respective heirs, executors, administrators, successors and assigns.
32. COMPLIANCE WITH CONDITIONS:

32.1 Notwithstanding anything else contained herein, the Owner agrees that it shall comply in all respects with the conditions contained in the Revised Notice of Decision of the United Counties of Leeds & Grenville dated February 24, 2022 and attached hereto as Appendix "P".

IN WITNESS WHEREOF the parties hereto have executed this agreement as at the date first set out above.

SIGNED, SEALED AND DELIVERED

THE CORPORATION OF THE TOWNSHIP OF EDWARDSBURGH/CARDINAL

Per: Tory Deschamps

Mayor

Per: Sean Nicholson

Chief Administrative Officer

(We have the authority to bind the corporation)

EDWARDSBURGH DEVELOPMENT INC.

Per: David Simpson

President

(I have the authority to bind the corporation)

SCHEDULE "A" DESCRIPTION OF THE LANDS

PT LT 7 CON 1 Edwardsburgh; Edwardsburgh/Cardinal [PIN 68153-0243]

SCHEDULE "B"

PLAN OF SUBDIVISION

Attached:

• Draft Plan of Subdivision (S-1) February 6, 2024



	DLUUN
BLOCK No.	AREA (m
BLOCK A	32492.21
BLOCK B	397.71
BLOCK C	58.27
BLOCK D	38.97
BLOCK Da	23.67
BLOCK E	647.19
BLOCK F	1039.96
BLOCK G	626.92
BLOCK H	283.10



SCHEDULE "C"

WORKS TO BE PROVIDED BY THE OWNER

1. ROADS, CURBS AND PATHWAY

As set out in Schedule "I" and specifications provided in Schedule "F"

2. STORMWATER MANAGEMENT SYSTEM AND DETENTION BASIN

As set out in Schedule "H"

3. SANITARY SEWER SYSTEM AND PUMPING STATION

As set out in Schedule "I" and specifications provided in Schedule "F"

4. <u>WATER SYSTEM</u>

As set out in Schedule "I" and specifications provided in Schedule "F"

5. STREET LIGHTING and UTILITY SERVICE

As set out in Schedule "L."

6. <u>STREET SIGNS</u>

As set out in Schedule "J."

7. <u>LANDSCAPING</u>

As set out in Schedule "K."

8. PARK DEVELOPMENT

As set out in Schedule "N."

9. NOISE ATTENUATION MEASURES

As required by section 13 to 14 of this agreement and as shown in Schedule "M" and Schedule "K."

10. SAFETY BERM AND CHAIN LINK FENCE

As required by section 14 of this agreement and as shown in Schedule "K."

11. LOT GRADING

As per Schedule "G."

12. <u>COMMUNITY MAIL BOXES</u>

As required by Canada Post and as shown in Schedule "F."

NOTE: As constructed drawings of all installations shall be given to the Municipality (one print and one digital copy) complete with types of pipe and fittings including all fixture hydrant makes, streetlight makes, etc. before assumption by the Municipality.

SCHEDULE "D"

ESTIMATED COST OF WORK

Attached:

• Cost Estimate provided by Edwardsburgh Developments Inc. May 8, 2024

Edwardsburgh Developments Ltd.

Lockmaster's Meadow Subdivision (Phase 1 & 2), Shanly Rd, Cardinal ON

Lockmaster's Meadow Subdivision – On-Site Work

EST	IMATE					
No.	Description	Unit	Quantity	Unit Price	Total	
	General – Subdivision					
1	Mobilization/Demobilization	LS				
2	Erosion Control, Maintenance, Sediment Removal	LS			\$65,000,00	
3	Site Clearing	LS			φ05,000.00	
4	Site Trailer/Office	LS				
5	Watermain, fittings, appurtenances & Service Lines	LS			\$528,395.00	
6	Force main and fittings	LS			\$505 588 00	
7	Sanitary Sewer & Laterals	LS			ψ000,000.00	
8	Storm Sewer & Laterals, Subdrains inc. Stormceptor	LS			\$492,015.00	
9	Supply & Place Granular B Type II	TONN			\$480.000.00	
10	Supply & Place 150mm Granular A	TONN			\$ 4 60,000.00	
11	Supply & Install Concrete Mountable Curb	m			\$175,000.00	
12	Street Lighting and Signage	LS			\$28,000.00	
13	Topsoil Removal - Earth Excavation – ROW	m ³				
14	Earth Berm, Stormwater Pond & Outlet Structure	LS			¢175 000 00	
15	Utility Trenches: Hydro, Gas, Bell, Street Lighting, Ducts	m			\$175,000.00	
16	Rough Lot Grading, Swales, Parks	LS				
	Total Price	ral Items:	\$2,448,998.00			
	Pumping Station					
1	Concrete Wet Well	LS				
2	Pumping & Accessories	LS				
3	Generator Building	LS				
4	Generator, Electrical and SCADA	LS				
	Total	Price for	^r Pumpin	g Station:	\$334,900.00	
	Pavement					
1	Supply & Place HL8	TONN			\$200,000.00	
2	Supply & Place HL3 – Surface	TONN			\$225,000.00	
P		Total P	rice for I	Pavement:	\$425,000.00	
				Total:	\$3,208,898.00	
IV	Contingency					
	Contingency				\$300,000.00	
				Sub-Total:	\$3,508,898.00	
				GST (13%)	\$456,156.74	
				Total:	\$3,965,054.74	

Cost per metre of Road: \$4,956

SCHEDULE "E"

FINANCIAL REQUIREMENTS

Prior to the signing of this Agreement, the Developer shall pay to the Municipality the following deposit(s) and fee(s):

1. <u>DEPOSIT / LETTER OF CREDIT</u>

The Owner shall deposit, per clause 23, cash, certified cheque, or letter of credit in a form satisfactory to the Municipality's solicitor in the amount of \$ 2,000,000.00 two million dollars. If a letter of credit is provided it may not expire or be terminated without the written authorization of the Municipality.

The Owner shall further cause to be registered a first charge against not less than 2 lots within the subdivision in favour of the Municipality. The lots to be provided as security shall be selected by the Owner and may be replaced from time to time with other lots of a similar size and location. The Charge shall be in satisfactory form to the solicitor for the Municipality acting reasonably.

In the event that the Works remaining to be completed have a value of less than the security required, the Municipality shall provide discharges of one or more lots. The amount of security required shall be determined in the sole and unfettered discretion of the Municipality.

The cash or Letter of Credit shall remain in place until 50% of the total works has reached the substantial completion benchmark as deemed by the municipality. The owner may request to the municipality upon reaching the benchmark, to have the cash or letter of credit reduced to \$1,000,000.00 one million dollars. The reduced cash or letter of credit shall remain in place until the entire works reach substantial completion. Following substantial completion, the cash or letter of credit and lots will be returned as per section 23 excluding costs for the second layer of asphalt that will be returned once the roads are assumed by the Municipality into their road network.

2. INSPECTION FEE

The Owner shall pay sewer and water connection inspection fees as set out in the current fees by-law.

The Owner shall pay the Municipality engineering review and inspection fees as may be incurred and as set out in Clause 5.4 and 5.5 of this Agreement.

The Owner shall reimburse the Municipality for all reasonable costs incurred by its staff for inspections, reviews, and administration of this development. These costs will be invoiced to Edwardsburgh Development Inc. by the Municipality and payable within thirty (30) days from the invoice date.

SCHEDULE "F"

DESIGN CRITERIA AND SPECIFICATIONS

1. <u>ROADWAYS AND CURBS</u>

All roadways and curbs shall be constructed in accordance with the latest edition of the Ontario Provincial Standard Specifications and Drawings (OPSS and OPSDs), in accordance with the requirements of the Municipality and in accordance with the approved drawings and specifications.

A walkway connecting Shanly Road and Street B on Block H, as shown in Schedule "I", shall be constructed in accordance with the approved drawings and specifications.

Fill shall not be placed within the ROW in excess of 300mm per lift. Prior to the placement of any new material, native soil should be proof rolled and observed by the Geotechnical Consultant. All imported structural material and all material to be reused in the ROW shall be approved by the Geotechnical Consultant prior to placement.

Concrete curbs shall be in accordance with OPSD 600.100 "mountable curb with narrow gutter" with provisions made for curb depression at driveways.

The final lift of asphalt for streets in phase 1 shall not be placed and compacted until 80% of the homes for phase 1 are completed. Likewise, the final lift of asphalt for streets in phase 2 shall not be placed and compacted until 80% of the homes for phase 2 are completed.

2. WATERMAINS AND WATER SERVICES

All watermains, water services and related appurtenances are to be constructed in accordance with the latest edition of the OPSS and OPSDs, relevant AWWA specifications, the Certificate of Approval as issued by the Ministry of the Environment, and the approved drawings. All new watermains and water services are to be hydrostatically tested as described in the OPSS and to be disinfected and tested for bacteriological presence as described in AWWA C651-99. The swabbing, hydrostatic testing and disinfection testing will be completed by the Owner with Municipal oversight to ensure compliance with the MECP disinfection procedure.

If pumping exceeds 50,000L per day, a permit to take water must be obtained. Pumping records are to be maintained for the duration of construction to document whether or not this amount is exceeded. Any discharge to the municipal sewer is to be shown to be in compliance with the sewer use bylaw and written approval shall be obtained by the Municipality prior to any such discharge.

Tracer wire testing is required as part of the commissioning process. The Owner shall ensure this is completed by their Contractor prior to backfilling.

Water Meters shall be obtained from the Municipality at the cost of the Owner, and are to be installed by the Owner during construction, and must be inspected and approved by the Municipality prior to activating any new water service.

The Municipality shall ensure that water service is available on the south side of County Road #22 within a reasonable time. Such water service shall have a proper shut off valve installed.

The Owner agrees to pay the Municipality the following rate per connection for access to water:

\$1,500.00 per unit

3. SANITARY AND STORM SEWERS

Storm and sanitary sewers shall be installed to comply with the Municipality's Consolidated Linear Infrastructure Environmental Compliance Approvals (CLI ECA) requirements; the MECP publication "Design Criteria for Sanitary Sewers, Storm Sewers and Forcemains for Alterations Authorized under Environmental Compliance Approval", as amended, and in accordance with the approved drawings and specifications herein.

The storm and sanitary sewer systems shall comply with the inspection and testing requirements set out in the MECP publication "Design Criteria for Sanitary Sewers, Storm Sewers and Forcemains for Alterations Authorized under Environmental Compliance Approval", as amended, and documentation of the inspection and testing results shall be submitted to the Municipality. CCTV for sanitary sewers is required to be submitted to the Municipality.

All sewers shall be installed with pipe laser and checked with level instrument prior to backfilling.

The Owner agrees to pay the Municipality the following rates per connection for access to sanitary sewer:

\$1,500.00 per unit.

4. <u>COMMUNITY MAIL BOXES</u>

The Owner covenants and agrees to provide the Municipality with evidence that satisfactory arrangements, financial and otherwise, have been made with Canada Post Corporation for the installation of Community Mail Boxes (CMB) as required by Canada Post Corporation and as shown on the approved Plan. The Owner further covenants and agrees to provide notice to prospective purchasers of the location of the CMB and that home mail delivery will be provided via CMB, provided the Owner has paid for the activation and equipment installation of the CMB.

Attached:

- General Notes and Specifications (N1) December 1, 2023
- Details (D1 to D5 inclusive) February 6, 2024

UNITED COUNTIES OF LEEDS AND GRENVILLE VILLAGE OF CARDINAL

LOCKMASTER' S MEADOW SUBDIVISION ROADS, SEWERS & WATERMAINS

	LIST OF DRAWINGS					
No.	INDEX	TITLE	REV. No.	DATE		
1	CS-1	COVER SHEET - LIST OF DRAWINGS	5	04-22-2024		
2	N-1	GENERAL NOTES AND SPECIFICATIONS	5	12-01-2023		
3	S-1	DRAFT PLAN OF SUBDIVISION	8	02-06-2024		
4	GSP 1	GENERAL SERVICES PLAN PHASE 1	8	02-06-2024		
5	GSP 2	GENERAL SERVICES PLAN PHASE 2	8	02-06-2024		
6	PP-1	PLAN & PROFILE STREET A - STATION 0+000 TO 0+169	8	02-06-2024		
7	PP-2	PLAN & PROFILE STREET B - STATION 0+000 TO 0+375	8	02-06-2024		
8	PP-3	PLAN & PROFILE STREET B - STATION 0+375 TO 0+670	8	02-06-2024		
9	PP-4	PLAN & PROFILE STREET B - STATION 0+670 TO 0+796.2	8	02-06-2024		
10	PP-5	PLAN & PROFILE STREET C & PATHWAY	8	02-06-2024		
11	PP-6	PLAN & PROFILE COUNTY RD 22	8	02-06-2024		
12	GR-1	GRADING AND DRAINAGE PLAN PHASE 1	7	02-06-2024		
13	GR-2	GRADING AND DRAINAGE PLAN PHASE 2	7	02-06-2024		
14	GR-3	GRADING AND DRAINAGE PLAN DETAILS	7	02-06-2024		
15	D-1	DETAILS SHEET 1	5	02-06-2024		
16	D-2	DETAILS SHEET 2	5	02-06-2024		
17	D-3	DETAILS SHEET 3	5	02-06-2024		
18	D-4	DETAILS SHEET 4	5	02-06-2024		
19	D-5	DETAILS SHEET 5	5	02-06-2024		
21	ES-1	EROSION AND SEDIMENT CONTROL PLAN	6	02-06-2024		
20	LS-1	LANDSCAPE PLAN	3	09-05-2023		
20	CUP 1/3	COMPOSITE UTILITY PLAN PHASE 1	4	07-25-2023		
20	CUP 2/3	COMPOSITE UTILITY PLAN PHASE 2	4	07-25-2023		
20	CUP 3/3	COMPOSITE UTILITY PLAN DETAILS	4	07-25-2023		
22	PND	POND PLAN	4	02-06-2024		
23	SIG-1	TRAFFIC SIGNAGE PLAN	1	09-06-2023		
24	EW-1	EARTHWORKS PLAN	1	02-06-2024		

PART OF LOT 7, CONCESSION 1 GEOGRAPHIC TOWN OF EDWARDSBURGH TOWNSHIP OF EDWARDSBURGH/CARDINAL COUNTY OF GRENVILLE ADDRESS: COUNTY RD No. 22 CARDINAL, ONTARIO

> APPLICANT: Edwardsburgh Developments Ltd. 434-300 EARL GREY DRIVE KANATA, ON K2T 1C1 613-282-5601

> > CONSULTANT:

ADVANCE ENGINEERING Civil - Municipal - Structural 613-986-170

PROJECT No. 114

APRIL 2024





GENERAL NOTES AND SPECIFICATIONS

- ALL WORKS AND MATERIALS SHALL CONFORM TO THE LATEST REVISIONS OF THE STANDARDS AND SPECIFICATIONS OF THE CITY OF OTTAWA, AND ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD) AND SPECIFICATIONS (OPSS). AS AMENDED BY THE CITY OF OTTAWA. REFER TO THE LATEST MS-22.15 AND MW-19.15 FOR APPROVED PRODUCTS AND MATERIAL TO BE USED FOR WATERMAIN AND SANITARY AND STORM SEWERS
- ALL WORKS TO BE IN ACCORDANCE WITH TOWNSHIP OF EDWARDSBURGH CARDINAL BY-LAWS, INCLUDING BY-LAW No. 2013-69.
- ALL SANITARY AND STORM WORKS SHALL COMPLY WITH THE TOWNSHIP'S CLI-ECA REQUIREMENTS AND THE MECP DESIGN CRITERIA FOR SANITARY SEWERS, STORM SEWERS AND FORCEMAINS DATED MAY 31, 2023 OR AS REVISED; AND THE MECP DESIGN GUIDELINES FOR SEWAGE WORKS, 2008, AS AMENDED FROM TIME TO TIME.
- 4. ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH THE "OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS" THE GENERAL CONTRACTOR SHALL BE DEEMED TO BE THE CONSTRUCTOR AS DEFINED IN THE ACT.
- ALL CONSTRUCTION SIGNAGE MUST CONFORM TO THE M.T.O. MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES (LATEST AMENDMENT).
- THE CONTRACTOR SHALL CONFIRM THE LOCATION OF ALL EXISTING UTILITIES WITHIN THE SITE AND ADJACENT WORK AREAS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING ALL EXISTING UTILITIES TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR REPAIR OR REPLACEMENT OF ANY SERVICES OR UTILITIES DISTURBED DURING CONSTRUCTION, TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION.
- ANY CONFLICTS WITH EXISTING SERVICES AND/OR UTILITIES SHALL BE REPORTED TO THE ENGINEER FOR REVIEW & ADVICE PRIOR TO COMMENCEMENT OF CONSTRUCTION.
- RELOCATION OF EXISTING SERVICES AND/OR UTILITIES SHALL BE AS SHOWN ON THE DRAWINGS OR AS DIRECTED BY THE ENGINEER AT THE EXPENSE OF THE DEVELOPER.
- THE SUPPORT OF ALL UTILITIES SHALL BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE AUTHORITY HAVING JURISDICTION.
- 10. ANY AREAS BEYOND THE LIMIT OF THE SITE DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO ORIGINAL CONDITION OR BETTER TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION AT THE CONTRACTOR'S EXPENSE.
- 11. ALL DIMENSIONS AND ELEVATIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO THE START OF CONSTRUCTION. ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE ENGINEER.
- 12. ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE SPECIFIED. PIPE SIZES ARE IN MILLIMETRE. PIPE/CULVERT SECTION SIZES REFER TO INSIDE DIMENSIONS.
- 13. THERE WILL BE NO SUBSTITUTION OF MATERIALS UNLESS PRIOR WRITTEN APPROVAL BY VILLAGE OF CARDINAL HAS BEEN OBTAINED.
- 14. ALL BOREHOLES SHOWN ON THE DRAWINGS ARE FOR INFORMATION ONLY. REFER TO GEOTECHNICAL INVESTIGATION REPORT BY ST LAWRENCE TESTING & TESTING INSPECTION CO. LTD. DATED MAY 31, 2021, FOR ADDITIONAL DETAILS REGARDING MATERIAL AND CONSTRUCTION SPECIFICATIONS. IN CASE OF DISCREPANCIES BETWEEN THESE SPECIFICATIONS AND THE GEOTECHNICAL RECOMMENDATIONS, FOLLOW THE GEOTECHNICAL.
- 15. SHOULD DEEPLY BURIED ARCHAEOLOGICAL REMAINS BE FOUND ON THE PROPERTY DURING CONSTRUCTION ACTIVITIES, THE HERITAGE OPERATIONS UNIT OF THE ONTARIO MINISTRY OF CULTURE MUST BE NOTIFIED IMMEDIATEI Y
- 16. CLEARING AND GRUBBING SHALL BE COMPLETED BY THE CONTRACTOR.
- REVIEW WITH THE VILLAGE OF CARDINAL PRIOR TO ANY TREE CUTTING. 17. VEGETATION REMOVAL WHERE REQUIRED SHOULD TAKE PLACE OUTSIDE OF THE SPRING AND SUMMER ACTIVE SEASON (TYPICALLY APRIL 1 TO SEPTEMBER 30).
- 18. SHOULD ANY SPECIES AT RISK BE DISCOVERED THROUGHOUT THE CONSTRUCTION PERIOD, THE LOCAL MECP DISTRICT SHOULD BE CONTACTED IMMEDIATELY.
- 19. DURING CONSTRUCTION. SHOULD THE GROUNDWATER VOLUME OF PUMPING EXCEED 50,000 LITRES PER DAY, A PERMIT TO DEWATER SHOULD BE OBTAINED. SUITABLE FILTRATION WILL BE REQUIRED BEFORE DISCHARGING GROUNDWATER INTO SEWERS.
- 20. PERMIT WILL BE NEED TO BE OBTAINED FROM THE VILLAGE FOR ROAD CUTS.
- 21. ALL WATER CUSTOMERS SUPPLIED BY A WATERMAIN TO BE SHUT DOWN SHALL BE NOTIFIED BY THE CONTRACTOR AT LEAST 24 HOURS IN ADVANCE OF THE SHUT DOWN OR AS DIRECTED BY VILLAGE OF CARDINAL STAFF. 22. EXCESS SOILS MANAGEMENT SHALL COMPLY WITH O. REG. 406/19 ONSITE
- AND EXCESS SOIL MANAGEMENT. CONTRACTOR SHALL FILE A NOTICE AT RPRA "EXCESS SOIL REGISTRY" PRIOR TO EXCAVATION.
- 23. SHOP DRAWINGS: CONTRACTOR TO SUBMIT SHOP DRAWINGS FOR REVIEW FOR ALL STRUCURES SHOWING EXACT DETAILS. 24. CONTRACTOR SHALL PERFORM LEAKAGE TESTING, IN THE PRESENCE OF THE
- ENGINEER, FOR SANITARY AND STORM SEWERS IN ACCORDANCE WITH OPSS 410 AND OPSS 407. CONTRACTOR SHALL PERFORM VIDEO INSPECTION OF ALL SEWERS. A COPY OF THE VIDEO AND INSPECTION REPORT SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW.
- 25. CLAY SEALS TO BE INSTALLED AS PER OPSS 1205 AND OPSD 802.095 AS INDICATED ON THE GENERAL PLAN OF SERVICES PLAN. CLAY LAYERS TO BE COMPACTED TO A MINIMUM OF 95% SPMDD.
- 26. ALL SEWERS CONSTRUCTED WITH GRADES 0.50% OR LESS, SHALL BE INSTALLED WITH PIPE LASER AND CHECKED WITH LEVEL INSTRUMENT PRIOR TO BACKFILLING.
- 27. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ADDITIONAL BEDDING OR ADDITIONAL STRENGTH PIPE IF THE MAXIMUM TRENCH WIDTH, AS SPECIFIED BY OPSD, IS EXCEEDED.
- 28. ALL PVC PIPES AND RUBBER GASKETED JOINTS SHALL CONFORM TO THE REQUIREMENTS OF OPSS 1841 AND OPSD 806.040 & 806.060 WITH REGARD TO MAXIMUM FILL/COVER.

WATER SUPPLI

WATERMAIN SHALL BE PVC MINIMUM DR 18 WITH GASKETED JOINTS EQUAL TO AWWA C-900, C-905 & C-907 CLASS 150, OR APPROVED EQUAL.

- SPATIAL SEPARATION: A MINIMUM HORIZONTAL SEPARATION OF 2.5 m MUST BE MAINTAINED BETWEEN WATERMAIN AND SANITARY OR STORM SEWERS. WATER SERVICES SHALL COMPLY WITH OBC 7.3.5.7., IN A COMMON TRENCH. 31. THE WATER SERVICE SHALL BE PLACED ON A SHELF AT ONE SIDE OF THE TRENCH WITH A MINIMUM VERTICAL CLEARANCE OF 0.5 m ABOVE THE SANITARY PIPE
- WATERMAIN TRENCH AND BEDDING SHALL BE IN ACCORDANCE WITH CITY OF OTTAWA STANDARD W17 OR OPSD 802.010, UNLESS OTHERWISE SPECIFIED. BEDDING AND COVER MATERIAL SHALL BE AS SPECIFIED BY PROJECT GEOTECHNICAL ENGINEER.
- MINIMUM DEPTH OF COVER FOR MAIN AND SERVICE CONNECTION FROM TOP OF PIPE TO FINISHED GRADE IS 2.4 m. WHEN LESS COVER. PROVIDE INSULATION AGAINST FROST AS PER OTTAWA DETAIL W22 OR OPSD 1109.03. INSULATION SHALL BE 275 kPa (40 psi). WATERMAIN SHALL BE AT LEAST 1.1 m BELOW BOTTOM OF ROAD SIDE DITCH.
- THE DEPTH OF WATER SERVICES AT PROPERTY LINE SHOULD BE A MINIMUM OF 2.2 m AND A MAXIMUM OF 2.6 m. THE DISTANCE BETWEEN THE GROUND ELEVATION AND THE TOP OF THE ROD SHOULD BE BETWEEN 0.5 m AND 1.0 m.
- SERVICE CONNECTION SHALL BE 25 mm DIA. TYPE K SOFT COPPER. INSTALL AS PER OPSD 1104.010. 50 mm DIAMETER SHALL BE USED FOR PARK SERVICES AND PUMPING STATION.
- WATER SERVICES SHALL BE MARKED WITH A "50 mm x 100 mm". EXTENDING FROM THE INVERT TO 1.0 m ABOVE GRADE PAINTED BLUE. STAND POSTS/SHUT-OFFS SHALL BE INSTALLED AT THE PROPERTY LINE.
- CATHODIC PROTECTION IS REQUIRED ON ALL PVC WATERMAIN AND METALLIC FITTINGS, RESTRAINERS AND HYDRANTS AS PER OPSD 1109.011 OR OTTAWA STD. W40.
- ALL SACRIFICIAL ANODES SHALL CONFORM TO A.S.T.M. B-418 TYPE II AND SHALL BE MADE OF HIGH GRADE ELECTROLYTIC ZINC, 99.99%.
- 10. ALL WELD CONNECTIONS TO BE COATED WITH "TC MASTIC" OR APPROVED EQUIVALENT.
- 11. FOR ALL ANODES CONNECTED TO NEW PIPE, FITTINGS OR TO EXISTING METALLIC WATERMAINS, A CADWELDER AND CA-15 OR EQUIVALENT CARTRIDGE SHALL BE USED. ANODE INSTALLATION SHALL BE PERFORMED IN ACCORDANCE WITH THE MANUFACTURERS INSTRUCTIONS.
- 12. CONTRACTOR TO SUPPLY HYDRANT EXTENSION TO ADJUST THE LENGTH OF HYDRANT BARREL
- 13. FIRE HYDRANTS TO BE IN ACCORDANCE WITH AWWA A502 LATEST EDITION. ACCEPTED MODELS: CLOW CANADA M-67/M93 BRIGADIER, MCAVITY M67B OR CONCORD D67-M WITH PUMPER NOZZLE OUTLETS OR EQUIVALENT. HYDRANTS TO BE PAINTED YELLOW WITH A RED CAP. VILLAGE TO BE CONTACTED DURING CONSTRUCTION TO CONFIRM IF DRAIN HOLES ARE TO BE PLUGGED OR REMAIN OPEN.
- FIRE HYDRANTS SHALL BE INSTALLED AS PER OPSD 1105.10 AND AT LEAST 1.5 m FROM EDGE OF DRIVEWAYS. CITY OF OTTAWA STD. W19 MAY BE USED
- 15. TAPPING FOR SERVICE CONNECTION SHALL BE DONE WITH FULL OPERATING PRESSURE IN THE MAIN. CONNECTION TO MAIN AT ANGLE OF 15 DEGREE TO 45 DEGREE FROM HORIZONTAL C/W WITH SADDLE.
- 16. PROVIDE CURB-STOP AND BOX AT PROPERTY LINE ON THE STREET SIDE. CURB-STOP SHALL NOT BE IN DRIVEWAY OR FUTURE SIDEWALK.
- 17. PVC WATERMAIN SHALL BE INSTALLED WITH A 10 GAUGE STRANDED COPPER TWU OR RWU TRACER WIRE IN ACCORDANCE WITH CITY OF OTTAWA STD. W36
- THE CONTRACTOR SHALL PROVIDE ALL TEMPORARY CAPS, PLUGS AND - 18. BLOW-OFFS AND NOZZLES REQUIRED FOR TESTING AND DISINFECTION OF THE WATERMAIN.
- INSULATION FOR WATERMAIN CROSSING OVER AND BELOW SEWER SHALL BE IN ACCORDANCE WITH CITY OF OTTAWA STD. W25.2 AND W25, RESPECTIVELY, WHERE WATERMAIN COVER IS LESS THAN 2.4 m
- WHERE THE SEPARATION BETWEEN SERVICES AND MANHOLES IS LESS THAN 20. 1.2 m. WATER SERVICES ARE TO BE INSULATED AS PER CITY OF OTTAWA STD. W23.
- 21. THE MINIMUM VERTICAL CLEARANCE BETWEEN WATERMAIN AND SEWER UTILITY IS 0.25 m FOR CROSSING OVER THE SEWER, AS PER CITY STD W25.2. FOR CROSSING UNDER SEWER. THE MINIMUM VERTICAL CLEARANCE IS 0.50 m AS PER CITY STD. W25. FOR CROSSING UNDER SEWER, ADEQUATE STRUCTURAL SUPPORT FOR THE SEWERS IS REQUIRED TO PREVENT EXCESSIVE DEFLECTION OF JOINTS AND SETTLING. THE LENGTH OF WATER PIPE SHALL BE CENTRED AT THE POINT OF CROSSING SO THAT THE JOINTS WILL BE EQUIDISTANT AND AS FAR AS POSSIBLE FROM THE SEWER.
- 22. VALVE IN BOXES SHALL BE INSTALLED AS PER CITY OF OTTAWA STD. W24. 23. ALL PLUGS. CAPS. TEES AND BENDS SHALL BE MECHANICALLY RESTRAINED AS PER MANUFACTURERS SPECIFICATIONS. RESTRAINTS SHALL MEET UNI-B-13-92.
- 24. VALVES SHALL BE RESILIENT-SEATED AS OPER AWWA C509 AND SHALL OPEN COUNTER-CLOCKWISE. VALVES SHALL BE SUPPLIED BY MUELLER, CANADA VALVE, MCAVITY CLOW OR APPROVED EQUIVALENT.
- 25. VALVE BOXES SHALL BE A 130 mm DIAMETER SLIDE VALVE BOX COMPLETE WITH CASE IRON CAP AS SUPPLIED BY BIBBY-SITE-CROIX OR APPROVED EQUIVALENT.
- PIPE BARREL BENDING DEFLECTION SHALL NOT BE ALLOWED. PIPE JOINT DEFLECTIONS ARE DISCOURAGED, HOWEVER, IF ABSOLUTELY NECESSARY, THE MAXIMUM ALLOWABLE PIPE JOINT DEFLECTION SHALL BE 50% OF THE MANUFACTURER'S SPECIFICATIONS.
- TRACER WIRE IS TO BE INSTALLED ON ALL NEW PVC WATERMAIN PIPE FOR LOCATING PURPOSES. A SOLID 10 GAUGE T.W.U. COPPER WIRE IS TO BE INSTALLED ALONG THE PIPE, STRAPPED TO THE PIPE AT 6 METRE INTERVALS. JOINTS IN THE WIRE BETWEEN VALVES ARE NOT PERMITTED
- THE INSPECTOR MAY TEST THE TRACING WIRE FOR CONDUCTIVITY. IF THE TRACING WIRE IS NOT CONTINUOUS FROM VALVE TO VALVE. THE CONTRACTOR SHALL, AT HIS OWN EXPENSE, REPLACE OR REPAIR THE WIRE.



- 29. OPERATION OF EXISTING WATERMAINS SHALL BE BY VILLAGE OF CARDINAL STAFF ONLY
- 30. WATERMAIN IN FILL AREA OR IN PREVIOUSLY DISTURBED GROUND TO BE INSTALLED WITH RESTRAINED JOINTS AS PER CITY OF OTTAWA STD. W25.5 AND W25.6.
- THRUST BLOCKING OF WATERMAIN TO BE INSTALLED AS PER CITY OF OTTAWA STD. W25.3 AND W25.4. 32. FOR STUBS DESIGNED FOR FUTURE WATERMAIN CONNECTION, THE END OF
- THE PIPE SHOULD BE CAPPED TO MAKE IT WATERTIGHT AND THRUST RESTRAINT ADDED ACCORDING TO CITY STANDARD.
- OF OTTAWA STD. W38. 34. VALVE CHAMBER COVER TO BE SET FLUSH WITH BASE COURSE ASPHALT AND ADJUSTED TO FINAL GRADE PRIOR TO INSTALLING TOP LIFT OF
- <u>SANITARY</u> SEWERS
- SANITARY SEWER PIPE SHALL BE PVC MINIMUM SDR 35, IPEX "RING-TITE" OR EQUIVALENT, AS PER CSA STANDARD B182.2 (LATEST AMENDMENT), WITH A MINIMUM PIPE STIFFNESS OF 320 kPa.
- SANITARY FORCEMAIN SHALL BE PVC MINIMUM DR 26. SANITARY SEWER TRENCH AND BEDDING SHALL BE AS PER CITY OF OTTAWA STD. S6 AND S7, CLASS 'B' BEDDING OR OPSD 802.010 UNLESS
- OTHERWISE NOTED. MINIMUM COVER FOR SEWER MAIN BELOW ROAD CENTRELINE IS 2.5 m. WHEN LESS COVER, PROVIDE INSULATION FROST PROTECTION AS PER OTTAWA DETAIL W22 OR ONTARIO STANDARDS OPSS 1605 AND OPSD 1109.030. INSULATION SHALL BE 275 kPa (40 psi).
- ALL SANITARY LATERALS ARE TO BE PVC SDR 28 CONFORM TO CSA B182.2, W/ RUBBER GASKET JOINT, IPEX "RING-TITE" (OR EQUIVALENT), ANY COLOUR EXCEPT WHITE AND MARKED WITH A 50 mm x 100 mm WOODEN MARKER, EXTENDING FROM THE INVERT TO 1.0 m ABOVE GRADE PAINTED RED. SINGLE CONNECTIONS SHALL BE 135 mm DIAMETER.
- SERVICE CONNECTION SHALL BE LAID AT 1-2 % SLOPE AND 2.15 m MIN. AND 2.75 m MAX. DEEP BELOW FINISHED GRADE AT PROPERTY LINE. SERVICE CONNECTION SHALL BE TERMINATED AT 1.5 - 3.0 m INSIDE THE
- SANITARY MANHOLES TO BE AS PER OPSD 701.010. BENCHING IN MANHOLES AS PER OPSD 701.021. GRANULAR BACKFILL AROUND MANHOLES SHALL BE COMPACTED BY MECHANICAL MEANS TO A MINIMUM OF 95% SPD. SANITARY MANHOLE FRAME AND COVERS SHALL BE AS PER OPSD. 401.010 TYPF A
- 10. SAFETY PLATFORMS WHEN REQUIRED SHALL BE AS PER OPSD 404.020. 11. MANHOLE COVER TO BE SET FLUSH WITH BASE COURSE ASPHALT AND ADJUSTED TO FINAL GRADE PRIOR TO INSTALLING TOP LIFT OF ASPHALT.
 - FOR SANITARY MANHOLES, DEPENDING ON THE ELEVATION OF THE GROUNDWATER TABLE, AND BASED ON THE RECOMMENDATION OF THE PROJECT GEOTECHNICAL CONSULTANT, CRETEX SEALS, OR A SIMILAR PRODUCT. SHALL BE INSTALLED IN THE FIRST PRE-CAST MANHOLE SECTION TO JUST BELOW THE MANHOLE FRAME TO PREVENT INFILTRATION.
- STORM SEWER:
- MAINTENANCE HOLES, CATCH BASINS, PIPES, CHAMBERS TO BE AS PER OPSD. MATERIAL USED SHALL BE APPROVED BY THE VILLAGE.
- POLYVINYL CHLORIDE (PVC) PIPE SHALL BE SDR 35 AND MEET THE CANADIAN STANDARD ASSOCIATION REQUIREMENT C.S.A. B182.2 AS NOTED WITHIN OPSS 1841. THE BASIC MATERIAL USED IN MANUFACTURING THIS PIPE SHALL HAVE A CELL CLASSIFICATION OF 12454-B OR 12454-C OR ASTM STANDARD D-3034 AND OPSS 18. PVC PIPE MAXIMUM ALLOWABLE DEFLECTION OF MAIN SEWER IS 5%.
- ALL STORM LATERALS SHALL BE PVC SDR 28 TO CSA B182.2. WHITE IN COLOUR AND MARKED WITH A 50 x 100 mm WOODEN MARKER EXTENDING FROM THE INVERT TO 1.0 m ABOVE GRADE PAINTED GREEN, HOUSE CONNECTIONS SHALL BE 2.0 m MIN. BELOW FINISHED GRADE AT PROPERTY LINE WHERE POSSIBLE. SINGLE CONNECTIONS SHALL BE 100 mm DIAMETER. STORM SEWERS WITH DIAMETERS LARGER THAN 375mm SHALL BE HDPE N-12, OR REINFORCED CONCRETE IN ACCORDANCE WITH CSA A257.2
- (LATEST AMENDMENT), MINIMUM CLASS 65-D. STORM MANHOLES TO BE AS PER OPSS 1351 AND OPSD 701.010-701.081 (INCLUSIVELY). ADJUSTMENT UNITS: PRECAST CONCRETE TO OPSD 704.010, PARGED OR SEALED PER OPSS 407. MAXIMUM 3 ADJUSTMENTS UNITS PER
- STRUCTURE. PRECAST CONCRETE CATCH BASINS SHALL CONFORM TO OPSD 705.010 IN ROAD AND OPSD 705.030 IN GRASSED AREA.
- CATCH BASIN FRAME AND GRATE AS PER OPSD DETAILS 400.010 AND 610.010 IN ROAD AND 403.010 IN GRASSED AREA.
- THE COMPACTION OF ALL BEDDING AND COVER MATERIAL SHALL BE 95% STANDARD PROCTOR OR BETTER. MAXIMUM COVER SHALL BE IN ACCORDANCE WITH OPSD 806.040 AND 806.060. SPECIAL CARE MUST BE GIVEN TO CONTOURING THE BEDDING MATERIAL TO CONFORM WITH THE PIPE BOTTOM AND PROJECTING BELLS, ALONG WITH PROPER COMPACTION OF THE HAUNCHES IN ORDER TO PROVIDE EVEN SUPPORT THROUGHOUT THE PIPE. ALL STORM SEWER MANHOLES SHALL BE CONSTRUCTED WITH A 300 mm
- SUMP. CATCHBASINS AND CATCHBASIN MANHOLES SHALL BE CONSTRUCTED WITH A 600 mm SUMP UNLESS OTHERWISE NOTED. 10. DOUBLE CATCHBASINS SHALL BE IN ACCORDANCE WITH OPSD 705.020 11. SINGLE AND DOUBLE CATCHBASIN LEADS SHALL BE 200 AND 250 mm
- DIAMETER (MIN.), RESPECTIVELY, AT 1.0% SLOPE (MIN.) UNLESS OTHERWISE NOTED.

- 12. CONTRACTOR SHALL ENSURE THAT CATCHBASINS ARE INSTALLED AT THE LOW POINT OF SAG CURB WORKS.
- 13. PROVIDE SUB-DRAINS OF 150 mm HDPE PERFORATED BELOW CURBS AS PER OPSS 405, 140 AND 18. SUBDRAINS TO HAVE POSITIVE OUTLET TO
- STORM SEWERS 14. THE MINIMUM DIAMETER FOR REAR LOT PERFORATED PIPE IS 250 mm,
- REFER TO OTTAWA STD. S29 FOR DETAIL, UNLESS OTHERWISE NOTED. 15. FOR TWO OR MORE REAR LOT CATCH BASINS CONNECTED IN SERIES, THE
- LEAD FROM THE LAST REAR LOT CB TO THE STORM SEWER SHALL BE SOLID PIPE 33. ALL WATER SERVICES CROSSING SEWERS ARE TO BE INSTALLED AS PER CITY 16. RLCB LEAD DRAINAGE EASEMENTS SHOULD BE 2.4 m WIDE AND CLEAR OF
 - ANY ROOF OVERHANGS AND FOOTINGS. 17. PROVIDE MOUNTABLE CONCRETE CURB AS PER OPSD 600.100.
 - 18. STORM PIPES TO BE CONNECTED OBVERT TO OBVERT WHEN DOWNSTREAM PIPE IS HIGHER THAN UPSTREAM PIPE. A MINIMUM DROP OF 75 mm IS TO BE MAINTAINED.
 - 19. ALL SEWERS ARE TO HAVE AN UNDISTURBED BASE. 20. STORM SERVICE CONNECTIONS SHALL BE EXTENDED A MINIMUM OF 2.0 m
 - BEYOND THE PROPERTY LINE AND CAPPED TO ALLOW FOR FUTURE CONNECTION.
 - <u>ROADWORK SPECIFICATIONS:</u>
 - ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD ALLOWANCE PRIOR TO THE COMMENCEMENT OF CONSTRUCTION. 2. PAVEMENT DESIGN TYPE AS PER GEOTECHNICAL REPORT:
 - LOCAL ROADS (STREET A, STREET B, STREET C)
 - 40 mm ASPHALT HL3 (TOP COURSE)
 - 40 mm ASPHALT HL8 (BASE COURSE)
 - 150 mm GRANULAR 'A' COMPACTED TO 100%
 - 375 mm GRANULAR B' TYPE II COMPACTED TO 100% SPD 605 mm TOTAL THICKNESS
 - PAVED WALKWAY
 - 50 mm ASPHALT HL3
 - 150 mm GRANULAR 'A' COMPACTED TO 100%
 - 250 mm GRANULAR 'B' TYPE II COMPACTED TO 100% SPD 450 mm TOTAL THICKNESS
 - PAVEMENT FOR INDIVIDUAL DRIVEWAY
 - 25 mm OF HL3 ASPHALT
 - 50 mm OF HL8 ASPHALT
 - 150 mm COMPACTED DEPTH OF GRANULAR 'A'
 - PAVEMENT REINSTATEMENT FOR SERVICE AND UTILITY CUTS SHALL BE IN ACCORDANCE WITH CITY OF OTTAWA STD. R10 AND OPSD 509.010, OPSS 310.
 - ALL GRANULAR 'A' AND GRANULAR 'B' MATERIALS QC TESTING SHALL BE UNDERTAKEN BY THE CONTRACTOR AS PER RELEVANT OPSS SPECIFICATIONS AND THE RESULTS OF THE QA TESTING WILL DETERMINE THE ACCEPTANCE OR REJECTION OF PLACED MATERIALS.
 - 5. GRANULAR 'A' AND GRANULAR 'B' TYPE II TO MEET OR EXCEED OPSS 1010 AND SHALL BE QUARRIED BEDROCK OR RECYCLED MATERIAL.
 - 6. GRANULAR 'A' SHALL BE PLACED TO A MINIMUM THICKNESS OF 300 mm AROUND ALL STRUCTURES WITHIN PAVEMENT AREA. ANY AREAS WITHIN THE R-O-W- WHICH REQUIRE FILL IN EXCESS OF 300
 - m ARE SUBJECT TO COMPACTION TESTS AND SUCH TESTS MUST SHOW A MIN. COMPACTION OF 95% S.P.D. AT ALL DEPTHS. ALL GRANULAR FOR ROADS SHALL BE COMPACTED TO A MINIMUM OF 98%
 - STANDARD PROCTOR DENSITY AND TO THE SATISFACTION OF THE GEOTECHNICAL ENGINEER.
 - 9. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'B' COMPACTED IN MAXIMUM 300 mm LIFTS. 10. THE BEDDING AND COVER FOR ALL SERVICES SHOULD BE 150 mm OF
 - GRANULAR 'A' COMPACTED AT 95% STANDARD PROCTOR DENSITY. 11. ALL OF THE EXISTING SOIL CAN BE REUSED IN THE TRENCHES, PROVIDED
 - THE SOIL IS MOIST. WHERE THE TRENCHES WILL BE WITHIN THE ROADWAYS THE TRENCH BACKFILL MUST BE RAMPED DOWN IN 300 mm LIFTS TO 95% STANDARD PROCTOR DENSITY
 - WHERE THERE ARE TRENCHES WITHIN THE ROADWAYS. THE TRENCH SURFACE MUST BE RECOMPACTED TO 95% STANDARD PROCTOR DENSITY BEFORE PLACING ANY GRANULARS.
 - 13. ALL HOT LAID ASPHALTIC CONCRETE SHALL MEET OR EXCEED OPSS 1150. 14. THE ASPHALT TO BE PLACED AND COMPACTED IN 2 LIFTS TO 96% MARSHALL DENSITY. THIS IS TO ALLOW HAVING A PAVED STREET BEFORE CONSTRUCTION OF THE HOUSES, FOLLOWED BY A SECOND COURSE NEAR THE END OF CONSTRUCTION.
 - ASPHALT WEAR COURSE SHALL NOT BE PLACED UNTIL THE VIDEO INSPECTION OF SEWERS Sc NECESSARY REPAIRS HAVE BEEN CARRIED OUT TO THE SATISFACTION OF THE ENGINEER.
 - 16. A GEOTECHNICAL ENGINEER IS TO INSPECT ALL PAVEMENT STRUCTURES.

DRIVEWAYS

- RESIDENTIAL DRIVEWAY APRONS SHALL BUTT UP TO CONCRETE CURB. DRIVEWAY ENTRANCES SHALL BE AS PER OPSD 351.010. - 3. COMPACTION OF SUBGRADE SHALL BE INSPECTED BY A GEOTECHNICAL ENGINEER PRIOR TO PLACEMENT OF GRANULAR BASE.

- <u>UTILITIES:</u> REFER TO COMPOSITE UTILITY PLAN FOR MORE DETAILS AND NOTES TRANSFORMERS AND PEDESTALS SHALL BE LOCATED BETWEEN HOUSES AND
- TOWNHOUSE BUILDING BLOCKS TO AVOID ENCUMBERING AND PREVENTING THE PLANTING OF TREES. ALL PEDESTALS TO BE INSTALLED IN LINE WITH HYDRO TRANSFORMERS OR ON SIDE OF TRENCH AWAY FROM ROAD.
- - THE BASE OF A HYDRO TRANSFORMER MUST BE LOCATED A MINIMUM OF 2.0 m FROM THE EDGE OF A DRIVEWAY.
 - REQUIREMENTS FOR PROTECTIVE BOLLARDS AT TRANSFORMERS SHALL BE DETERMINED BY HYDRO ONE ON A CASE BY CASE BASIS. SERVICE LATERALS MUST BE LOCATED A MINIMUM OF 3.0 m FROM THE
 - BASE OF A HYDRO TRANSFORMER.
 - HYDRO TRANSFORMER AND SIDEWALKS ARE TO BE LOCATED ON OPPOSITE SITE OF THE R-O-W- WHERE POSSIBLE.
 - OF THE R-O-W- WHERE POSSIBLE.
 - 9. AT CATCH BASIN AND HYDRANT LOCATIONS, THE GAS MAIN SHALL HAVE A MINIMUM 0.5 m CLEARANCE FROM STRUCTURES. 10. JOINT USE TRENCH TO HAVE A MINIMUM COVER AS PER GOVERNING
 - AUTHORITY. 11. PRIMARY HYDRO DUCTS & COMMUNICATION DUCTS (ENCASED) TYPICALLY REQUIRED ON ONE SIDE OF R-O-W- ONLY. PROVIDE 1.0 m COVER ON ALL CONCRETE ENCASED DUCTS.
 - 12. 1.5 m CLEARANCE TO BE MAINTAINED AROUND WATER SERVICE POST. 13. STREET LIGHT CABLE SHALL BE PLACED IN JOINT USE TRENCH. STREET LIGHT CABLE SHALL BE AT SAME OFFSET AS STREET LIGHTS WHEN JOINT USE TRENCH NOT CONSTRUCTED.
 - 14. TRAFFIC DUCT ALTERNATIVE PLACEMENT LOCATIONS ARE: 1-JOINT USE TRENCH LOCATION, OR
 - 2-SAME OFFSET AS STREETLIGHT POLES IN A SEPARATE TRENCH. 15. FOUR PARTY TRENCH OPTION REQUIRES THE AGREEMENT OF ALL UTILITIES. 16. THE DEVELOPER SHALL SUPPLY AND INSTALL DUCTS FOR UTILITY CROSSINGS AT INTERSECTIONS AS REQUIRED.
 - WATER, STORM AND SANITARY SERVICE LATERALS; UTILITY STRUCTURES; GRANULAR BASE AND SUBBASE; WATERMAIN COMMISSIONING; SEWER TESTING AND VIDEO INSPECTION: ASPHALT FIRST LIFT; JOINT USE UTILITY TRENCH; GAS MAINS; UTILITY LOT SERVICES; STREET LIGHTING AND TREES. ASPHALT SURFACE COURSE AFTER 50% OF THE HOUSES HAVE BEEN CONSTRUCTED PRESCRIBED ORDER OF INSTALLATION MAY VARY DEPENDING UPON CIRCUMSTANCES AS APPROVED BY AN AUTHORIZED REPRESENTATIVE
 - 17. PRESCRIBED ORDER OF INSTALLATION: SEWERS AND WATERMAINS; HYDRANTS; -18

<u>GRADING SPECIFICATIONS:</u>

- 1. ALL GRADING TO CONFORM TO VILLAGE OF CARDINAL STANDARDS AND SPECIFICATIONS.
- NO EXCESS DRAINAGE TO BE DIRECTED TOWARDS ADJACENT PROPERTIES. A FLAT AREA HAVING A WIDTH OF 0.6 m SHALL BE PROVIDED AT THE BOUNDARY LIMITS OF ADJACENT DEVELOPED PROPERTIES IN ORDER THAT THE EXISTING BOUNDARY ELEVATIONS WILL BE MAINTAINED.
- GRADING WITHING LOTS GRADING SHALL BE 2% TO 7%.
- ALL SWALES SHALL BE 0.15-0.30 m DEEP WITH 3: 1 SIDE SLOPES UNLESS OTHERWISE INDICATED. THE MINIMUM LONGITUDINAL SLOPE IS 1% AND 1.5% WITH INSTALLATION OF SUBDRAIN OR WITHOUT. RESPECTIVELY.
- ALL EXTERNAL SITE AREAS DISTURBED BY THE ACTIVITIES OF THE CONTRACTOR SHALL BE RESTORED TO EXISTING CONDITION OR BETTER AND TO THE SATISFACTION OF THE TOWN. GRASSED AREAS SHALL BE RESTORED BY PLACING 150mm TOPSOIL AND ACTIVELY GROWING No.1 NURSERY SOD.
- TOPSOIL IN FILL AREAS TO BE STRIPPED. ALL FILL MATERIAL SHALL BE APPROVED FOR SUITABILITY BY THE GEOTECHNICAL ENGINEER PRIOR TO ANY FILLING OR REUSE OF EXCAVATED MATERIAL. APPROVED FILL MATERIAL SHALL BE COMPACTED TO THE SATISFACTION OF THE GEOTECHNICAL ENGINEER.
- PAVEMENT GRADES (MINIMUM 0.50%, MAXIMUM 5%) 10 SLOPES IN LANDSCAPE AREAS AND ON BERMS SHALL NOT EXCEED 3 HORIZONTAL TO 1 VERTICAL WITH MAXIMUM VERTICAL ELEVATION NOT IN EXCESS OF THE APPLICABLE VILLAGE STANDARDS.
- 11. GRADING WITHIN 2 m OF THE BUILDING SHALL BE MAINTAINED AT 2% SLOPE OR HIGHER. 12. ALL ROOF DOWNSPOUTS SHALL DISCHARGE TO THE GROUND ONTO SPLASH
- PADS
- 14. UNLESS OTHERWISE SHOWN ON THE GRADING AND/OR EROSION SEDIMENT CONTROL PLAN, PROPOSED STOCKPILING OF TOPSOIL DURING CONSTRUCTION WILL BE REQUIRED THE DEVELOPER'S ENGINEER TO PROVIDE THE LOCATION AND HEIGHT OF STOCKPILED TOPSOIL. TOPSOIL MUST BE STABLE AND SEEDED TO ESTABLISHED A TEMPORARY VEGETATIVE COVER AND TO PREVENT

STREET LIGHTS AND SIDEWALKS ARE TO BE LOCATED ON OPPOSITE SIDES

2. EXISTING ELEVATIONS WITH ABUTTING PROPERTIES SHALL BE MATCHED.

- 13. ALL FILL (NOT ON MUNICIPAL ROADWAY) SHALL BE PLACED AND COMPACTED TO 95% STD. PROCTOR DENSITY M MAXIMUM 0.20m LIFTS TO SUBGRADE. FILL SHALL BE COMPACTED TO 95% SPD AS DIRECTED BY THE CONSULTANT

EROSION

15. ALL TOPSOIL STOCKPILE LOCATIONS ARE SUBJECT TO VILLAGE APPROVAL.

<u>RETAINING WALLS</u>

- RETAINING WALL TYPE TO BE SPECIFIED BY PROJECT LANDSCAPE ARCHITECT AT LOCATIONS, AS SPECIFIED ON THE GRADING PLAN.
- 2. ALL RETAINING WALLS SHALL BE ARMOUR STONE UNLESS NOTED OTHERWISE. ALL TYPICAL RETAINING WALLS GREATER THAN 1.0 m HEIGHT ARE TO BE
- DESIGNED, APPROVED AND STAMPED BY A STRUCTURAL ENGINEER.
- FENCES OR RAILINGS ARE REQUIRED FOR WALLS HIGHER THAN 0.6 m.

MISCELLANEOUS

- ALL STORM AND SANITARY SERVICES TO BE EQUIPPED WITH APPROVED BACKWATER VALVES.
- WATER AND SANITARY SERVICE CONNECTIONS SHALL NOT BE UNDER A DRIVEWAY
- EXACT ELEVATIONS FOR CONNECTIONS SHALL BE VERIFIED BY CONTRACTOR AND APPROVED BY VILLAGE AUTHORITY. COORDINATE WITH VILLAGE WATER WORKS FOR ALL SERVICE CONNECTION
- 4. PRIOR TO ANY FILLING OR REUSE OF EXCAVATED MATERIAL. APPROVED FILL MATERIAL SHALL BE COMPACTED TO THE SATISFACTION OF THE GEOTECHNICAL ENGINEER.
- TRAFFIC SIGNS SHALL BE APPROVED BY THE VILLAGE OF CARDINAL 5.
- REFER TO LANDSCAPE PLAN AND EROSION AND SEDIMENT CONTROL PLAN FOR MORE RELATED SPECIFICATIONS.
- REFER TO PUMPING STATION DRAWINGS FOR RELATED DETAILS AND SPECIFICATIONS.

UNITED COUNTIES OF LEEDS AND GRENVILLE PART OF LOT 7, CONCESSION ' GEOGRAPHIC TOWN OF EDWARDSBURGH TOWNSHIP OF EDWARDSBURGH/CARDINAL COUNTY OF GRENVILLE

LEGAL INFORMATION LEGAL INFORMATION PROVIDED BY IBW SURVEYORS. PROJECT # A-026727. PLAN I5R-12193.

TOPOGRAPHIC INFORMATION TOPOGRAPHIC INFORMATION PROVIDED BY IBW SURVEYORS.

GEOTECHNICAL REPORT

REFER TO GEOTECHNICAL SUBSURFACE INVESTIGATION REPORT No. 21C350, DATED MAY 31, 2021, PREPARED BY ST. LAWRENCE TESTING & INSPECTION CO. LTD.. INFORMATION PRESENTED IN THESE DRAWINGS HAS BEEN INTERPOLATED FROM THE GEOTECHNICAL REPORT AND ACCURACY IS NOT GUARANTEED CONTRACTORS ARE ADVISED TO READ THE GEOTECHNICAL REPORT

USE AND INTERPRETATION OF DRAWINGS UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION" THIS DRAWING SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

AND ASSUME THEIR OWN CONCLUSIONS.

TOWNSHIP COMMENTS - 10-18-23 TOWNSHIP COMMENTS - 06-30-23 FOWNSHIP COMMENTS PEER REVIEW COMMENTS OWNER / APPROVAL REVISION / ISSUE PREPARED BY: Mongi Mabrouk P.Eng. Phone: 613-896-9170 Email: eng.services.ca@gmail.com ENGINEERING PROJECT NAME AND ADDRESS: LOCKMASTER'S MEADOW SUBDIVISION COUNTY ROAD No. 22 (SHANLY RD), CARDINAL, ON APPLICANT Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata, ON 613-282-5601 TITLE: **GENERAL NOTES &** SPECIFICATIONS

SCALE: VARIES	DRAV
DRAFTED BY:	
PROJECT No.: 0114	
DATE: 12/01/2023	















d L	2. Tee conne	ection 3	3. Three way	junction	
	+				
	5 Straight t	brough	6 Dead of	and	
			U. Deud e		
	+/		H: 1V max		max /2 min Omm
า	8. 45° be	end	Sectior	ו	•
E HOLE	IN THE WALL	IN PRECAS	ST RISER SEC	TIONS	
1-4	No 5 and 6	No 8	N	p.7	
			Inlet Hole	Outlet Hole	
700	860	780	700	860	
860	1220	960	860	1170	
220	1485	1220	1220	1485	
485	2020	1760	1485	2020	
930	2450	2300	1930	2450	
470 3085 2730			2470	3085	J
the outlet hole opening for top of benching. MPa. t shall be given wood float finish, channel shall be given steel trowel finish. e as specified. t that are 1200mm in diameter with a uniform channel for 200 or 250mm pip acturer with standardized benching slope and channel orientation.					



4.21.2024 114-details-d1-d.





















SCHEDULE "G"

LOT GRADING AND DRAINAGE

For the lands set out in Schedule "A," the Owner agrees to implement and maintain the objectives and criteria of the Grading and Drainage Plan (GR-1 to GR-3 inclusive), prepared by Advance Engineering, stamped and dated July 31, 2024.

For the lands set out in Schedule "A," the Owner agrees to implement and maintain the objectives and criteria of the Earthwork Plan, prepared by Advance Engineering, stamped and dated June 18, 2024.

For the lands set out in Schedule "A," the Owner agrees to implement and maintain the objectives and criteria of the Subsurface Geotechnical Report, prepared by St. Lawrence Testing, stamped and dated May 31, 2021.

ROUGH LOT GRADING

Rough lot grading shall be completed for all lots prior to acceptance of the Works by the Municipality and the release of all security. Such grading may be completed in stages if approved by the Municipality. Nothing contained herein shall prevent the owner from stockpiling clean fill and/or topsoil on any lot so long as such storage does not interfere in any way with the drainage of water within the Subdivision.

EXCESS SOIL MANAGEMENT

The Owner shall be responsible for ensuring that any material removed from the site meets the requirements of O. Reg. 406/19 On-Site and Excess Soil Management.

MAINTENANCE OF LOT GRADING AND DRAINAGE

These restrictions shall run with and be binding upon the Lands. The Grantees, in respect to the herein described lands, shall maintain proper grades and levels thereon in accordance with the approved Lot Grading and Drainage Plan, prepared by Advance Engineering, stamped and dated February 6, 2024 in order to ensure that no back yard, side yard, or front yard accumulation of storm water occurs on the land or neighbouring lands. Future maintenance of drainage Works shall be completed by the Municipality and costs charged back to benefiting properties as a local improvement.

In the event that the Grantees do not maintain the proper grades and levels herein referred to, or in the event that they impede any drained system or pattern on the herein described lands or neighbouring lands, they shall be responsible for the curing of any problems resulting thereto and costs arising out of same.

Attached:

- Grading and Drainage Plans
 - Phase 1 (GR1) July 31, 2024
 - Phase 2 (GR2) July 31, 2024
 - o Details (GR3) July 31, 2024
- Earthwork Plan (EW1) June 18, 2024
- Geotechnical Subsurface Investigation Report May 31, 2024



4-2-grad-500.dw(

		LEGEND:
		LOT NUMBER
		LOT LINE
		CULVERT
		PROP. RETAINING WALL
		PROPOSED TERRACING
		TOP OF SLOPE
		FLOW DIRECTION PROPOSED SURFACE DRAINAGE PATTERN
		PROPOSED GRADING ELEVATION
		EXISTING GRADE ELEVATION
		PROPOSED SWALE
		CURB & DEPRESSED CURB
EX.SAN		PROPOSED DRIVEWAY
		PROPOSED CATCHBASIN
		MANHOLE OPSD 701.010
		PERFORATED PIPE
		ELBOW CATCHBASIN STD S31
		PROPOSED SANITARY SEWER
ω		PROPOSED STORM SEWER
80 L		BUILDING INFORMATION
₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩		GARAGE ELEVATION (8 FINISHED FLOOR ELEVATION 8
¢ 20 65.48		TOP OF FOUNDATION ELEVATION
2 2 2 4 . H		NUMBER OF RISERS WALKOUT UNITS
		REQUIRE SPECIAL DESIGN
SHED		
WETAL METAL		
		8 PLANS UPDATE – WEST DRAINAGE
		6 PLANS UPDATE
21		5 REVIEW COMMENTS - 06-30-2023
		4 REVIEW COMMENTS – BERM LAYOUT 1 OWNER / APPROVAL
		No. REVISION / ISSUE
		PREPARED BY:
		Phone: 613-896-9170
FUTURE		
		ADVANCE 2 1 ENGINEERING 8
STIN STIN		PROJECT NAME AND ADDRESS:
EXI		LOCKMASTE
		MEADOW SUBDI
		COUNTY ROAD No. 22 (SH
B B B B B B B B B B B B B B B B B B B		Edwardsburgh Developments I to
		434-300 Earl Grey Drive
		613-282-5601
<u>−−−−−−−−−−−−−−−−−−−−−−−−−−−−−−−−−−−−</u>		
84.44 84.44		GRADING
		PH-1
	_	SCALE: DRAWING NO
	0 10 20	DRAFTED BY:
		PROJECT No.:
		0114



DATE: 07/31/24



14-2-grad-500.dv

<u>LEGE</u>	END:
LUI	
PROF	Perty limit
LOT	LINE
SETB	ACK LINE
CULV	ERT
PROP	. RETAINING WALL
CONT	OUR —
PROP	osed terracing
TOP	OF SLOPE
EXIST	MAJOR OVERLAND
PROP	OSED SURFACE DRAINAGE PATTERN
HIGH	POINT
EXIST	ING GRADE ELEVATION
TOP	OF GRATE ELEVATION
PROP	OSED SWALE
SWAL	e invert
CURB	& DFPRESSED CURB
	DC
PROP	OSED DRIVEWAY → A 1.5r
PROP	OSED CATCHBASIN
PROP	OSED CATCHBASIN
MANH	ULL UFOU /UI.UIU
IEE (CATONIADIN 210 230
PERF	ORATED PIPE
FLBO	W CATCHBASIN STD S31
PROP	OSED SANITARY SEWER
PROP	OSED WATERMAIN
PROP	CHAINLINK FENCE -
<u>BUILD</u>	ING INFORMATION
GARA	GE ELEVATION
FINIS	HED FLOOR ELEVATION
TOP	OF FOUNDATION ELEVATION
NUME	BER OF RISERS
WALK	OUT UNITS
REQU	WITH FILL EXCEEDING 1.2m IRE SPECIAL DESIGN
GARA	GE ELEVATION
8	PLANS UPDATE – WEST DRAINAGE
7	PLANS UPDATE
6	PLANS UPDATE
5	REVIEW COMMENTS - 06-30-202
4	REVIEW COMMENTS - BERM LAYO
1	OWNER / APPROVAL
NO.	REVISION / ISSUE
PREP	ARED BY:
Мо	ngi Mabrouk P.Eng.
Pnc Ema	ail: eng.services.ca@gmail.com
L	
PRO.	IFCT NAME AND ADDRESS!
	LOCKMAST
M	IFADOW SUBE
СО	UNTY ROAD No. 22 (S
	CARDINAL, C
יחם	
APPL	י ו אודעוי
Edw	ardsburgh Developments Ltd.
434-	300 Earl Grey Drive
Kana	ata, ON
640	

TITLE:	
GRAD DRAINA	OIN GE
PF	1-2
scale: 1:500	DRAWING
DRAFTED BY:	
PROJECT No.: 114	6
DATE: 02/06/24	

0 10 20





DRAINAGE WEST LAND PROFILE STA. -0+015 TO STA. 0+190 SCALE: H = 1:500 / V = 1:50

	CULVERT SCHEDULE						
ID	DIA (mm)	LENGTH (m)	SLOPE	MATERIAL	INV. IN	INV. OUT	COVER (m)
C1	450	9.1	-0.50%	REINFORCED CONCRETE	78.56	78.60	0.50 m
C2	450	13.5	-0.50%	REINFORCED CONCRETE	78.60	78.67	0.40 m
C3	600	14.5	-5.00%	REINFORCED CONCRETE	78.60	79.32	0.95 m
CLVT 1	750	65.5	1.00%	REINFORCED CONCRETE	81.39	80.74	<pipe_data:pipe_cover></pipe_data:pipe_cover>
CLVT2	750	65.9	1.00%	REINFORCED CONCRETE	80.74	80.08	<pipe_data:pipe_cover></pipe_data:pipe_cover>



14-2-arad-500.dwa





* DISTANCES ARE IN MILLIMETRE
<u>CHANNEL SECTION</u>
SCALE: 1:50



ELEVATION TABLE LEGEND						
NUMBER	MINIMUM ELEVATION	MAXIMUM ELEVATION	COLOUR			
1	-0.872 m	-0.150 m				
2	0.150 m	1.000 m				
3	1.000 m	2.000 m				
4	2.000 m	4.000 m				

PHASE 2: 36 LOTS _____ PHASE 1: 59 LOTS

NOTE: 1 – CUT/FILL DEPTH IN METRE 2 – ELEVATION GRID: 10 m x 10 m 3 – ELEVATIONS IN RIGHT-OF-WAY: DATUM SURFACE 4 – LOT GRADING: FINISHED GRADE 5 – EXCESS SOILS MANAGEMENT SHALL COMPLY WITH O. REG. 406 (10 ONSITE AND EXCESS SOIL MANAGEMENT CONTRACTOR 406/19 ONSITE AND EXCESS SOIL MANAGEMENT. CONTRACTOR SHALL FILE A NOTICE AT RPRA "EXCESS SOIL REGISTRY" PRIOR TO EXCAVATION.



1	TOWNSHIP REVIEW (06-14-2024)	06/18/2
1	OWNER / REVIEW	02/06/2
No.	REVISION / ISSUE	DATE MM/DD/Y1
PREP	ARED BY:	
Mor Phoi Ema	ngi Mabrouk P.Eng. ne: 613-896-9170 il: eng.services.ca@gmail.com	
	Г	_

PROJECT NAME AND ADDRESS:

CARDINAL

LOCKMASTER'S MEADOW

APPLICANT:

Edwardsburgh Developments Ltd. Address

TITLE:

EARTHWORK PLAN

SCALE:

DRAFTED BY:

PROJECT No .:

DATE: 06-18-24

DRAWING	No.:
---------	------

⊢ ,



P.O. Box 997, Cornwall, ON, Canada K6H 5V1 814 Second Street W., Phone (613) 938-2521 E-mail: slt@ontarioeast.net Fax (613) 938-7395

May 31, 2021

Mr. David Simpson Edwardsburgh Development Inc. 434-300 Earl Gray Dr. Kanata, ON K2T 1C1

RE: Lockmaster's Meadow, Cardinal, ON Geotechnical Subsurface Investigation Report No. 21C350

Dear Mr. Simpson:

In accordance with verbal and e-mail instructions received from you, this report is submitted, outlining the results of a geotechnical subsurface investigation carried out at the site on Shanley Rd, South of the CN Main Line, in Cardinal, ON

A) DESCRIPTION OF FIELD WORK & STRATIGRAPHY

After receiving the approval, we sent you a plan showing the proposed borehole locations. We then contacted Ron Jason Surveying to lay out the boreholes in the field.

After the stakes were placed in the field by Ron Jason Surveying, we called for service locates. Drilling and sampling took place on April 7, 2021 using a CME 55 track mounted auger drill from E.O.D.D. of Hawkesbury, ON. Supervision was by the undersigned geotechnical engineer. Report No. 21C350 Continued

Page 2

A total of 7 boreholes were put down as noted on the sketch. Most boreholes were put down to 4.6m. or to refusal if above this. One borehole was advanced to 5.18m. The borehole next to Shanley Rd. was advanced to 2.1m. The boreholes were advanced by split spoon sampling. Standard Penetration tests were conducted along with the split spoon sampling. The recovered samples were placed in glass jars for later detailed lab classification and washed gradation tests. The results are found in the attached borehole logs and washed gradation sheets.

We had one of our staff return on April 8, 2021 to measure the water levels in each borehole.

A sketch is attached showing the borehole locations. Also attached are a topographic map of the whole area and a colour map showing the location in relation to the Town of Cardinal.

B) STRATIGRAPHY

The stratigraphy is fairly similar throughout.

The general stratigraphy is a brown, moist, stiff clayey silt overlying a brown to grey, moist, compact to dense silty sand and gravel till.

There is a brown, moist loose silt and sand stratum noted at Boreholes 4 and 7 below the topsoil. This extends to 0.91m. at Borehole 4 and 1.58m. at Borehole 7.

Report No. 21C350 Continued

Page 3

The clayey silt is noted throughout the property below the topsoil at the other boreholes and below the silt and sand at Boreholes 4 and 7. The clayey silt is mainly stiff, but is occasionally hard, at Boreholes 5 and 6.

Underlying the clayey silt is a brown, moist, compact to dense silty sand and gravel till. This was noted at 2.7m. at Borehole 1, 3.7m. at Borehole 2, 2.9m. at Borehole 5 and 2.6m. at Borehole 6. The sand and gravel till was not reached at Boreholes 3 and 4.

Borehole 7 was only advanced to 2.1m. for the pavement design information, to connect the new street on to Shanley Rd.

For the specific stratigraphy at each borehole, the borehole logs should be referred to.

C) GEOTECHNICAL DISCUSSION

1) General

It is our understanding that it is proposed to build a residential subdivision at this property. It would appear to be 94 lots in the prepared plan.

2) Services

The soil throughout is a Type 2 to Type 3 soil from a trench perspective. As such, normal trenches can be used. The bottom 1.2m. can be vertical. Above 1.2m., the side slopes must be cut back to a 1 to 1 side slope.

Report No. 21C350 Continued

Page 4

The bedding and cover for all services should be 150mm. of Granular "A" compacted at 95% Standard Proctor Density.

All of the existing soil can be reused in the trenches, provided the soil is moist. Where the trenches will be within the roadways, the trench backfill must be ramped down in 300mm. lifts to 95% Standard Proctor Density.

3) Roadways

Where there are trenches within the roadways, the trench surface must be recompacted to 95% Standard Proctor Density before placing any granulars. Where there is topsoil at the surface, this should be removed over the full width of the roadway.

The granular subbase should consist of 375mm. of Granular "B" Type 2 and compacted to 100% Standard Proctor Density. The granular base should consist of 150mm. of Granular "A", compacted to 100% Standard Proctor Density.

The asphalt should consist of 75mm. of HL3, placed and compacted in 2 lifts to 96% Marshall Density. This is to allow having a paved street before construction of the houses, followed by a second course near the end of construction.

4) House Foundations

The bearing capacity at Boreholes 1, 2, 3 and 7 is in the 50KPa S.L.S. range. The bearing capacity at Boreholes 4, 5 and 6 is in the 100Kpa S.L.S. range. St. Lawrence Testing & Inspection Co. Ltd.

Report No. 21C350 Continued

Page 5

Where the bearing is 75KPa S.L.S. or higher, standard footings will be applicable. The site seismic factor is Site Class D throughout.

It is recommended that a bearing capacity evaluation be done of each house when the footings are being dug in order to provide the proper recommended footing size.

D) CONSTRUCTION CONTROL

In order to ensure that the recommendations of this report are adhered to, it is recommended that our firm be retained to inspect, test, and report accordingly.

Respectfully submitted ST. LAWRENCE TESTING & INSPECTION CO. LTD.

G.G. McIntee, P. Eng. GGM:mhm



Attachments

Attachment "C" Site Location Map





.

.

Page 140 of 465

Attachment "A" Draft Plan of Subdivision



4 OF 6

Bt. Lawrence Teating & Inspection Co. Ltd. OFFICE BOREHOLE RECORD CUIENT Edwardsburgh Development Inc. BOREHOLE NO. 21C350 CUIENT Edwardsburgh Development Inc. BOREHOLE NO. 1 LOCATION Shanley Rd. South of CN Rail Cardinal, ON CASING HE Auger DATE OF BORING April 7, 2021 DATE OF WL READING April 8, 2023 OATUM SOIL PROFILE SAMPLES LAB TEST No E E E E E No E E E E E E

н	NOI H	SOIL DESCRIPTION	101	SNO	NO		E E	Å	ĽF.	AATORV STS	CHIMED				LA	18	1691 160000																	
DEPT	ELEVAT		STRAL.	WATE	CONDIT	JYPE	NUMB	RECOVI	N - VAL							W	A	TE	R C W	201 'P	NT	ENT	8	AT W	TEF	18E	RG	W	МЛ "L	rs.				
$\left \right $				\vdash			-			┼	DYNAMIC PENETRATION TEST BLOWS PER FOOT K																							
-0-		200mm. Topsoil				-					ŕ	Π	Π	Π	Τ	Π	$\prod_{i=1}^{2}$	Î	Π	Π	Π	T	4	Î	Π	Π	Π	TT	Î	Т	Π	Π	Π	80
Ħ		Clayey Silt				[ļ		ļļ		ļ					F
		Brown, moist, still									ł			ľ															I					Π
							L				h	┢			┥	-				╉	┝	╢		H			╞		Ħ		╈	┝╋		┢
Н				78												1															ĺ			
																								İ		Ì								Н
												T	Π		Π		T		Π	Π		Π	Π	Π	Π	T			Π					Η
匚												l			ļ				ĺ															П
											H	+		Ļ			╞	Ц	-	ļļ	╉	╢	Ц	Ц	╢	Ц	+		╢	Н	Н		ļļ	Ħ
					\	1										ł																		Н
┠╌┥					XI	ss	1	100	3												Į			Í				F		$\ $				Н
- 2-				-	\mathbb{A}						H	$\left \right $		╢	╉	₩	╉	╢	╉	╢	╉	╢	╢	╢	╫	╢	╇	┢╋	╂┼	₩	H	+	╫	Н
				¥	<u> </u>	ĺ																			Ιİ									П
																										$\left \right $			Ì					Ц
				ŀ	+						H	Π	╉	╢	+	╢	╉	╢	ł	┢┝	┢		┟┟	╢	łł	┼┥	Н	╈	╽	Ħ	╫	╈	₩	日
						ĺ																												Н
	2.74	Sand and Gravel Till																																Н
- 3		compact to dense		ħ	7	Ť		- 1			Ħ		t	ľ	Ť	Ì	Î	Ħ	t	Ħ	T	T	I	Ħ	Π	ÌÌ	T	T			ŤÎ	T	Π	П
					VI		2	75	20																		1							Ħ
					ΧĹ	33	2	, , , , , , , , , , , , , , , , , , ,	50		L																							Н
				[\sum								Ì			Π	Π	ĺ]							Н
			ĺ	ľ								ł																						P
							~					ļ			ļ		L		ļļ					4		ļļ	╢	Ц		ļļ	╢	Ц	4	Ц
н																				ļ													Ì	
																									ł									
				Ļ		_				ļ		ļ	H		╢	+		+	╟		Н	╢	┦		-		H	┦	$\frac{1}{1}$	╟	₩	╢	+	Η
	4.57	Termination of																													$\left \right $			H
		borehole																ľ																
-5 -	1			┢	\rightarrow	_+				ł	+	╞	╢		╢	$\left \right $	╟	+	╟	╢		╢	H	╢	╢	╟	╟	╢		╟	╟	╢	╢	Н
																																		4
																											$\ $							7
				┢			-			ł	AF	PE	LL Ent	L) XIX	((L	LL.	Ļ	Ļ	Ц	Ц	11	11	11		_		11	Ц			<u></u>	<u>ن ا</u>	1
				Pa	igę	142	2 df	465	5		_		_																					

St. Lawrence Testing OFFICE BOREHOLE RECORD & Inspection Co. Ltd. REPORT NO. _21C350_ CLENT <u>Edwardsburgh Development Inc.</u> BOREHOLE NO. _2 LOCATION Shanley Rd. South of CN Rail Cardinal, ON CASING <u>HF</u> Auger DATE OF BORING April 7, 2021 DATE OF WL READING April 8, 2021 DATUM ___ SOIL PROFILE SAMPLES RESULTS LABORATORY TESTS PERFORMED LAB TEST DEPTH ELEVATION WATER CONDITIONS STRAT. PLOT CONDITION N - VALUE RECOVERY NUMBER OEPTH TYPE SOIL DESCRIPTION WATER CONTENT & ATTERBERG LIMITS. WP W WL DYNAMIC PENETRATION TEST BLOWS PER FOOT. 40 20 n 230mm. Topsoil Clayey Silt Brown, moist, stiff, with some sand below 3.Om. 11 Ŵ

							1			l	[]				Ш
			X	SS	1	75	3								
2															
			X	SS	2	100	11								
3.68	Sand and Gravel Till Brown, moist, silty,														
	compact to dense														
4.57	Termination of ` borehole	-													

Page 143 of 465

3

4

5

APPENDIX
St. Lawrence Testing & Inspection Co. Ltd.

OFFICE BOREHOLE RECORD

REPORT NO. _210350

	BOREHOLE NO	3
--	-------------	---

CUENT Edwardsburgh Development Inc. LOCATION Shanley Rd. South of CN Rail Cardinal, ON _____ CASING HF Auger

DATE OF BORING April 7, 2021 DATE OF WL READING April 8, 2021 DATUM

			SOIL PROFILE				5	SAMP	LES		[ନ LAB TEST RESULTS																			
	z			10	ş	N		G	2	ц	ATORY TTS RMED				LA	B					TE	ST					R	ESI	JLT	S	i
DEPTH	EVATIO	ОЕРТН	SOIL DESCRIPTION	RAT. PL	VATER	ONDITIC	TYPE	UMBER	ECOVEF	- VALU	LABOR TES PERFO					W	IAT	ER	CC NP	NT	EN	T 8	AT W	TEP	BE	RG	UM WL	ITS.			
-	EL	-		STI	CO ^	ö		2		z									-				-0-		PCC	EO					
-0-												0	тт	DY TT		mc TT	2					ייי דד		т. ТТ				。 11	11	П	<u>eo</u>
			230 mm. Topsoil Clavey Silt																												
			Brown, moist, stiff																		Ì										Ш
			becoming grey below 3.3m.		70					<u>.</u>			╟	╢	╢	μ	╢	╂	+	+	╟	╢	╟	₩	H		╢	₩	╢	Н	╢
			5.6.1		.70																										IP
					<u> </u>																										ĮΠ
-1-						-						╉	╟	ti	1	+	ľ	╢		╋	┢┿	Ħ	ÌÌ	╞┿╸			ΪÎ	╢	ÎÌ		ŤΗ
	Ì																ĺ														IЦ
													ļļ				ļļ	Ц		┥								╢	Ц		
						\/																									
						XI	SS	1	100	4																					IЦ
- 2-						A						+	╟╋	H		+		╂	+	+	┢╋	╢	╟	╟	╫	╉	\parallel	╫	H		╫
							•																								Ш
								;	[
														Ħ	T	ļ	Ť	Ħ	T	Ť	Π	ÎÌ	I	Π		T	Π	Î	Ì	Π	Π
-												╢		ļļ	ļļ			ļļ		Ц		Ц		μ	Ц		Ц	╢	Ļ	4	旧
												1																			
						χI	SS	2	75	4																					
					-	А						+	╈	╟		+	╉	╟		ł		╟	ļ.	┢╋╋		╫	$\left \right $	╂╋	┟┼	+	╫
						<u> </u>																									H
																															H
-4-															††	T	T	Ì				T	Π	П	Π	T	1				Π
											ļ				ļļ		-	Ц	Ц		\downarrow			Ш	\parallel	\downarrow	╢		\prod	-	H
						$\overline{\Lambda}$																									
				ĺ		χI	ss	3	100	6																					
-5-				ľ		A					┝	+	╉	╟	╢	╢	╀	╟	╢	$\left \right $	+		Н	┢╋┥	╢	╢	╢	╢	╉	+	怡
	5.1	8	Termination of		ł	+	,																								H
			borehole																												Ш
					ŀ							AF	PPE	N	DIX																
					D -			_ f																							
					Ра⊈	le 1	44	ot 4	65																						

St. Lawrence Testing

OFFICE BOREHOLE RECORD

			e usbaction	0 تى 1). Lt	ci.					-								f	REF	OR	T N	0.		2](<u>3</u>	5()		· _		-
	CLIE	CLIENT <u>Edwardsburgh Development Inc.</u>																_ {	BÔF	REH	OL	EN	0		Ļ	_					-	
	LOC/ DATE	ATION E OF	ORING April 7, 2021	<u> </u>	Rail DATE 0	<u>Ca</u> F WL	rdi: READU	nal, NG	<u>ON</u>	 i1 8	. 202	21				_			_ (_ (cas Dat	UN UM	- î	Н	<u>F</u>	<u>A</u> 1	1g	<u>er</u>					-
F			SOIL PROFILE	,			<u> </u>	SAMP	LES		<u> </u>	Т										_									_	
F	NO			LOT	SN	Z	Τ	Ē	<u>}</u>		ATORY STS BRMED				LA	В					ΤE	ST					F	₹ES	iUL	TS		
DEPTI	ELEVATI	OEPTI	SOIL DESCRIPTION	STRAT. P	WATER	CONDITI	TYPE	NUMBE	RECDVE	N - VALI	LABOR TEL					W	AT	ER	CC NP	ТИС	EN	Τ&	AT W	TEF	RBE	RG	LIN WL	AUTS -	<u>3</u> .			
	╉				+						┠───	L		DY	NAN	IIC	PE	NET	RA	TIO	V 71	ST 4	8L0	WS	PEF	i FO	ŌT.	1	к			
-0			150mm. Topsoil <u>Silty Sand</u> Brown, Moist, loose																													
			Clause Silt		.78																											
		L	Brown, moist, stiff, becoming grey below 3.1m.			-																							++ 			
	- - -					\mathbb{V}	ss	1	100	7																						
- 2																								┦┼								
• -		ĺ							-																							
3-					Ī	$\overline{\mathbf{A}}$	ss :	2	70	9																						
					Z																											
4 -		1																														
	4.5	7	Termination of borehole		ľ																											
5-																																
					Pa	ge	145	5 of	465		A	.PP	ENI	DIX			شمين ا													······		

St. Lawrence Testing Le & Inspection Co. Ltd. OFFICE BOREHOLE RECORD

	CLIENT . LOCATIO	Edwardsburgh Developm N Shanley Rd. South of	ent CN	<u>Inc.</u> Rail	Ca	rdi	nal.	ON										Ri Bi C/	ep(or/ Asi	DRT Eh(NG	OLI	0. E N H	_2 0 F _	 	13 5_ 1g	:5(:e)	0_ 				-
	DATE OF	BORING April 7, 2021	<u> </u>	DATE O	FWL	READI	NG	Apr	i1_8	3,_20	21							D/	ŧΤŲ	М	_										-
		SOIL PROFILE		·	Τ		SAMP	LES		Γ	Τ																				
L =	NOI	=	LOT	SNO	NO		8	RV H	1	AATORY ISTS			i	LA	В				٦	'ES	Τ					ł	RES	SUI	LŤS	;	
DEPT	ELEVAT	SOIL DESCRIPTION	STRAT. I	WATER	CONDIT	TYPE	NUMBI	RECOVI	N - VAL	LABO					W.	ATE	R (W	COI 'P	NTE	ENT	8	AT W	fer	(BE	ĀĠ	UN WI	MIT L -	S.			
			+		[.0	•	DYN	VAN	IIC I	PEN 20	ÊTÊ	ATI	ΙÕΝ	TE	ST : 4	8L0 0	ws	PER	I FO)ÖT.	60	К.	• •		 8(
		180mm. Topsoil <u>Clayey Silt</u> Brown, moist, hard		73																											
				=						-																					
- E																															
					X	SS	1	100	16																						
- <u> </u>																															
· -																															
<u>-</u>	2.92	Sand and Gravel Till Grey, moist, silty, compact to dense		Ī	X	SS	2	65	10																						
				Z					-																						
4-																															
	4.57	Termination of borehole																													
5-																															
- 				Pa	ge	146	of	465		ſ	\PP	EN	DIX										- Anglang	نشد. ا							

St. Lawrence Testing (

OFFICE BOREHOLE RECORD

	CLIENT LOCAT DATE (T 10N 0F B1	Edwardsburgh Developme Shanley Rd. South of DRING April 7, 2021	ent_ CN_	Inc. Rail	Ca	rdi.					21	REPORT NO BOREHOLE NO. CASING <u>HF</u>	210350 6 '_Auger	
\vdash			SOIL PROFILE			T T		SAMP	Apr LES	1.1_8	 		DATUM		
Ξ	ION	н		101	RNS SNO	NO		Æ	<u> </u>	1	AATORY STS ORMED	LAB	TEST	RESULTS	÷
DEP	ELEVAI	DEPT	SOIL DESCRIPTION	STRAT. I	WATE	CONDIT	ΤΥΡΕ	NUMBE	RECOVE	N - VAL	LABOF TE PERFI	WATER W	CONTENT & ATTE	erberg limits. WL	
-0-												DYNAMIC PENET	ATION TEST BLOW	S PER FOOTK 60	ac
			250mm, Topsoil <u>Clayey Silt</u> Brown, moist, hard												
_ 7_					1.16										
								l							
						\mathbb{X}	SS	1	100	10					TIT
	2.64	¥	Sand and Gravel Till Brown, moist, silty, dense												
	3.30	, ,	Sampler and auger		2	Z	SS 2	2	75	50+					
)- - - -															
					Pag	ge	147	of	465		AP	PENDIX	<u></u>	<u></u>	

St. Lawrence Testing OFFICE BOREHOLE RECORD & Inspection Co. Ltd. REPORT NO. _21C350____ CLENT <u>Edwardsburgh Development Inc.</u> BOREHOLE NO. __7_____ LOCATION Shanley Rd. South of CN Rail Cardinal, ON ___ CASING _____ HF_ Auger DATE OF BORING April 7, 2021 OATE OF WL READING April 8, 2021 _____ DATUM ____ SOIL PROFILE SAMPLES RESULTS LABORATORY TESTS PERFORMED LAB TEST ELEVATION WATER CONDITIONS STRAT. PLOT N - VALUE CONDITION RECOVERY NUMBER ОЕРТН DEPTH ТҮРЕ SOIL DESCRIPTION WATER CONTENT & ATTERBERG LIMITS. WP W WL DYNAMIC PENETRATION TEST BLOWS PER FOOT. . .K 40 0 150mm. Topsoil Silt and Sand Brown, moist, loose .61 V SS 40 1 6 1.58 Clayey Silt Brown, moist, stiff SS 2 70 4 2 2.13 Termination of borehole

Page 148 of 465

APPENDIX





ļ



SCHEDULE "H"

STORMWATER MANAGEMENT PLAN & EROSION AND SEDIMENT CONTROL

For the lands set out in Schedule "A", the Owner agrees to implement and maintain the objectives and criteria of the Stormwater Management Report, prepared by Advance Engineering Ltd., stamped and dated July 31, 2024; and the Pond Plan prepared by Advance Engineering Ltd., stamped and dated July 31, 2024.

For the lands set out in Schedule "A", the Owner agrees to implement and maintain the objectives and criteria of the Erosion and Sediment Control Plan, prepared by Advance Engineering, stamped and dated February 6, 2024, during the course of developing the lands in accordance with this Agreement.

NEIGHBOURING PROPERTIES

No disturbance is permitted outside of the subject property boundaries without written permission from the property owner.

STORMCEPTOR

A Stormceptor shall be installed upstream of the detention structure to achieve the required stormwater quality.

Attached:

- Stormwater Management Report July 31, 2024
- Pond Plan (PND) July 31, 2024
- Erosion and Sediment Control Plan (ES1) February 6, 2024
- Stormceptor EF Sizing Report November 12, 2022

Township of Edwardsburgh/Cardinal



STORMWATER MANAGEMENT REPORT

PROJECT: LOCKMASTER'S MEADOW SUBDIVISION (95 Single-Detached Lots)

ADDRESS: COUNTY ROAD 22 (SHANLY ROAD), CARDINAL, ON

PREPARED FOR: Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata, Ontario K2T 1C1

PREPARED BY: Advance Engineering Ltd. Ottawa, ON (613) 986 9170

Date	Revision / Issue
July 31, 2024	SNC Comments about 2 nd Watercourse
June 19, 2024	SNC Review Comments – June 14, 2024
March 05, 2024	Update HGL – Neighbouring Land Drainage
April 03, 2023	SNC Review Comments
December 09, 2022	Peer Review Comments
March 09, 2022	Issued for Subdivision Application

TABLE OF CONTENTS

1.0 INTRODUCTION	1
1.2 SITE DESCRIPTION	1
1.3 BACKGROUND AND LAND USE	
1.3 PROPOSED DEVELOPMENT AND PHASING	
2.0 EXISTING CONDITIONS	
2.1 TOPOGRAPHY / GEOLOGY	
2.1 EXISTING DRAINAGE CONDITIONS	
3.0 PROPOSED STORMWATER MANAGEMENT AN	D DRAINAGE3
3.1 DESIGN CRITERIA	
3.2 QUANTITY CONTROL REQUIREMENTS	4
3.2.1 Runoff Coefficient	4
3.2.2 Rainfall Intensity	
3.2.3 Drainage Areas And Runoff Calculations	5
3.2.4 Allowable Release Rates	5
3.2.5 Proposed On-Site Storage	
3.2.6 Hydrological and hydraulic modelling	
3.2.7 Hydraulic Grade Line	7
3.2.8 Major System	7
3.2.9 Flow Restriction	7
3.3 QUALITY CONTROL REQUIREMENTS	7
3.4 DRAINAGE OF NEIGHBOURING LAND	7
3.4.1 Watershed Delineation and Parameters	7
3.4.2 Peak Flows Estimation	
3.4.3 Culvert Design	
4.0 EROSION AND SEDIMENT CONTROL MEASUR	ES9
4.1 TEMPORARY SEDIMENT CONTROL MEASURES	
4.2 CONSTRUCTION SEQUENCING	
4.3 INSPECTION & MAINTENANCE OF ALL THE EROS	ION AND SEDIMENT CONTROLS
5.0 CONCLUSIONS AND RECOMMENDATIONS	11
List of Appendices: A - Location – Figures B - Geotechnical Report (2021) C - Sto E - Watercourse in Neighbouring Land <u>Related Report:</u> - Site Servicing Report by Advance Engine List of Related Drawings:	ormwater Design D - ICD and Stormceptor Details ering Ltd.
GSP-1&2 General Services Plan PP-1 TO PP-5 - Plan & Profile - Streets A, B, C & Pathway	ES-1 - Erosion and sediment Control Plan PND - Pond Plan

1.0 INTRODUCTION

Edwardsburgh Developments Ltd. has retained *Advance Engineering Ltd.* to provide a stormwater management study, a site grading and drainage plan and an erosion and sediment control plan for the proposed subdivision of 95 single detached lots. The report provides information and assumptions used in the design of the drainage system and storm sewer and should be read in conjunction with the design drawings prepared by *Advance Engineering Ltd.*.The project is located off County Road No.22 (Shanly Road), in the north west part of the village of Cardinal, Ontario. This report is prepared in support of a subdivision application by the applicant.

1.1 OBJECTIVE AND STRATEGY

The objective of the stormwater management study is to develop a strategy that will:

- Identify and mitigate potential stormwater runoff negative impacts on the receiving watercourses from the proposed development area.
- Address the concerns from the review agencies including the Township of Edwardsburgh/Cardinal, the United Counties of Leeds and Grenville, Ministry of Environment, Conservation and Parks (MECP), South Nation Conservation (SNC) and Canadian National (CN) regarding stormwater management solutions for quantity and quality controls as well as erosion and sediment control.
- Design an appropriate site drainage system for safe operational use while minimizing postdevelopment stormwater runoff.
- Determine the location and size of stormwater management components and structures located within the site.

The stormwater management will meet the requirements and criteria set out by South Nation Conservation Authority (SNC), Township of Edwardsburgh/Cardinal, and MECP in terms of applying quantity and quality controls. The City of Ottawa "*Sewer Design Guidelines-2012*" has been used in the drainage design. "*Stormwater Management Planning and Design Manual*" by the Ministry of the Environment, Conservation and Parks (MECP) has been used for stormwater management. The report will cover Phase 1 and Phase 2 of the project.

1.2 SITE DESCRIPTION

The proposed development is on a single parcel of land. It is located off the west side of County Road No. 22, village of Cardinal, Township of Edwardsburgh / Cardinal, Ontario (Figure-1, **Appendix A**). The legal description of the property is: "*Part of Lot 7, Concession 1, Geographic Township of Edwardsburgh / Cardinal, County of Grenville*". The site is bounded as follows:

- County Road 22 (Shanley Road) and three residential dwelling units to the east,
- CN railway to the north,
- vacant agriculture land to the west, and
- residential dwellings to the south.

The subject property is approximately 10.9275 hectares (27 acres) with a rectangular shape of 600 m in length and 180 m in width approximately. Currently, the property is vacant, undeveloped and covered

with short grass and pasture. The property is not currently serviced, however municipal water, sanitary sewers, gas main, telecom and hydro lines have been identified in the immediate area of the site.

1.3 BACKGROUND AND LAND USE

The original draft plan of the proposed subdivision was approved on April 24, 2013 (*File No. 07-T-10005*). In 2021, changes have been applied to the draft plan. A copy of the updated agreement conditions is attached in **Appendix B**.

The site has never been developed and has always been a green field. The current zoning of the subject property is "Residential First Density R1" that allows single family dwellings of lot areas not less than 465 m² and lot frontages not less than 15 m for fully serviced lots.

The site has been surveyed by *Ron M. Jason Surveying Ltd.*. A topographic survey dated April 28, 2021, has been provided by *IBM surveyors*.

A copy of the report outlining the results of the geotechnical subsurface investigation carried out by *St. Lawrence Testing & Inspection Co. Ltd.* is attached in **Appendix B**.

1.3 PROPOSED DEVELOPMENT AND PHASING

The proposed development, as shown in the updated Draft Plan of Subdivision, consists of the construction of paved roadways, sanitary and storm sewers, watermains and utilities (gas, Bell and Hydro) to service the proposed 95 detached lots.

The two phases of the project are:

- Phase 1: comprises 59 lots and a dedicated parkland located in the south side of the property.
- Phase 2: consists of developing the remaining 36 lots in the north side of the subdivision.

The total gross area of phase 1 is 4.74 ha and 2.96 ha of phase 2. There is an open space shown as Block A on the Draft Plan with an area of 3.25 ha where the stormwater management facility will be constructed. An earth berm topped with trees will be constructed in the open space to act as a noise barrier between the subdivision and CN railway.

ROADWAY DESIGN

The subdivision has two road intersections with County Road No. 22 to the east. Two reserved ROWs for future street extensions are located at the south and north-west of the property. A 6 m wide pathway is planned between Street B and County Rd 22.

All subdivision streets (Baslam St, Lockhouse St and Conifer Ln) will be constructed as per the typical road cross-section shown on the Draft Plan. The proposed 20-metre right-of-way will have a 7-metre asphalt pavement and mountable curbs. A sidewalk will be constructed at the subdivision entrances. Roadway pavement structure consists of (from top to bottom) 35 mm asphalt wear course (HL3), 40 mm asphalt base course (HL3), 150 mm base (Granular A) and 375 mm subbase (Granular B – Type

II), with total thickness of 600 mm.

2.0 EXISTING CONDITIONS

2.1 TOPOGRAPHY / GEOLOGY

The site is generally well graded and has a uniform slope from south to the north. The highest grades are located to the south and the lowest grades to the north. Elevations are between 79.00 and 84.50 m (Geodetic Vertical Datum).



According to the geotechnical report *No. 21C350* prepared by *St. Lawrence Testing & Inspection Co. Ltd.* (Appendix B), the stratigraphy of the soil is fairly similar throughout the site. The parcel is covered by a surficial layer of topsoil ranging in thickness between 0.15 m to 0.25 m, underlain by a brown moist and stiff clayed silt ranging in thickness between 2.4 to 3.3 m. Underlying the clayey-silt layer is a brown, moist, compact to dense silty sand and gravel till.

The groundwater table was observed at the seven boreholes at depths ranging from 0.61 m to 1.17 m from existing grade. Groundwater flows toward the St. Lawrence River located approximately 700 m south of the site. Clayed silt and sandy silt have a moderate percolation rate.

2.1 EXISTING DRAINAGE CONDITIONS

The site is located within the sub-watershed of *Sawmill Creek*. There is no storm water sewer in the immediate area of the subdivision.

Under existing conditions, the majority of the site area drains south to north towards the existing unnamed watercourse that outlets into *Sawmill Creek*.

<u>Watercourse 1:</u> the watercourse crosses the site from north to east. It is approximately 170 m long, 4 m wide and 0.5 to 1 m deep. There is a 1400 mm dia. RCP culvert at the inlet (under CN railway, invert elevation is 79.24), and a1900 mm dia. CSP culvert at the outlet (under County Rd 22, invert elevation is 78.58). The capacity of the outlet culvert is estimated at 7 m³/s using Manning's equation.

<u>Watercourse 2</u>: the watercourse drains an estimated are of 17 hectares approximately split between the subdivision site and the west neighbouring land which is outside the urban zone. According to data obtained from *Ontario Watershed Information Tool* website, the watercourse is approximately 750 m long. It joints watercourse 1 near the Cty Rd culvert. Refer to **Appendix E** for detailed information about watersheds. 4 m wide and 0.5 to 1 m deep. There is a 1400 mm dia.

There is a swamp near the watercourse (proposed Block A) where water is ponding and soil exhibits signs of regular saturation due to periodic inundation.

Smaller ditch culverts have been identified along the county road west side adjacent to the property. No stormwater flows from the site directly into county road ditches.

Existing site drainage conditions and patterns have been illustrated in Drawing ST-1, Appendix C.

3.0 PROPOSED STORMWATER MANAGEMENT AND DRAINAGE

3.1 DESIGN CRITERIA

• Minor system drainage: designed for the 5 year storm event without street ponding; stormwater captured and conveyed via the proposed storm sewer network (street and rear yard catchbasins, manholes and pipes) to the proposed stormwater facility. ICDs will be installed to prevent surcharging the sewer during major events.

• Major System: uses the road cross-section as an open channel for overland flows during major events. Runoff rate is controlled on-site to the 5-year release rate. Temporary storage will be provided in the stormwater management detention structure.

• Quantity control: post-development runoffs to match pre-development runoffs for the 1 or 5 and the 100 year storm events.

• Quality control: an "Enhanced" level of treatment with minimum 80% of TSS (total suspended solids) removal is required for the minor system drainage as per MECP guidelines.

• No surface drainage shall be directed toward neighbouring properties or County Road 22.

• Canadian National Railway: no drainage shall be directed toward the CN right-of-way and no adverse effect from the development stormwater management shall impact the CN right-of-way.

• Hydraulic Grade Lines (HGL) for 100-year event to be kept at least 300 mm below the underside of footing elevations of the proposed dwelling units. Otherwise houses will be equipped with sump pumps.

• Erosion and sediment control: Low Impact Development (LID) measures are required to retain, detain or infiltrate the first 5 mm of runoff from post-development impervious areas.

• Culverts at the entrances of the subdivision to be designed for 25 year storm event and shall be subject to approval by the County.

• Runoff from the adjacent agriculture land at the west limit will be diverted to the open space. It has not been included in the calculation of the detention structure.

• The large watershed draining north to south is beyond the scope of this study.

3.2 QUANTITY CONTROL REQUIREMENTS

Quantity control target is to limit the maximum post-development runoff rate discharged from the site for all storm events, up to and including the 100-year design storm, to that of the pre-development flow rates. Runoff in excess will be temporarily stored on site and discharged gradually into the watercourse. The Rational Method is used to estimate the pre-development and post-development runoffs.

3.2.1 Runoff Coefficient

Runoff Coefficient C	
Surface Type	C*
Impervious: Rooftop- Asphalt Pavement- Driveway	0.9
Road Shoulders	0.7
Grass-Cultivated-Pasture	0.2-0.4

* For Q $_{\rm 100yr}$ add 25% to C value. For $\,$ Q $_{\rm 25yr}$ add 10% to C value

* Table 5.7 Ottawa Sewer Design Guidelines – October 2012

Table 1: Runoff Coefficient C

Post-development average runoff coefficient has been estimated at **0.56** (0.64 for 100 year events) and impervious ratio at 0.43 based on the surface nature and the maximum impervious surfaces permitted by the current Zoning. Minimum lot area is 465 m² and maximum lot coverage is 30% with driveways 6 m wide. Refer to **Appendix C** for detailed calculations of perviousness ratio and weighted runoff coefficient for post-development condition.

3.2.2 Rainfall Intensity

Rainfall peak intensity formulas for the City of Ottawa have been used.

- * 2 year rainfall intensity: $I_2 = (732.951)/((T_c + 6.199)^{0.810})$; where $T_c = time of concentration in min$
- * 5 year rainfall intensity: $I_5 = (998.071)/((T_c + 6.053)^{0.814})$
- * 25 year rainfall intensity: $I_{25} = (1402.884)/((T_c + 6.018)^{0.819})$
- * 100 year rainfall intensity: $I_{100} = (1735.688)/((T_c + 6.014)^{0.82})$

* *Time of concentration:* depending mainly on soil roughness, terrain slope, rainfall intensity and longest runoff path. The farthest points to the outlet (watercourse) are 495 m for per-development and 520 m



for post-development (including 40 m overland flow). Several formulas resulted in different values of Tc (see Appendix C). A conservative estimation for Tc is 20 min for pre-development and 15 min for postdevelopment. Rainfall Intensity will be:

Pre-development: I₂ = 52.03 mm/hr ; I₅ = 70.25 mm/hr ;I₁₀₀ = 119.25 mm/hr Post-development: I₂ = 61.77 mm/hr ; I₅ = 83.56 mm/hr ;I₁₀₀ = 142.89 mm/hr

3.2.3 Drainage Areas And Runoff Calculations

Pre-development and post-development drainage areas are shown in the drawings ST-1 and ST-2 in Appendix C and are summarized as follows in Table 2 and Table 3:

Pre-development:

The topography of the site generally has a uniform slope between 0.5 % and 2 % from south to north toward the watercourse as shown in drawing ST-1, Appendix C. The site surface is 100% pervious and is used as a fallow / cultivated land.

IFRE-DEVELOF		UNOFFCA	LCULAII						
Catchment	ID	Area (ha)	Percent of Total Area	C*	AxC (ha)	C mistve	Q 2- year (L/s)	Q 5- year (L/s)	Q 100- year (L/s)
Subdivision Area	A1	7.6725	70.21	0.3	2.3018	0.21	332.9	449.5	959.4
Block A and C	A2	3.2550	29.79	0.3	0.9765	0.09	141.2	190.7	407.0
TOTAL SITE A	REA	10.9275	100%	_	3.2783		474	640	1,366

I/ DDE DEVELODMENT DUNCEE CALCULATION

Table 2 – Pre-Development (Existing) Drainage Areas

Post-development:

Storm water of the subdivision will be captured and conveyed via underground storm sewer to a proposed detention structure in the open space (Block A). Excess flow beyond pre-development levels will be stored and will eventually be discharged through an outfall into the existing watercourse.

The housing area is approximately 7.6732 ha (A1-A43). The runoff in the open space beyond the earth berm will remain uncontrolled and will outlet directly into the watercourse.

Table 3 summarizes post-development drainage areas breakdown.

II/ PUSI-DEVEL	OPINENTR	UNOFF	ALCULA	TION	1			i		i	
Catchment	ID	Area (ha)	Percent of Total Area (%)	с	AxC (ha)	C minitive	Q 2- year (L/s)	Q 5- year (L/s)	Q 100- year (L/s)	Que Con Measur	by trol re (L/s)
					1 -		1.1.1	1.00		CONT.	UNC.
Subdivision	A1 to A36 & A38 to A44	8.1368	74.45	0.56	4.5566	0.417	782.4	1,058.4	2,069	2,069	-
Open Space	A45	2.6716	24.45	0.30	0.8015	0.073	137.6	186.2	398		398
Uncontrolled Area	A37	0.1191	1.09	0.56	0.0667	0.006	11.5	15.5	30		30
TOTA	L	10.9275	100%		5.4248		932	1,260	2,497	2,069	428

W DOCT DEVELODMENT DUNOFE CALCULATION

Table 3: Proposed Post-Development Drainage Areas

3.2.4 Allowable Release Rates

Post-development allowable release rates are calculated using the Rational Formula for controlled areas. A45 drainage area is not included in the calculation since it is unaltered. The difference in runoff generated by A37 is considered in the calculation to. Table 4 summarizes

Post-Dev. n-y Relea	ase Rate From A1 to A44	<	Pre-Dev. n-y Rate From	A1 to A44
Post-Dev. n-y Relea and A38	ase Rate From A1 to A36 to A44 (Pond)	<	Pre-Dev. n-y Rate From A1 to A (-) Difference Post Dev and	36 and A38 to A44 Pre Dev of A37
2у	782.4	controlled	353.1 - (11.5-5.2)	346.8
5y	1,058.4	to	467.7 - (15.5-7.0)	468.2
100y	2263,0		1017.5 - (33-14.9)	1,002.1

post-development allowable release rates.

Table 4: Proposed Post-Development Drainage Areas

As requested by the Conservation Authority, post-development flow rates will match per-condition levels. These rates represent approximately 7% and 15% of the capacity of the existing culvert for the 5 y and 100 y events.

3.2.5 Proposed On-Site Storage

It is proposed a detention basin with an outlet control structure at the north side of the site. (Refer to **Appendix C and Pond Plan** for all details).

- Bottom length, Bottom width and depth: ~ 45m, 15m, 1.5m; a maximum volume capacity of 1500 m³.

- Maximum interior embankment slopes: 3:1.

- Minimum 0.3 m freeboard to embankment crest.

- Emergency spillway on the watercourse side.

- Minimum setback from watercourse: 30 m.

- 2 x 2 x 0.4 m Riprap apron at inlet location as per OPSD and scour protection at outfall.

- A concrete outlet control structure with an opening (orifice) and a rectangular weir will be installed inside the pond as per details.

- A chain-link fence will be installed surrounding the pond for safety purpose, a

3.2.6 Hydrological and hydraulic modelling

EPA SWMM 5.2 has been used for the hydrological modelling of storm water using different design storms and hydrographs for pre-development and post-development conditions. The 4-hour Chicago Storm derived from Ottawa IDFs generates the highest peaks. Refer to **Appendix C** for all details. SWMM has been used in pond routing and sizing of an orifice and a weir designed to limit post-development peak flows to those of pre-development levels.

Infiltration losses for catchment areas have been modelled using Horton's infiltration equation and default values provided by City of Ottawa guidelines. Horton's Equation: f(t) = fc + (fo - fc)e-k(t); where: initial infiltration rate: fo = 76.2 mm/hr; final infiltration rate: fc = 13.2 mm/hr; decay Coefficient: k = 4.14/hr. Equivalent width and imperviousness ratio have been assigned to each sub-basin. Imp(%)= (C-0.2) / 0.7

Hydrology Toolbox 5.4 has has been used for various hydraulic designs and capacity estimations.

3.2.7 Hydraulic Grade Line

SWMM hydrodynamic routing method has been used to determine the maximum hydraulic grade lines in storm sewer during major events. ICDs in catchbasins and catchbasin-manholes are designed to keep the HGL low in the main sewer. Maximum HGL table is exhibited in **Appendix C**. For the minor system, the HGL is maintained lower than obverts of sewer pipes. For the 100y event, the HGL is still near the obverts levels. In no case the HGL is above ground. Underside footings of future buildings will be kept above HGL by at least 0.3 m. For houses located downstream, foundation drains will be disconnected from the storm sewer to prevent basement flooding. All houses will be equipped with backwater valves for storm and sanitary connections.

3.2.8 Major System

The additional runoff exceeding the proposed sewer capacity designed for 5 year return period will flow overland in open roads. Major system capacity is estimated at 2.0 m³/s at 0.5 % road slope and 0.2 m depth based on Manning's equation for open channel. The 12.5 m wide path, adjacent to Block B, is part of the major system route. Overland flow depth is not expected to exceed 0.3 m in all roads. Refer to **Appendix C** for major system details.

3.2.9 Flow Restriction

ICDs with diameters varying from 55 to 127 mm will be installed inside catchbasins and catchbasinmanholes as per the City of Ottawa specifications.

3.3 QUALITY CONTROL REQUIREMENTS

Enhanced level of treatment (80% of TSS removal) is required to protect receiving waters. It will be achieved by the installation of a Stormceptor EFO12 by Imbrium or equivalent **(Appendix C)**.

Moreover, LID measures and Best Management Practices (BMPs) will be implemented such as:

- Flattened grassed areas will increase the travel time and provide some quality enhancement to the stormwater before it reaches receiving sewer.

- All roof leaders from buildings shall be directed away from buildings toward the landscaped areas and grassed swales in order to promote infiltration.

- Vegetated or enhanced swales: helps by tracking pollutants such as heavy metals, lowering peak flows and reducing erosion.

- Sub-drains where low grades improve the quality of released water and increases infiltration.
- Storing water temporarily helps clean stormwater and control sediments.

3.4 DRAINAGE OF NEIGHBOURING LAND

3.4.1 Watershed Delineation and Parameters

The DEM surface and contours of the neighbouring land have been obtained from LiDar data downloaded from Ontario Geo-hub website. The watercourse contributing watershed is delineated using ridge-lines and flow-lines. The portion of the watershed located within the developed site will be urbanized and therefore considered when designing the storm sewer. The area left from the property line to the highest point (90.24) is approximately 9.17 ha. The entry point is located at Lot 45 rear line and has an elevation of 81.50.



Ontario Watershed Information Tool (OWIT) also provides watershed boundaries with less accuracy. Refer to **Appendix E** for watershed maps and parameters.

Using OWIT, the two watersheds contributing to both watercourses that drain to the culvert outlet are:

	A (ha)	Width (m)	Longest Path (m)
Watershed 1	476.37	1,200	4,480
Watershed 2	17.01	176	750
Watershed 1+2	493.38	1,200	4,480

Table 5: Watershed Information

The large watershed draining north to south contains 1.047 km² of lakes/wetlands.

3.4.2 Peak Flows Estimation

Since the risk of flooding or topping could affect residential properties, the design of the culvert will be based on the Rational Method for 100 year event.

Runoff coefficient: C= 0.25 for 5 year event and 0.313 for 25 and 100 year events.

<u>Time of Concentration</u>: Using Airport and Bransby-Williams formulas: Tc = 25 min.

Rainfall Intensity:

where T_c = time of concentration in min

- * 5 year rainfall intensity: $I_5 = (998.071)/((T_c + 6.053)^{0.814})$
- * 25 year rainfall intensity: $I_{25} = (1402.884)/((T_c + 6.018)^{0.819})$
- * 100 year rainfall intensity: $I_{100} = (1735.688)/((T_c + 6.014)^{0.82})$

<u>Peak Flows:</u> Calculated peak flows are as follow:

	5-YEAR	25-YEAR	100-YEAR
Tc (min) =	25	25	25
I ₅₋₂₅₋₁₀₀ (mm/hr) =	60.90	84.22	103.85
A (ha)=	9.1795	9.1795	9.1795
C=	0.250	0.313	0.313
Qp (L/s)	388.5	672.7	829.5

Table 6: Peak Flows

An additional flow of 32.5 L/s from drainage area A37 (A= 0.1191 ha, Tc = 10 min, C= 0.55), is included in the design of the trapezoidal channel and culvert pipe.

3.4.3 Culvert Design

The design of the trapezoidal open channel is performed using Manning's equation for a lined channel.

The design of the culvert is performed using HY8 using inlet control, the culvert will be a concrete pipe one barrel diameter 750 mm or two barrels 500 mm diameter with a minimum slope of 1.0%. Headwater elevation for the required flow is 82.35 for the 750 diameter culvert.

Culvert hydraulics have been checked using software simulations with Chicago storm distributions.

The HGL remains lower than the pipe obvert. Lot grading elevation at the west bank of the ditch is 82.42 which is above high water levels in the ditch during 100 year events.

Construction Measures:

A side tapered headwall shall be constructed at the inlet of pipe culvert.

Erosion protection measure shall be implemented at:

- the inlet of the open channel.
- along the open channel.
- the inlet and outlet of culvert pipe.

Refer to **Appendix E** for design details and to the grading plan for other details.

The drainage easement will be accessible from the right of way and will be dedicated to the Township.

4.0 EROSION AND SEDIMENT CONTROL MEASURES

The purpose of Erosion and Sediment Control (ESC) measures is to mitigate the adverse environmental impacts caused by the release of silt-laden stormwater runoff into receiving sewers and watercourses and to ensure that sediment is contained within the site. Temporary ESC measures will be implemented and maintained during construction period as specified in related drawings and in accordance with the requirements of latest provincial standards *OPSS 805*. They will be maintained in good order until vegetation has been re-established on the site.

4.1 TEMPORARY SEDIMENT CONTROL MEASURES

> Temporary silt fencing shall be placed prior to topsoil stripping and for the duration of the construction around the perimeter of the site and adjacent to any disturbed areas and surrounding topsoil stockpiles in order to prevent sediment from entering into the watercourse. It shall be inspected regularly and after every rainfall event for rips or tears, broken stakes, structural failure. Accumulated sediment/silt shall be removed when it reaches 50% of the height of the fence.

> Mud-mats shall be constructed at all locations of access/egress to and from the site.

> Straw bale and rock check dams shall be installed in any temporary drainage ditches required during the construction period.

> All exposed soil and disturbed slopes shall be stabilized as soon as possible with a seed and mulch application

> No construction activity or machinery shall intrude beyond the silt/snow fence or limit of construction area. All construction vehicles shall leave the site at designated locations.

> All materials and equipment used for the purpose of site preparation and project completion should be operated and stored in a manner that prevents any deleterious substance from leaving the site or entering the water (silt, petroleum products, etc.).

> Stockpiles of soil shall be set back of at least 15 m from any watercourse and stabilized against erosion as soon as possible.

➤ Erosion problem can be mitigated by reducing the peak flow rate, decreasing the duration of storm flows, minimizing the volume of runoff, and implementing Low-Impact Development (LID) techniques in new construction.

4.2 CONSTRUCTION SEQUENCING

The schedule of construction activities with respect to sediment controls are as follows:

- Installation of silt fences prior to any other activities on the site.
- Construction of temporary mud-mats at all construction access/egress.
- > Installation of site servicing and underground utilities.

- > Disposal of all the surplus excavated materials off site.
- Construction of roadways.

> Restoration / re-vegetation of disturbed areas either with temporary measures such as mulch or seeding or with final landscape and paving materials.

> All re-graded areas that are not occupied by buildings, sidewalks, or driveways shall be topsoiled and sodded/seeded immediately after completion of final grading operations.

Erosion controls shall be kept in place and functional until the site is stabilized (lot grading and sodding complete).

4.3 INSPECTION & MAINTENANCE OF ALL THE EROSION AND SEDIMENT CONTROLS

Shall be undertaken with the following frequency:

- On a weekly basis
- After every rainfall event
- > After significant snow melt events
- Prior to forecast rainfall events
- If damaged control measures are found, they should be repaired and/or replaced within 48 hrs.

5.0 CONCLUSIONS AND RECOMMENDATIONS

This report addresses the stormwater management and erosion control for the proposed residential subdivision development. The conclusions and recommendations are as follows:

- The 30m setback for the unnamed watercourse in the north side of the site is to be considered a no-touch zone and existing vegetation is to be retained in perpetuity to protect terrestrial and aquatic habitats.
- The release of post-development stormwater will be controlled to the pre-development levels for all storm events up to and including the 100-y event. Post-development excess of stormwater will be stored in the proposed detention basin located in the open space (Block A) to be conceded to the Village of Cardinal.
- Downstream capacity is not expected to be affected by the development since expected postdevelopment peak flows do not exceed the current peak flows under undeveloped conditions.
- No negative impact is expected on the existing County Rd culvert since the storm flow generated from the developed site will be kept at pre-development levels.
- The watercourse at the site west side shall be detoured to the open space.
- A Stormceptor will be installed upstream the detention structure to achieve the required storm water quality. Lot level LID measures such as flattened lot grading and directing downspouts to lawns will also help improve water quality.
- The majority of foundation drains surrounding future buildings will be connected directly to the storm sewer. When 100-y HGL is higher than foundation elevations and to protect basements against flooding, foundation drains shall not be connected directly to the storm sewer. Flow collecting in the foundation drain shall be pumped to the surface or to a sewer extension using a sump pump.
- Backwater valves shall be installed on all sanitary and storm laterals.
- No drainage will be directed to County Road or neighbouring properties.
- No drainage will be directed to Canadian National righ-of-way.
- Culverts shall be installed at entrances of the subdivision with a minimum slope of 0.5% with riprap at both ends.
- Road and yard catchbasins shall be equipped with inlet control devices (ICD).
- The owner understands that it is his duty to keep stormwater management control structures in good working order until transfer of ownership to the Village of Cardinal.
- All outlets to watercourses and open ditches require a permit from the Conservation Authority prior to any development of the lot, including grading and placement of fill.
- During all construction activities, erosion and sedimentation shall be controlled as outlined in this report and as shown in related drawings.

Respectfully submitted,

Mongi Mabrouk M.Eng., P.Eng.

Advance Engineering Ltd.



APPENDICES

Appendix A

- Figure 1: Site Location

Appendix B

- Geotechnical Report
- Letter from SNC, dated October, 2010

Appendix C

- Drawing ST-1: Pre-development Drainage Areas
- Drawing ST-1: Post-development Drainage Areas
- Runoff Coefficient Calculations
- Time of Concentration Tc
- Design Storm Calculations
- Allowable Release Rate
- Required Storage Calculation

Appendix D

- ICD
- Stormceptor

Appendix E

- Watercourse of West Neighbouring Land
- Watershed Parameters
- Hydraulic Design

APPENDIX - A





Aerial view of the subject site



Phot**Bagen169Apfri465**, 2021

APPENDIX - B



P.O. Box 997, Cornwall, ON, Canada K6H 5V1 814 Second Street W., Phone (613) 938-2521 E-mail: slt@ontarioeast.net Fax (613) 938-7395

May 31, 2021

Mr. David Simpson Edwardsburgh Development Inc. 434-300 Earl Gray Dr. Kanata, ON K2T 1C1

RE: Lockmaster's Meadow, Cardinal, ON Geotechnical Subsurface Investigation Report No. 21C350

Dear Mr. Simpson:

In accordance with verbal and e-mail instructions received from you, this report is submitted, outlining the results of a geotechnical subsurface investigation carried out at the site on Shanley Rd, South of the CN Main Line, in Cardinal, ON

A) DESCRIPTION OF FIELD WORK & STRATIGRAPHY

After receiving the approval, we sent you a plan showing the proposed borehole locations. We then contacted Ron Jason Surveying to lay out the boreholes in the field.

After the stakes were placed in the field by Ron Jason Surveying, we called for service locates. Drilling and sampling took place on April 7, 2021 using a CME 55 track mounted auger drill from E.O.D.D. of Hawkesbury, ON. Supervision was by the undersigned geotechnical engineer. Report No. 21C350 Continued

Page 2

A total of 7 boreholes were put down as noted on the sketch. Most boreholes were put down to 4.6m. or to refusal if above this. One borehole was advanced to 5.18m. The borehole next to Shanley Rd. was advanced to 2.1m. The boreholes were advanced by split spoon sampling. Standard Penetration tests were conducted along with the split spoon sampling. The recovered samples were placed in glass jars for later detailed lab classification and washed gradation tests. The results are found in the attached borehole logs and washed gradation sheets.

We had one of our staff return on April 8, 2021 to measure the water levels in each borehole.

A sketch is attached showing the borehole locations. Also attached are a topographic map of the whole area and a colour map showing the location in relation to the Town of Cardinal.

B) STRATIGRAPHY

The stratigraphy is fairly similar throughout.

The general stratigraphy is a brown, moist, stiff clayey silt overlying a brown to grey, moist, compact to dense silty sand and gravel till.

There is a brown, moist loose silt and sand stratum noted at Boreholes 4 and 7 below the topsoil. This extends to 0.91m. at Borehole 4 and 1.58m. at Borehole 7.

Report No. 21C350 Continued

Page 3

The clayey silt is noted throughout the property below the topsoil at the other boreholes and below the silt and sand at Boreholes 4 and 7. The clayey silt is mainly stiff, but is occasionally hard, at Boreholes 5 and 6.

Underlying the clayey silt is a brown, moist, compact to dense silty sand and gravel till. This was noted at 2.7m. at Borehole 1, 3.7m. at Borehole 2, 2.9m. at Borehole 5 and 2.6m. at Borehole 6. The sand and gravel till was not reached at Boreholes 3 and 4.

Borehole 7 was only advanced to 2.1m. for the pavement design information, to connect the new street on to Shanley Rd.

For the specific stratigraphy at each borehole, the borehole logs should be referred to.

C) GEOTECHNICAL DISCUSSION

1) General

It is our understanding that it is proposed to build a residential subdivision at this property. It would appear to be 94 lots in the prepared plan.

2) Services

The soil throughout is a Type 2 to Type 3 soil from a trench perspective. As such, normal trenches can be used. The bottom 1.2m can be vertical. Above 1.2m, the side slopes must be cut back to a 1 to 1 side slope.

Report No. 21C350 Continued

Page 4

The bedding and cover for all services should be 150mm. of Granular "A" compacted at 95% Standard Proctor Density.

All of the existing soil can be reused in the trenches, provided the soil is moist. Where the trenches will be within the roadways, the trench backfill must be ramped down in 300mm. lifts to 95% Standard Proctor Density.

3) Roadways

Where there are trenches within the roadways, the trench surface must be recompacted to 95% Standard Proctor Density before placing any granulars. Where there is topsoil at the surface, this should be removed over the full width of the roadway.

The granular subbase should consist of 375mm. of Granular "B" Type 2 and compacted to 100% Standard Proctor Density. The granular base should consist of 150mm. of Granular "A", compacted to 100% Standard Proctor Density.

The asphalt should consist of 75mm. of HL3, placed and compacted in 2 lifts to 96% Marshall Density. This is to allow having a paved street before construction of the houses, followed by a second course near the end of construction.

4) House Foundations

The bearing capacity at Boreholes 1, 2, 3 and 7 is in the 50KPa S.L.S. range. The bearing capacity at Boreholes 4, 5 and 6 is in the 100Kpa S.L.S. range. St. Lawrence Testing & Inspection Co. Ltd.

Report No. 21C350 Continued

Page 5

Where the bearing is 75KPa S.L.S. or higher, standard footings will be applicable. The site seismic factor is Site Class D throughout.

It is recommended that a bearing capacity evaluation be done of each house when the footings are being dug in order to provide the proper recommended footing size.

D) CONSTRUCTION CONTROL

In order to ensure that the recommendations of this report are adhered to, it is recommended that our firm be retained to inspect, test, and report accordingly.

Respectfully submitted ST. LAWRENCE TESTING & INSPECTION CO. LTD.

G.G. McIntee, P. Eng. GGM:mhm



Attachments

Attachment "C" Site Location Map





.

.

Page 177 of 465

Attachment "A" Draft Plan of Subdivision



4 OF 6

St. Lawrence Testing & Inspection Co. Ltd. OFFICE BOREHOLE RECORD CUENT Edwardsburgh Development Inc. BOREHOLE NO. _1_____ LOCATION Shanley Rd. South of CN Rail Cardinal, ON BOREHOLE NO. _1_____ DATE OF BORING April 7, 2021 DATE OF WL READING _April 8, 2023 DATUM SOIL PROFILE SAMPLES LAB TEST

			SOIL PROFILE SAMPLES																										•		
E	NOL	Ŧ		PLOT	R DNS	NOIL		E.	ERV	Ē	RATORY ESTS ORMED		LAB TEST RES									SULTS									
DEPT	ELEVAT	DEPT	SOIL DESCRIPTION	STRAT. I	WATE	CONDIT	JYPE	NUMB	RECOVI	N - VA	PERF		WATER CONTENT & ATTERBERG LIMITS.																		
			· · · · · · · · · · · · · · · · · · ·					<u> </u>	<u>├</u>	<u> </u>		DYNAMIC PENETRATION TEST BLOWS PER FOOT K																			
-0-			200mm. Topsoil					-				ή	Π	Π	Т	Π	\prod^{2}	п	Π	Т	Τ	m	п	Π	Π	Π	Î	ÌTT	Π	Π	_ <u>₿0</u>
			Clayey Silt					[1			1												
			Brown, moist, stiff																												
								L				Ħ			t			╬	╋	Ť			H	\uparrow		╏	Ħ		ÌÌ		
Н					78																								11		
					<u> </u>									ļ									İ		1						IП
-1-						-						H	┢┥	╫	Η	╉	╋	╢	╢	╁┟	╢	╢	╫	╂	╈╉	┢╋		╈╋	╁	╁┟	
\square															11		ł			ļļ									ÌÌ		Η
\vdash		ĺ															1														H
					k						-	H	\parallel	╢	╢	╢	┢	μ.	╢	₩	╢	╢	╢	┼┼	╂	₩	╢	╢	⋕	╢	$\left \right $
					ľ	\ A	ĺ							1	11	11															E
						VI.	92	-	100	3													$\ $	ľ				$\ $			H
						Δľ			100			Ц	\downarrow	Ц	Ц	Ц	Ц		Ц.	ļ	Щ	╢	╢		Ц	Ш		Ц	ļļ	Ļ	Ш
디					/	/ \															II	II							f		H
\vdash					ľ	1																1						ł			Ц
																						$\ $									ΙH
{					F	+			f			Ħ	╈	H	Η	₶	Ħ	Ħ	H	Ħ	Ħ	Ħ	ÌŤ	Ħ	╞╋┙		Ħ	Ħ	Ì	ÌŤ	П
																ll	lĺ										$\ $				Н
	2.7	4	Sand and Gravel Till														$\ $					1									
- 3			Brown, moist, silty,		F				+		ł		+	+	+	╢	╂┤	+	+	+	╟	╢	H		Щ	╢	╫	╢		┢	┼┥
		ĺ	compact to dense		۱\ ا	Λ																									П
						Vŀ	ss	2	75	30					ľ	IÍ.															Н
					L	ДĻ					ļ			Щ		╟	μ	Ц	⋣		\square			Ц		4	⋕	Ц.	Щ		П
						' V									ľ																Н
					ľ	-						$\ $	I																		Η
																															Н
4-					ſ			~			Ī	Π	Π	T	Π	Π	Π	Π	Π	Τ		T	Π	T	ר ר	Π	Π	Π			Η
																									ĺ						Ц
		ļ											$\ $																		Η
					⊢		+				H	Ħ	╉	╢	╢	H	╟	╢	Ħ	\parallel	╉┦	\dagger	╈	\ddagger	+	╢	╢	Ħ		╢	廿
	4.5	7	Cermination of																												Η
		[t	oorehole																												日
					Ļ		_				Ļ	╢	₽	╢	ļļ	4	Ļ	4	Щ	\parallel	Щ	Ц	\parallel	╢	╢	╢	╢	Щ	╢	╢	H
																															Ц
																															Н
-													\prod		Ш			Ц	IJ	\prod						\prod			\prod		
						- 1					Ī	AP	E	(DI)	ĸ				-												
																						1									
					Ра	gę	179) dł	465																						
1		1	ſ	1		1			1		I											_						_			
St. Lawrence Testing OFFICE BOREHOLE RECORD & Inspection Co. Ltd. REPORT NO. _210350_ CLIENT <u>Edwardsburgh Development Inc.</u> BOREHOLE NO. _2 LOCATION Shanley Rd. South of CN Rail Cardinal, ON CASING <u>HF</u> Auger DATE OF BORING April 7, 2021 DATE OF WL READING April 8, 2021 DATUM ___ SOIL PROFILE SAMPLES LABORATORY TESTS PERFORMED RESULTS LAB TEST DEPTH ELEVATION WATER CONDITIONS CONDITION N - VALUE STRAT. PLOT RECOVERY NUMBER DEPTH TYPE SOIL DESCRIPTION WATER CONTENT & ATTERBERG LIMITS. WP W WL DYNAMIC PENETRATION TEST BLOWS PER FOOT. . .K 40 20 'n 230mm. Topsoil Clayey Silt Brown, moist, stiff, with some sand below 3.Om.

		1,13	ų																Ш		
			\mathbb{N}	SS	1	75	3														
3-			X	SS	2	100	11														
3.68 Sand Brown	and Gravel Till , moist, silty,																				
	gt to dense							-													
4.57 Termi: boreh	nation of` ole																				
-5-																					
		Pa	ige	180) of	465			APP	PEN	DIX	المليع	<u>,</u>		<u></u>	<u></u>	ار کر	<u></u>	نيغيو ا	تتمور	

St. Lawrence Testing & Inspection Co. Ltd.

OFFICE BOREHOLE RECORD

REPORT NO. _210350

BOREHOLF	NO	3	
 00/12/1011			

CUENT Edwardsburgh Development Inc. LOCATION Shanley Rd. South of CN Rail Cardinal, ON _____ CASING HF Auger

DATE OF BORING April 7, 2021 DATE OF WL READING April 8, 2021 DATUM

			SOIL PROFILE				S	SAMP	LE\$			Ι			-															_	
	z			10	S	N		~	łł	Ц	ATORY TS RMED			ι	LAE	3				T	ES	T					RE	SUI	.15		i
DEPTH	EVATIO	DEPTH	SOIL DESCRIPTION	RAT. PL	WATER	ONDITIC	TYPE	NUMBE	ECOVEI	I - VALL	LABOR TES PERFO	╞			-	W	ATE	R (W	COI /P	NTE	NT	& .	ATT W	ERE	BER	G LI M	MIT /L	S.			
	ш —			SI	8	о 			_ <u> </u>					DVI		10	DEN		241	ION	TE	ST F		VS P	ER	F001		к			
-0-												ů	тг	ייזט TT	naw TT		20		П	T		40				1	6 0	11	Π		80
			230 mm. Topsoil Clavey Silt											li																	H
			Brown, moist, stiff																												Ц
	1		becoming grey below 3.3m.		70							4	╢	╟	╫	╢	╉	╟	╂	┽	╢	╢	╢	┼┼	╟	H	╢	╫	╫	Н	┨
					V																										Н
					-																										Я
-1-						-						┢╋		ÌÌ	İÌ	İİ	Ť		Π	ÌÌ	ÌÌ	ÌÌ			Ì	Π	ÌÌ	ÎÎ	Î	\prod	Ĥ
																															Ħ
												_			╨					ļļ	\parallel				ļļ.		╢	╢		Ш	Ħ
						$\backslash I$																									
-				:		XI	SS	1	100	4																					Н
- 2-						A						+		╟	╢	╫	H	-		╏	╫	╢	╫	┢╋	╟	Н		╫	╂		
					ľ	<u> </u>																						ľ			Н
																															Н
												╉		Ħ		Ħ	T	T		Ħ	ÎÎ	ĬÌ	Î				Ì	ŤÎ			П
												╢				Ц				ļ	╢	Ц			Ш		╢	╢	ļļ.	⊢	Ħ
					Í																										H
						Υ	SS	2	75	4																					Н
					ŀ	А		_				+	+			╢	+	-		╟	╢	╢	╢		-	+	╫	╢	┢╋╴	┝╋╋	Н
					ľ	<u> </u>																									Н
																															F
-4-												+					ti					Ħ				Π	Τ	Π	††	Π	Ħ
																															Ħ
																ļ	\parallel			\prod	╢	╢	\parallel				╢	╢	_	┝┼┥	Ħ
						7																									H
						χI	SS	3	100	6																					Н
-5-				ľ		\mathbb{A}					ļ	+	+		H	╟	╢	┥	+	╟	╢	╢		+	+	+	╂	╢	╢	┝┼┥	Н
	5.1	8	Termination of		ł		·																								Н
		~	borehole																												H
					ŀ							AF	PPE	ND	IX	<u>i I</u>	ل م			i ala	<u></u>	<u>.</u>	<u>.</u>	ليك			-				
_																															
					Pag	le 1	81	of 4	65																						

St. Lawrence Testing

OFFICE BOREHOLE RECORD

		2 🗉		GO	. 1.8	d.													f	REP	OR	r Ni	0	_2	10	35	0		<u> </u>		
	LOCA	IT TION	Edwardsburgh Developme Shanley Rd. South of	ent CN_	<u>Inc.</u> Rail	Ca	rdir	nal.	 				_						_ { _ (BOF CAS	reh Ing	OLE	NC H I) E	_4 <u>Au</u>	ge	:r				-
	DATE	0F B	ORING <u>April 7, 2021</u>		DATE O	FWL	READI	NG	Apr	i1 8	, 20	2				_			_ 0	TA(им										
	<u>.</u>		SOIL PROFILE	- 			, 	SAMP	LES												T C/	. т						eu	1 Te	-	
	NO	-		LOT	SN	N		- E	₽	4	ATORY STS DBMED				U	ΑB					IE:	51					нс	:50	L12	,	
DEPT	LEVATI	DEPTI	SOIL DESCRIPTION	RAL P	WATER	ITIONO	TYPE	NUMBE	ECOVE	- VALI	LABOR TE: PERFC					N	/A1	TER I	CC WP)NT	EN	&	ATT W	ER	BER	GL	imn Vl	TS.			_
					8	ō			~	Z													~ 								
-0-			150mm Topcoil							<u> </u>		-'n	T	DY	rna TT	міс 11			П					75 I TT	TT.	гоо 11	 m⊤	.к. ГП	 TT	TT	
	4		Silty Sand																												
			Brown, Moist, loose																												
• •					.78							h				┝╋┥		₩	╉╋	┥		╢	╫	╉╋				┝╋╋	┢╋	₩	╬
·- ··																															
-1-	.91		Clayey Silt			-						ļ	╽	╢	-		╉	ļļ	╟	$\prod_{i=1}^{i}$	\parallel	╢		┢┥	Щ		╢	╇	╟	₽	∦ ⊢
			becoming grey below																								$\ $				ļF
			3.1m.																												ļF
						$\overline{\Lambda}$						I			T	Ħ	Î	Π			\prod				\prod	T	T	T		Π	F
						XI	ss	1	100	7																lĺ				ľ.	IE
2		ĺ			þ	4						H	H	╢	╢	₩	H			╟	╢	╢	┥┤	+	╉	╢	⋕	⋕	+	\mathbb{H}	Æ
					ľ	-1																									E
																													\square		E
		Ì			ſ						ĺ	Π	Ţ			Π	Π		T	Τ	Π	Π	\prod	Π	Π	Π	Π	Π	\prod	Π	E
											i																				
3-						_					ł	╢	+		╟	╢	┟┤	┦╢	+	+	H	\mathbf{H}	╢	╢	╫	╀	₩	$\left \right $	╢	╫	H
					\	$\langle $	00	, .	70																						Н
						۸L	55 /	د .	/0	"																		Ш			Н
					ľ	_/													$\ $												Н
																															Н
4 -					-			_			H	╫	╢	╢		+	╟	╢	╢		╢	╢	╫	╫	╉	╟	╟╢	╫	₩	╫	Н
																			11											l	Ц
											Ľ										\prod	Ш		ļĮ.	Ш		Ш		Ш	╢	H
	4.57		Fermination of																												H
			porehole																												日
5-					\vdash			+			┟	H	╟	╢	╢	╢	╢		╟	╢	╢	╟	╢	┝╋┥	╟╢	+	╋	╢	╀	╫	Н
																															H
-]											ļ																	Ш	Ц		L
											 ^	AP	ΡEΝ	IDD	K																
			ł		Pa	ge	182	df	465																						
1		- 1	1		1	1	-	1	1																						1

CLIENT Edwardsburgh Development Inc. OFFICE BOREHOLE RECORD LOCATION Shanley Rd. South of CN Rail Cardinal, ON CASING HF Auger DATE OF BORING April 7, 2021 DATE OF WL READING April 8, 2023 DATUM

F			SOIL PROFILE	<u> </u>		Γ-		SAMP	LES		Ť	1			••••		_															_	
	2			F						Γ	S S	MED			IJ	٩B					T	ES'	r					RI	ESI	JLĨ	S		
DEPTH	VATIO	EPTH	SOIL DESCRIPTION	AT. PLO	ATER	DITION	ΠYPE	MBER	OVERV	VALUE	TEST	ERFO				V	VA	TEF	R C	ON	TE	NT	8/		ERE	ER	ĠL	IMI	TS.				
	8			STR	CON	CO		2	RE(ż	י כן								W! 	, 			۱ 	N >			V	VL —					
													}	D	(NA	MIC	; Pi 2	ENE 0	TŔ/	ATIC	ΟN '	TES	18 40	L0W	IS P	ER I	-00	T 6 (.K				80
٢			180mm. Topsoil									Ĩ	Π		Π	Π	Π	Ţ			T		Π	Í.			Ĩ	Π		Π	Π	Π	F
F			Brown, moist, hard													l	Ì																Ħ
È					.73							ļ	╉	4		╎	ļ				┦	┥	ļ								ļļ.	ļļ	H
					V						-																						H
	-																																H
┝┶					ľ							h	ĥ				ÌÌ				Ħ		Ĭ			††		Ť		Ϊ	T		Ħ
										ļ									Ì		[]					ll	ļ				1		H
					k		_					H	H	╢		4	╀	╢	╢		┝╋	╢		╢	┦	╢			╢	+	+		Η
					ľ	\mathbb{V}		,	100	16																							
						ÅΙ	55																										
-2 -					Į	\neg						\prod		Π	Π	I			Π	Ţ	Π	Π		Π	Π	Π		Π	Π	Π	Π		\exists
																																	Е
					┝	-	-					4	┦	╢	╢		╀	╟	₩	μ	H	╟	╢	╢	╢			╢	╢	╢	╢		-
															ļ															l			_
	63	-	Cand and Crowol Till													Í																	┫
	1 9 £		Grey, moist, silty,		Ν																											╟	
			compact to dense			XI	SS	2	65	10																						╞	
					H	$^{\prime}$						╢			+	╟	॑	╢	4	╢	+			╟		+-	╟	╢	╟	╟	₩	╢	
					-																											╠	
-/								-																				I				╟	1
											ľ																						
																			l]								
		4-			\vdash		+				ŀ	╫		╢		+	┢┼	╢	┥	+	╢	╢		╁	+		+				H		
	1.5/	1	porehole											l												ľ	Í						1
- 5-								_	_												I				ļ	Ш							1
																										$\ $							1
																																F	1
							+			-	ŀ	LL Api	١ E	101) 101)	K TT	Ц		ί.Ι.	LÍ		Ц.	Ц	Ļ		Ц	11	Ļ	U	4	Ļ	_	<u>+</u> .	1
							100		105																								
					На	ye	103		405				_																				J

St. Lawrence Testing OFFIC

OFFICE BOREHOLE RECORD

	CLI		Edwardsburgh Developm Shanley Rd. South of	ent_	<u>Inc.</u>											RI B(EPOF OREH	rt n Hol	10 E NC	_21	LC3 _6	50)			-
	DAT	E OF	BORING April 7, 2021		DATE 0	FWL	rai) READI	DAI NG _	, <u>ON</u> Apr	i1 8	, 202	21				CA DA	ASIN ATUN	G_ (<u>_</u>	£	<u>iug</u>	<u>,er</u>	<u> </u>			-
			SOIL PROFILE	<u>.</u>		Γ		SAMI	PLES		Ť	Γ													_	
 ≡	TION	E		PLOT	R	NOE	<u></u> е	E	ERV	4	RATORY ESTS ORMED		U	48			TE	ST				R	ESU	LTS		
	ELEVA	DEP.	SUL DESCRIPTION	STRAT.	WATE	CONDI	Ч	NUMB	RECOV	N - VAI	LABO TI PERF			Ŵ	ATER	CON NP	NTEN	IT &	ATT W	ERB	ERG	LIM WL	IITS.			
					1			╞	<u> </u>			. 0	DYNA	MIC F	PENET 2 0	RATI	ON T	EST 4	BLOV	VS PE	ER FO		, .K.			80
			250mm. Topsoil <u>Clayey Silt</u> Brown, moist, hard																							
						-						┣┿┿╇╇														
- <u> </u>																										
		į				\mathbf{X}	SS	1	100	10																
					Z																					
	2.	64	Sand and Gravel Till Brown, moist, silty, dense																							
	3.	30	Sampler and auger			Z:	SS 2	2	75	50+																
-			LELUSAL																							
4 -																										
					F																					
>																										
					Pa	ge	184	of	465		AF	PPENC)IX			<u></u>	┶┶╌┿┯	ĻĹĂ	<u>, </u>					, de adre	<u></u>	

St. Lawrence Testing OFFICE BOREHOLE RECORD & Inspection Co. Ltd. REPORT NO. _21C350____ CLENT <u>Edwardsburgh Development Inc.</u> BOREHOLE NO. __7_____ LOCATION Shanley Rd. South of CN Rail Cardinal, ON ___ CASING <u>HF Auger</u> DATE OF BORING April 7, 2021 DATE OF WL READING April 8, 2021 ____ DATUM ____ SOIL PROFILE SAMPLES RESULTS LABORATORY TESTS PERFORMED LAB TEST ELEVATION WATER CONDITIONS STRAT. PLOT N - VALUE CONDITION RECOVERY NUMBER DEPTH DEPTH ТҮРЕ SOIL DESCRIPTION WATER CONTENT & ATTERBERG LIMITS. WP W WL DYNAMIC PENETRATION TEST BLOWS PER FOOT. . .K 40 0 150mm. Topsoil Silt and Sand Brown, moist, loose .61 V SS 40 1 6 1.58 Clayey Silt Brown, moist, stiff SS 2 70 4 2 2.13 Termination of borehole

Page 185 of 465

APPENDIX









Tel: (613) 984-2948 + Fax: (613) 984-2872 + Toll Free: 1-877-984-2948 + 38 rue Victoria Street, Finch, ON KOC 1KO + www.nation.on.ca

Via Email Transmission

October 12, 2010

Sandy Hay County Planner UCLG 25 Central Ave. West, Suite 100 Brockville, ON K6V 4N6

> RE: Draft Plan of Subdivision Conditions Edwardsburgh Cardinal Developments Ltd. Village of Cardinal Lot 7, Concession 1 Former Edwardsburgh Township United Counties of Leeds & Grenville

Dear Mr. Hay,

South Nation Conservation (SNC) has received and reviewed the <u>Draft Plan of Subdivision</u>, prepared by Eastern Engineering Group Inc., dated June 28, 2010 for the above noted subdivision. It is understood from the Plan of Subdivision that it is proposed ninety-three (93) lots intended for single detached dwelling units, one (1) block intended for Park/Open Space, one (1) road and one (1) block for a stormwater management facility. Further, the entire development will be serviced by the municipal water and sanitary sewer networks.

In our review, SNC considered the environmental impacts of the proposed subdivision on the local environment, as outlined under Sections 2.1 (Natural Heritage), 2.2 (Water Quality and Quantity) and 3.1 (Natural Hazards) of the Provincial Policy Statement (March 1, 2005) issued under Section 3 of the <u>Planning Act</u> and the Edwardsburgh Cardinal Official Plan (OP).

Watercourse

An unnamed watercourse enters the property from the north from under the CN Railway proceeds south, takes a turn and exits the property on the east side via a culvert under County Road #22. SNC staff confirmed by a site visit on October 4, 2010 that the unnamed watercourse has potential for fish habitat.

Upon preliminary review of the proposed development, SNC finds no reason to object to the proposed subdivision. SNC kindly recommends that the following statements be included as conditions of subdivision draft plan approval:

Page 1 of 3

Our Local Environment. We're in it Together. = Notre environnement. Nous le partageons.



Stormwater Management

1. The owner agrees to prepare and submit a <u>Storm Water Management Plan</u> and describe how it is to be implemented in accordance with the current Storm water Management Best Management Practices to the satisfaction of the Township of Edwardsburgh Cardinal, the United Counties of Leeds and Grenville and South Nation Conservation. The plan should address both water quality and quantity concerns. The plan should consider proposed on-lot controls to reduce the rate of runoff and minimize contaminant transportation. Models, assumptions and calculations of pre and post development runoff are to be included with this submission.

Sediment and Erosion Control

2. The owner agrees to prepare and submit a <u>Sediment and Erosion Control Plan</u>, appropriate to the site conditions, prior to undertaking any site alterations (filling, grading, removal of vegetation, etc.) and indicate how it is to be implemented during all the phases of the site preparation and construction in accordance with the current Best Management Practices for Erosion and Sediment Control to the satisfaction of the Township of Edwardsburgh Cardinal, the United Counties of Leeds and Grenville and South Nation Conservation.

Lot Grading and Drainage

3. The owner agrees to prepare and submit a Lot Grading and Drainage Plan and indicate how it is to be implemented to the satisfaction of Township of Edwardsburgh Cardinal, the United Counties of Leeds and Grenville and South Nation Conservation.

Fisheries

- 4. The Owner acknowledges that the Unnamed watercourse is considered either direct or indirect Fish Habitat, as per Section 35 of the *Fisheries Act*.
- 5. The Owner agrees to establish a 30 metre "No touch/No Development" setback of the Unnamed watercourse, on both sides, measured from the top of the average annual highwater mark. The final approved plan of subdivision shall clearly show this setback. Any deviation from this setback shall be to the satisfaction of the Township of Edwardsburgh Cardinal, the United Counties of Leeds and Grenville and South Nation Conservation.
- 6. The Owner acknowledges that South Nation Conservation is under agreement with the Department of Fisheries and Oceans Canada to screen all works that are in or adjacent to water. In accordance with Section 35 of the *Fisheries Act*, the Harmful Alteration, Disruption or Destruction (HADD) of fish habitat is prohibited. The impacts that any such works may have on a fish habitat, whether directly adjacent to the site or downstream, will necessitate a review by South Nation Conservation and may require approval of the Department of Fisheries and Oceans Canada.

Subdivision Agreement

7. The subdivision agreement shall contain wording acceptable to South Nation Conservation that the above noted conditions (under 1-7) will be implemented.

Page 2 of 3

Our Local Environment. We're in it Together. ᆕ Notre environnement. Nous le partageons.

I trust the above meets your present requirements, but should you have any questions, please feel free to call the office.

Yours truly,

Farel 1aben

Nathan Farrell Watershed Planner nfarrell@nation.on.ca 877-984-2948 ext. 302

c.c. Debra McKinstry

Township of Edwardsburgh Cardinal

Page 3 of 3

Our Local Environment. We're in it Together. 🛹 Notre environnement. Nous le partageons.



APPENDIX - C



EXIST. DITCH AND	CULVERT	{}
PHASING LIMITS		
PROPERTY BOUND	ARY -	• • • • •

				PROJECT NAME AND ADDRESS:
3	OPEN SPACE AREA	06/19/24		
2	PEER REVIEW COMMENTS	11/08/22	APPLICANT:	
1	INITIAL ISSUE	03/10/22	EDWARDSBURGH	COUNTY RD No. 22. CARDINAL
No.	REVISION / ISSUE	DATE MM/DD/YY	DEVELOPMENTS LTD.	Page 193 of 465



REFER TO STORMWATER MANAGEMENT REPORT FOR DETAILS ABOUT WEST WATERCOURSE

7	TABLE OF	DRAINAG	BE ARE	EAS															
DA #	AREA (ha)	RUNOFF COEF. "C"	тос	OUTLE	T DA #	AREA (ha)	RUNOFF COEF. "C'	, тос	OUTLET	DA #	AREA (ha)	RUNOFF COEF. "C"	тос	OUTLET	DA #	AREA (ha)	RUNOFF COEF. "C"	тос	OUTLET
1	0.1855	0.44	10 min	101	14	0.1978	0.44	10 min	115	27	0.1042	0.44	10 min	127	40	0.3664	0.58	10 min	29
2	0.1336	0.44	10 min	105	15	0.1867	0.58	10 min	19	28	0.2532	0.58	10 min	16	41	0.3189	0.58	10 min	30
3	0.0748	0.44	10 min	105	16	0.1747	0.58	10 min	20	29	0.3162	0.58	10 min	15	42	0.1657	0.44	10 min	Pond
4	0.2038	0.58	10 min	3	17	0.2674	0.44	10 min	119	30	0.3435	0.58	10 min	17	43	0.0477	0.58	10 min	28
5	0.1376	0.58	10 min	4	18	0.1676	0.58	10 min	21	31	0.2449	0.58	10 min	18	44	0.5827	0.3	10 min	Pond
6	0.2324	0.58	10 min	5	19	0.1328	0.58	10 min	22	32	0.1626	0.44	10 min	129	45	2.6716	0.3	10 min	uncontrolled
7	0.2735	0.58	10 min	6	20	0.0848	0.58	10 min	27	33	0.1954	0.58	10 min	24	IFGEN	ND:			
8	0.0709	0.44	10 min	109	21	0.3133	0.58	10 min	12	34	0.1642	0.58	10 min	23	STORM	DRAINAGE BOUNI)ARY		
9	0.3564	0.58	10 min	7	22	0.0692	0.58	10 min	11	35	0.1662	0.58	10 min	26					١
10	0.1775	0.58	10 min	8	23	0.1666	0.44	10 min	123	36	0.1306	0.58	10 min	25		AGE AREA NUMBER	₹ —►	0.12 0.58)
11	0.0680	0.58	10 min	9	24	0.0911	0.44	10 min	123	37	0.1191	0.44	10 min	Uncontrolled		IN HECTARES -			
12	0.0375	0.58	10 min	10	25	0.2445	0.58	10 min	14	38	0.0310	0.58	10 min	31	FUTUR	F DEVELOPMENT			
13	0.0738	0.44	10 min	113	26	0.3912	0.58	10 min	13	39	0.0305	0.58	10 min	32	EXTER	NAL 2.78AC $=$			AC=14.00
															EXTERI EXTERI	NAL TIME OF COI NAL BLENDED RU	NCENTRATION — JNOFF COEFFICIEI		<u>4.5 min </u> =0.70
							P	ROJECT NAME	AND ADDRESS:			TITLE:				SCALE:	1.1250	DRAWING	No.:
		7 UPDATE WES	T WATERCO	URSE	07/31/24		/ANCE			VOTE	סיפ					DRAFTED I	BY:		
		6 UPDATE			06/19/24	eng.services.ca@	GINEERING					PUST	-DEV	ELOF	'IVIE				
		2 PEER REVIEW	COMMENTS	S	11/08/22	APPLICANT:	<u></u>	MEAL	JOW S	ORDI	VISION	DRA	INA	GE AF	REAS		No.: 0114) -2
		1 INITIAL ISSUE			03/10/22			COUNTY	YRD No. 2	22, CAF	RDINAL, ON					DATE:			
							L, D.										10 2024		

a)	RUNOFF COEF. "C"	тос	OUTLET	DA #	AREA (ha)	RUNOFF COEF. "C'	, TOC	OUTLET	DA #	AREA (ha)	RUNOFF COEF. "C"	тос	OUTLET	DA #	AREA (ha)	RUNOFF COEF. "C"	тос	OUTLET
	0.44	10 min	101	14	0.1978	0.44	10 min	115	27	0.1042	0.44	10 min	127	40	0.3664	0.58	10 min	29
	0.44	10 min	105	15	0.1867	0.58	10 min	19	28	0.2532	0.58	10 min	16	41	0.3189	0.58	10 min	30
	0.44	10 min	105	16	0.1747	0.58	10 min	20	29	0.3162	0.58	10 min	15	42	0.1657	0.44	10 min	Pond
	0.58	10 min	3	17	0.2674	0.44	10 min	119	30	0.3435	0.58	10 min	17	43	0.0477	0.58	10 min	28
	0.58	10 min	4	18	0.1676	0.58	10 min	21	31	0.2449	0.58	10 min	18	44	0.5827	0.3	10 min	Pond
	0.58	10 min	5	19	0.1328	0.58	10 min	22	32	0.1626	0.44	10 min	129	45	2.6716	0.3	10 min	uncontrolled
	0.58	10 min	6	20	0.0848	0.58	10 min	27	33	0.1954	0.58	10 min	24	LEGEN	JD:			
	0.44	10 min	109	21	0.3133	0.58	10 min	12	34	0.1642	0.58	10 min	23	STORM	DRAINAGE BOUNI)ARY		
	0.58	10 min	7	22	0.0692	0.58	10 min	11	35	0.1662	0.58	10 min	26					Λ
	0.58	10 min	8	23	0.1666	0.44	10 min	123	36	0.1306	0.58	10 min	25		GE AREA NUMBER	<►	0.12 0.58)
	0.58	10 min	9	24	0.0911	0.44	10 min	123	37	0.1191	0.44	10 min	Uncontrolled		IN HECTARES			
	0.58	10 min	10	25	0.2445	0.58	10 min	14	38	0.0310	0.58	10 min	31	FUTUR	F CUEFFICIENT -			
	0.44	10 min	113	26	0.3912	0.58	10 min	13	39	0.0305	0.58	10 min	32	EXTERI	NAL 2.78AC $=$			<u></u>
														EXTERI EXTERI	NAL TIME OF COI NAL BLENDED RU	NCENTRATION — INOFF COEFFICIEI	$ \begin{array}{c} \bullet & & Tc=1 \\ & & \bullet & C \\ & & \bullet & C \\ & & & \bullet & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & C \\ & & & & & C \\ & & & & & C \\ & & & & & C \\ & & & & & C \\ & & & & & & & & \\ & &$	<u>4.5 min </u> =0.70
						P	ROJECT NAME	AND ADDRESS:			TITLE:				SCALE:	1.1250	DRAWING I	No.:
7	UPDATE WES	T WATERCO	URSE O	7/31/24		/ANCE				סיכ	ПООТ				DRAFTED I	BY:	-	
6	UPDATE		0	6/19/24	eng.services.ca@	GINEERING Ogmail.com					P051	-DEV	ELOP			N		
2		COMMENTS	5 11 -	1/08/22	APPLICANT:			JON 2	URDI	V1210IN	DRA	INA	GE AR	REAS		0114) -2
			0.	3/10/22 DATE	EDWARDSBURGH	ILTD.	COUNTY	' RD No. 2	22, CAF	RDINAL, ON					DATE:		-	
No	· REVISION / I	SSUE	N	MM/DD/YY				Page 19	4 of 465						06	-19-2024		

Time of Concentration	
Overland Flow Image: The sequence of the sequenc	$107.0 \left(\frac{nL^{0.333}}{S^{0.2}} \right)$
C Branchu) (illiama an	
Overland sheet flow length	AOE metre
Slope of surface	1.00 %
Manning 'n' of surface	0.030
Overland time of concentration	25.3 minutes
Kerb Gutter Flow Time	
Kerb Gutter flow length	0.0 metre
Longitudinal Gutter slope	1.000 %
Kerb Gutter flow time	0.0 minutes
Conduit Travel Time	
Pipe Length	0.00 metre
Pipe Gradient	1.000 %
Pipe Manning 'n'	0.013
Pipe C Channel	
Pipe Diameter	0.200 metre
Pipe Travel Time	0.0 minutes
Total Time of Concentration	25.34 minutes

Time of Concentration	
Overland Flow C Friend's eq. (\bullet Kinematic Wave eq. C Airport method C Branchu Williams eq.	$5.989 \left(\frac{Ln}{\sqrt{S}} \right)^{0.6} i_{eff}^{-0.4}$
Overland sheet flow length Slope of surface Manning 'n' of surface	495 metre 1.00 % 0.030
Effective rainfall intensity Overland time of concentration	53 mm/hr 28.7 minutes
Kerb Gutter Flow Time Kerb Gutter flow length Longitudinal Gutter slope Kerb Gutter flow time	0.0 metre 1.000 % 0.0 minutes
- Conduit Travel Time Pipe Length Pipe Gradient Pipe Manning 'n' © Pipe © Channel	0.00 metre 1.000 % 0.013
Pipe Diameter Pipe Travel Time	0.200 metre 0.0 minutes
Total Time of Concentration	28.69 minutes

C Friend's eq. C Kinematic Wave eq. C Airport method C Bransby-Williams eq. Uverland sheet flow length Slope of surface Catchment area Uverland time of concentration Kerb Gutter Flow Time	495 1.00 11 22.2	metre % hectares
C Kinematic Wave eq. Airport method Bransby-Williams eq. Overland sheet flow length Slope of surface Catchment area Overland time of concentration Kerb Gutter Flow Time	<0.4 495 1.00 11 22.2	metre % hectares
Airport method Sansby-Williams eq. Overland sheet flow length Catchment area Overland time of concentration Zether Flow Time	495 1.00 11	metre % hectares
Gensby-Williams eq. Overland sheet flow length Slope of surface Catchment area Overland time of concentration Kerb Gutter Flow Time	495 1.00 11 22.2	metre % hectares
Overland sheet flow length If Slope of surface If Catchment area If Overland time of concentration If Kerb Gutter Flow Time	495 1.00 11 22.2	metre % hectares
Slope of surface Tachment area	1.00	% hectares
Catchment area	22.2	hectares
Overland time of concentration	22.2	
Kerb Gutter Flow Time		minutes
Kerb Gutter flow length	0.0	metre
Longitudinal Gutter slope	1.00	%
Kerb Gutter flow time	0.0	minutes
Conduit Travel Time		
Pipe Length	0.00	metre
Pipe Gradient	1.000	%
Pipe Manning 'n'	0.013	
Pipe C Channel		
Pipe Diameter	0.200	metre
Pipe Travel Time	0.0	minutes
Total Time of Concentration	22.20	minutes

Parameter	Value	U	Notes
Sheet Flow	Enable		
Top Elevation	84.000	m	
Bottom Elevation	83.000	m	
Length	80.000	m	Recommended length not to exceed 30 m. Maximum length
Manning's n	0.0300		See HDS-2 Table 2.1
2-year 24-hour precipitation depth	53.0000	mm	
Slope	0.0125	m/m	
Time of Concentration	8.7442	min	HDS-2 Equation 2.6
Shallow Concentrated Flow	Enable		
Top Elevation	83.000	m	
Bottom Elevation	80.000	m	
Length	300.000	m	
k (0.076-0.619)	0.213		See HDS-2 Table 2.2
Slope	0.010	m/m	
Velocity	0.214	m/s	HDS-2 equation 2.7
Time of Concentration	23.338	min	
Channel Flow	Enable		
Total Time of Concentration			
Time of Concentration	32.082	min	
This solution is a final solution.			

Page 195 of 465





<u>NOTES</u>

* DISTANCES ARE IN METRE

IMPERVIOUSNESS RATIO AND WEIGHTED WEIGHTED RUNOFF COEFFICIENT (1:750) (DRIVEWAY WIDTH 3.5m AND 6.0m) TOTAL DRAINAGE AREA = 6161.4 m² TOTAL AREA OF THE 8 LOTS = 4893 m² TOTAL AREA OF THE 8 ROOFS (MAX OF 30%) = 0.30 x 4893 = 1467.90 m² TOTAL AREA OF THE 8 DRIVEWAYS = 8 x 12.50 x 3.50 (MAX. WIDTH)= 350.00 m² AREA OF STREET PAVEMENT = 63.4 x 7.46 = 473 m² AREA OF FUTURE SIDEWALK = 63.4 x 1.5 = 95 m²

SUBEACE	ADEA (m2)	Runoff Coeff. C			
JURFACE	AREA (III)	2-5 year	100 year		
Roof Area	1467.9	0.9	1.0		
Driveways	350	0.9	1.0		
Paved road – Asphalt	473	0.9	1.0		
Sidewalk	95	0.9	1.0		
Total Impervious Area	2385.9	14			
Total Catchment Area	6161.4	-			
Total Pervious Area	3775.5	0.3	0.375		
Weighted C (Cavg)		0.53	0.62		
Imperviousness %		39%			

Runoff Coefficient and Imperviousness Ratio 6.0m DW									
SUDEACE	ADEA (m2)	Runoff	Coeff. C						
SURFACE	AREA (III-)	2-5 year	100 year						
Roof Area	1467.9	0.9	1.0						
Driveways	600	0.9	1.0						
Paved road - Asphalt	473	0.9	1.0						
Sidewalk	95	0.9	1.0						
Total Impervious Area	2635.9								
Total Catchment Area	6161.4	-							
Total Pervious Area	3525.5	0.3	0.375						
Weighted C (Cavg)		0.56	0.64						
Imperviousness %		43%							

RUNOFF CALCULATIONS – RATIONAL METHOD

	Q _{2,5,25,100-y}	r = 2.78	BCI _{2,5,25,1}	_{00-yr} A
Rainfall Intensity I (mm/hr)		Pre-Dev.	Post-Dev.	
	Tc (min) =	20	15	
2 year	I ₂ =	52.03	61.77	
5 year	I ₅ =	70.25	83.56	
25 year	I ₂₅ =	97.26	97.26	
100 year	I ₁₀₀ =	119.95	142.89	

Runoff Coefficient C

Surface Type	C*
Impervious: Rooftop-Asphalt Pavement-Driveway	0.9
Road Shoulders	0.7
Grass-Cultivated-Pasture	0.2-0.4

* For Q $_{\rm 100yr}$ add 25% to C value. For $\rm ~Q_{25yr}$ add 10% to C value.

* Table 5.7 Ottawa Sewer Design Guidelines – October 2012

PRE-DEVELOPMENT RUNOFF CALCULATION									
Catchment	ID	Area (ha)	Percent of Total Area	C*	A x C (ha)	C relative	Q 2- year (L/s)	Q 5- year (L/s)	Q 100- year (L/s)
Subdivision Area	A1	7.6725	70.21	0.3	2.3018	0.21	332.9	449.5	959.4
Block A and C	A2	3.2550	29.79	0.3	0.9765	0.09	141.2	190.7	407.0
TOTAL SITE	AREA	10.9275	100%		3.2783		474	640	1,366
Weighted C (C _{avg})=						(C _{avg})=	0.300	0.300	0.375
Calculation using Cava :Q (L/s)=						2 (L/s)=	474	640	1366

II/ POST-DEVELOPMENT RUNOFF CALCULATION

Catchment	ID	Area (ha)	Percent of Total Area (%)	с	A x C (ha)	C relative	Q 2- year (L/s)	Q 5- year (L/s)	Q 100- year (L/s)	Q ₁₀₀₁ Con Measur	,by trol e (L/s)
										CONT.	UNC.
Subdivision	A1 to A36 & A38 to A44	8.1368	74.46	0.56	4.5566	0.417	782.4	1,058.4	2,069	2,069	
Open Space	A45	2.6716	24.45	0.30	0.8015	0.073	137.6	186.2	398		398
Uncontrolled Area	A37	0.1191	1.09	0.56	0.0667	0.006	11.5	15.5	30		30
TOTAI	<u> </u>	10.9275	100%		5.4248		932	1,260	2,497	2,069	428
Weighted C (C _{avg})=					0.50				2,4	97	

C= 0.64 instead of 0.56 for 100 y events

III/ ALLOWABLE RELEASE RATE IN DETENTION BASIN

A45: is unaltered and uncontrolled, therefore it is removed from the calculation of the storage A37: is altered and uncontrolled, it is post development runoff is considered in the calculation of the storage

PRE-DEVELOPMENT RUNOFF TO BE MATCHED BY POST-DEVELOPMENT

Catchment	ID	Area (ha)	Percent of Total Area	C*	A x C (ha)	C relative	Q 2- year (L/s)	Q 5- year (L/s)	Q 100- year (L/s)
Subdivision Area	A1 to A36 & A38 to A44	8.1368	98.56	0.3	2.4410	0.30	353.1	476.7	1,017.5
Uncontrolled Area	A37	0.1191	1.44	0.3	0.0357	0.00	5.2	7.0	14.9
TOTAL SITE	8.2559	100%		2.4768		358	484	1,032	
Weighted C (C _{avg})=								0.300	0.375
								404	4022

Calculation using C_{avg} :Q (L/s)= 358 484 1032

Post-Dev. n-y Relea	se Rate From A1 to A44	<	Pre-Dev. n-y Rate From A1 to A44				
Post-Dev. n-y Relea and A38	se Rate From A1 to A36 to A44 (Pond)	<	Pre-Dev. n-y Rate From A1 to A36 (-) Difference Post Dev and Pr	6 and A38 to A44 re Dev of A37			
2у	782.4	controlled	353.1 - (11.5-5.2)	346.8			
5у	1,058.4	to	467.7 – (15.5-7.0)	468.2			
100y	2263,0		1017.5 – (33-14.9)	1,002.1			

DESIGN STORMS USED IN SWMM MODEL SIMULATION



CHICAGO STORM 4 HOURS 2-YEAR

CHICAGO STORM 4 HOURS 5-YEAR



CHICAGO STORM 4 HOURS 100-YEAR



HISTORIC STORM AUG 8 1996



HISTORIC STORM AUG 4 1988



HISTORIC STORM JUL 1 1979



CHICAGO STORM 4HRS 100-Y + 20%





PRE-DEVELOPMENT – POST DEVELOPMENT RUNOFFS

Catchment Area = 8.1368 ha, Area A45 not included

	2-YEAR	5-YEAR	100-YEAR	100-YEAR +20%	NOTER
HTDROLOGT METHOD	(L/s)	(L/s)	(L/s)	(L/s)	NOTES
I/ PRE-DEVELOPMENT					
RATIONAL METHOD	353.1	476.7	1017.5		C=0.3, C(100)=0.375 T=20
CHICAGO STORM 3-HRS		244.2	1465.8		
CHICAGO STORM 4-HRS	11.0	168.2	1017.5		AREA= 8.1368 ha
CHICAGO STORM 6-HRS			1623.0		0% IMPERVIOUS
HISTORIC STORM JULY1, 79			1437.3		SLOPE= 2%
HISTORIC STORM AUGUST 8, 96			747.7		DIRECT LINK
SCS 100 – 24 HRS			896.6		
II/ POST-DEVELOPMENT					
RATIONAL METHOD	782.4	1058.4	2069.0		C = 0.56 C(100)= 0.64 T=15
CHICAGO STORM 3-HRS		837.2	1824.7		
CHICAGO STORM 4-HRS	565.3	898.9	2096.9	2543.6	AREA= 8.1368 ha
CHICAGO STORM 6-HRS			1898.1		43% IMPERVIOUS
HISTORIC STORM JULY1, 79			1457.0		SLOPE= 2%
HISTORIC STORM AUGUST 8, 96			989.3		DIRECT LINK
SCS 100 – 24 HRS			1127.1		
MAXIMUM STORM	565.3	898.9	2096.9		

Parameters used in SSA input

Split Drainage (Ref Lot 32)

Drainage Area	Imperviousness %	No Depression in Imp. %	Imp. To Perv. %
Rear Yard	27	100	100
Front Yard	59	33	33

Back to Front Drainage (Ref Lot 87)

Drainage Area	Imperviousnes s %	No Depression in Imp. %	Imp. To Perv. %
Rear & Front Yard	42	54	54

PRE-DEVELOPMENT – POST DEVELOPMENT OUTFALL DISCHARGE

	2-YEAR	5-YEAR	100-YEAR		
	(L/s)	(L/s)	(L/s)		
I/ PRE-DEVELOPMENT					
RATIONAL METHOD	353.1	476.7	1017.5		
CHICAGO STORM 4-HRS	11.0	168.2	1017.5		
II/ POST-DEVELOPMENT		-	-		
RATIONAL METHOD – NO RESTRICT	782.4	1058.4	2069.0		
CHICAGO STORM 4-HRS (I)	214.2	371.6	939.0		
TARGET PRE-DEVELOPMENT (RM) (II)	346.8	468.2	1002.1		
DIFFERENCE (CHICAGO STORM) (I)-(II)	-132.6	-96.6	-63.1		

POND:

BOTTOM ELEV. =	79.4		
STORM EVENT	2-Y EVENT	5-Y EVENT	100-Y EVENT
REQUIRED STORAGE VOLUME cu.m	356.4	574.7	1180.9
MAX. SWEL (SURFACE WATER ELEVATION)	79.87	80.12	80.70
WATER DEPTH IN POND	0.47 m	0.72 m	1.30 m

OUTLET STRUCTURE DESIGN (RECTANGULAR):

I/ 2 – RECTANGULAR ORIFICES 300 x 300 mm	
CREST ELEV. =	79.4
ORIFICE COEFFICIENT =	0.616
II/ 1 – RECTANGULAR WEIR 1.2 x 0.3 m	
CREST INVERT ELEV. =	80.0
DISCHARGE COEFFICIENT =	1.84
III/ CULVERT HDPE	
DIAMETER =	750 mm
SLOPE =	0.60%
IV/ SPILLWAY 3.0 x 0.2 m (RECT. WEIR)	
CREST INVERT ELEV. =	81.1
DISCHARGE COEFFICIENT =	1.84

HYDROLOGICAL MODELING AND C	ATCHMENT PROPERTIES
Infiltration losses modeled using Hor	rton's infiltration equation
$f(t) = f_c + (f_o - f_c)e^{-k(t)}$	
Initial infiltration rate:	76.2 mm/hr
Final infiltration rate:	13.2 mm/hr
Decay Coefficient:	K = 4.14 /hr
Depression Storage:	
Pervious areas:	4.67 mm
Impervious areas:	1.57 mm
N-Pervious:	0.015
N-Impervious:	0.15 (Post) and 0.20 (Pred
Width of catchment Catchment width	n: Area / Longest flow path
Default values for the City of Ottawa	have been used.

Lockmaster Meadow Subdivision Dry Pond Storage Stages

Contour	Depth (Head)	Contour Area	Storage Volume (cu.m)		
	(m)	(sq.m)			
79.40	0	716.28	0		
79.50	0.1	751.81	73.4		
79.60	0.2	788.35	150.41		
79.70	0.3	825.46	231.1		
79.80	0.4	863.12	315.53		
79.90	0.5	901.34	403.75		
80.00	0.6	940.11	495.82		
80.10	0.7	979.44	591.8		
80.20	0.8	1019.33	691.74		
80.30	0.9	1059.77	795.7		
80.40	1	1100.77	903.73		
80.50	1.1	1142.33	1015.89		
80.60	1.2	1184.45	1132.23		
80.70	1.3	1227.12	1252.81		
80.80	1.4	1270.34	1377.68		
80.90	1.5	1314.13	1506.9		

Page 1

Parameters used in SSA input

Manning's Roughness for Overland Flow	a Barrel
Land Surface Type	Manning n
Urban:	1
Concrete, Asphalt, or Gravel	0.005 - 0.015
Average Grass Cover	0.40
Rural Residential (1 - 10 acre lots, maintenance or grazing assumed)	0.40
Urban Residential (maintained lawns assumed, with effects of landscaping, driveways, roofs included in combined value):	
1 - 3 building units/acre	0.30
3 - 10 building units/acre	0.20
> 10 building units/acre	0.15
Commercial/Industrial (effects of landscaping, driveways, roofs included in combined value)	0.11
Grass:	
Average Grass Cover	0.40
Poor Grass Cover, Moderately Rough Surface	0.30 - 0.40
Light Turf	0.20
Dense Turf	0.17 - 0.80
Dense Grass	0.17 - 0.30
Bermuda Grass	0.30 - 0.48
Dense Shrubbery and Forest Litter	0.40
Natural:	
Short Grass Prairie	0.10 - 0.20
Poor Grass Cover, Moderately Rough Surface	0.30 - 0.40
Sparse Vegetation	0.05 - 0.13
Oak Grasslands, Open Grasslands	0.60
Dense Cover of Trees and Bushes	0.80
Rangeland:	
Typical	0.13
No Debris Cover	0.09 - 0.34
20% Debris Cover	0.05 - 0.25
Woods:	
Light Underbrush	0.40
Dense Underbrush	0.80
Rural Residential (1 - 10 acre lots, maintenance or grazing assumed)	0.40
Cultivated Areas:	
Bare Packed Soil (free of stone)	0.10
Fallow (no residue)	0.05
Conventional Tillage:	
No Residue	0.06 - 0.12
With Residue	0.16 - 0.22
Chisel Plow:	
No Residue	0.06 - 0.12
With Residue	0.10 - 0.16
Fall Disking (with residue)	0.30 - 0.50
No Till:	
No Residue Cover	0.04 - 0.10
20 - 40% Residue Cover	0.07 - 0.17
60 - 100% Residue Cover	0.17 - 0.47
Rural Residential (1 - 10 acre lots, maintenance or grazing assumed)	0.40
Sources: -USACE, 1998, HEC-1 Flood Hydrograph Package User's Manual, Hydrologic Enginee CA -Soil Conservation Service, 1986, Urban Hydrology for Small Watersheds, Technical Re Department of Agriculture, Washington, DC	ring Center, Davis, elease 55, U.S.

Table for Manning n for Overland Flow for Various Surfaces

SCS Soil Group	f0 (mm.hour)	fc (mm/hour)	k (1/hour)
A	250	25.4	2
в	200	12.7	2
с	125	6.3	2
D	76	2.5	2

Drifice Coefficients	
Orifice Shape	C
Circular	0.614
Triangular	0.615
Square with Vertical Walls	0.616
Rectangular	
Side ratio of 4.1, long side in vertical direction	0.626
Side ratio of 4.1, long side in horizontal direction	0.627
Side ratio of 10:1, long side in vertical direction	0.637
Side ratio of 10:1, long side in horizontal direction	0.637

Page 1/1

vpical Infiltration	Rates	
Surface	infiltra	tion
	US Units	Metric Unit
Dry Soils (with Little of	or no Vegetation):	
Sandy Soils	5.00 in/hr	127 mm/hr
Loam Soils	3.00 in/hr	76 mm/hr
Clay Soils	1.00 in/hr	25 mm/hr
Dry Soils (with Dense	Vegetation):	
Sandy Soils	10.00 in/hr	254 mm/hr
Loam Soils	6.00 in/hr	152 mm/hr
Clay Soils	2.00 in/hr	51 mm/hr
Moist Soils (with Little Dried Out, i.e., Field C	e or no Vegetation, which f apacity):	nave Drained but not
Sandy Soils	1.50 in/hr	38 mm/hr
Loam Soils	1.00 in/hr	25 mm/hr
Clay Soils	0.30 in/hr	8 mm/hr
Moist Soils (with Den out, i.e., Field Capacit	se Vegetation, which have y):	Drained but not Dried
Sandy Soils	3.50 in/hr	89 mm/hr
Loam Soils	2.00 in/hr	51 mm/hr
Clay Soils	0.70 in/hr	18 mm/hr
Moist Soils (Close to	Saturation) :	
Use value close to M	linimum Infiltration Rate (se	ee below)
Moist Soils (with Little Out, i.e., Field Capacit	e or no Vegetation, which f ty):	nave Partially Dried
Sandy Soils	2.00 - 3.30 in/hr	51 - 84 mm/hr
Loam Soils	1.20 - 2.00 in/hr	30 - 51 mm/hr
Clay Soils	0.40 - 0.70 in/hr	10 - 18 mm/hr
Moist Soils (with Den i.e., Field Capacity):	se Vegetation, which have	Partially Dried Out,
Sandy Soils	4.00 - 6.50 in/hr	102 - 165 mm/hr
Loam Soils	2.50 - 4.00 in/hr	64 - 101 mm/hr
Clay Soils	0.80 - 1.30 in/hr	20 - 33 mm/hr

Table for Horton Infiltration Rates For Various Soils





MAJOR SYSTEM DESIGN





CTY RD CULVERT - UPSTREAM SIDE

-	Dennes [Parameter	Value	Units
21_		Flow	7.000	cms
3.0	H · Tv	Depth	1.513	m
3.0	H TV	Area of Flow	2.422	m^2
0.0	lid	Wetted Perimeter	4.191	m
1.900000	(m)	Hydraulic Radius	0.578	m
0.01	(m/m)	Average Velocity	2.891	m/s
0.01	hund	Top Width (T)	1.530	m
: [0.0240		Froude Number	0,733	
		Critical Depth	1.299	m
		Critical Velocity	3,389	m/s
7.000	(cms)	Critical Slope	0.01439	m/m
1 612	Text	Critical Top Width	1.767	m
11:010	(in)	Calculated Max Shear Stress	148.345	N/m^
		Calculated Avg Shear Stress	56.640	N/m^
	11	Depth vs. Flow - Doubl		
Chan	1	Depth vs.	Flow	
Chan	nel	2.0 E Depth vs.	Flow	4
Cham		2.0 1.5	Flow	,
Chan		2.0 1.5	Flow	1
Chan	nel	Depth vs.	Flow	1
Chan	nel	2.0 1.5 1.0	Flow	1
Chan	nel	Depth vs.	Flow	1
Cham	mel (m) (m)	2.0 1.5 1.0 0.5	Flow	1
Chan	nel	2.0 1.5 1.0 0.5	Flow	-
Chan	nel	Depth vs.	Flow	
	3.0 3.0 0.0 1.900000 0.01 0.0240 7.000 1.513 culate Compl	3.0 He To 3.0 He To 3.0 He To 3.0 He To 3.0 He To 3.0 He To 3.0 He To 3.0 He To 0.0 Ito 1.9000000 (m) 0.01 0.01 (m/m) 0.0240 (m) 1.513 (m) culate Compute Curves	Image: Stress stress stress stress stress Image: Stress stress stress stress stress stress stress stress stress	Image: Second state state Flow 7,000 3.0 H 11/ Depth 1,513 3.0 H 11/ Depth 1,513 3.0 H 11/ Area of Flow 2,422 0.0 (m) Vetted Perimeter 4,191 1.3000000 (m) Average Velocity 2,891 0.01 (m/m) 1,530 Froude Number 0,733 Critical Depth 1,299 Critical Slope 0,01439 Critical Slope 0,01439 Critical Top Width 1,767 Calculated Max Shear Stress 148.345 Calculated Avg Shear Stress 56.640











Ottawa Sewer Guidelines Model STORM SEWER DESIGN CALCULATION SHEET (RATIONAL METHOD)

Return frequency = 5 years

	LOCA	ΓΙΟΝ		RUNOFF FLOW							SEWER DESIGN								
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Street Name	From	To	Catchment	Indiv Area (ha)	Indiv R (See tables)	Indiv.	Accum.	Time of Conc.	Rainfall Intensity	Peak Flow Q _p	Pipe Nominal Dia.	Pipe Actual Int. Dia.	Type of Pipe	Slope s	Length	Pipe Capacity Q _f	Full Flow Velocity V _f	Time of Flow	Q _p / Q _f
	00110.	00110.			,	2.78 AR	2.78 AR	(min)	(mm/hr)	(m³/s)	(mm)	(mm)		%	(m)	(m³/s)	(m/s)	(min)	%
Otres et D	404	400		0.4055	0.50	0.00	0.00	40.00	404.0	0.000	200	000	DDac	0.05	20.0	0.070	1.10	0.50	000/
Street B	101	103	A1	0.1855	0.50	0.29	0.29	10.00	104.2	0.030	300	300	DR35	0.05	38.8	0.078	1.10	0.59	39% 11%
Sileer D	103	105	Δ2	0.0000	0.50	0.00	0.29	10.59	101.2	0.029	300	300	DR35	0.55	14.1	0.072	1.01	0.23	41/0
Street B	105	107	A2 A3	0.1330	0.56	0.21	0.50	10.82	100.1	0.061	450	457	Conc.	0.30	57.9	0.163	0.99	0.97	38%
			A4	0.2038	0.56	0.32	0.93												
Street B	107	109	A5	0.1376	0.56	0.21	1.14	11.79	95.6	0.109	450	457	Conc.	0.62	66.5	0.234	1.43	0.78	47%
			A6	0.2324	0.56	0.36	1.51												
Street B	109	111	A7	0.2735	0.56	0.43	1.93	12.57	92.3	0.189	525	533	Conc.	0.32	41.0	0.253	1.14	0.60	74%
			A8	0.0709	0.56	0.11	2.04												
Street B	111	113	A9	0.3564	0.56	0.55	2.60	13.17	90.0	0.259	600	610	Conc.	0.32	41.6	0.363	1.24	0.56	71%
			A10	0.1775	0.56	0.28	2.87												
Ctreat D	442	445	A11	0.0680	0.56	0.11	2.98	40.70	07.0	0.077		610	Como	0.50	744	0.402	1.00	0.70	FC0/
Street B	113	115	A12	0.03/5	0.56	0.06	3.04	13.73	87.9	0.277	600	610	Conc.	0.59	74.1	0.493	1.69	0.73	50%
			Δ14	0.0730	0.56	0.11	3.15												
			A15	0.1867	0.56	0.29	3 75												
			A16	0.1747	0.56	0.27	4.02			• • • •				0.00	0	0 505	4.70		
Street B	115	117	A17	0.2674	0.56	0.42	4.44	14.46	85.3	0.419	600	610	Conc.	0.62	75.9	0.505	1.73	0.73	83%
			A18	0.1676	0.56	0.26	4.70												
			A19	0.1328	0.56	0.21	4.91												
			1																
Street B	121	123		0.0000	0.56	0.00	0.00	10.00	104.2	0.000	300	300	DR35	0.65	14.4	0.078	1.10	0.22	0%
Street D	400	405	A21	0.3133	0.56	0.49	0.49	10.22		0 000	275	201	0025	0.26	70.0	0.110	0.00	4.00	000/
Street B	123	125	A22	0.0692	0.50	0.11	0.60	10.22	103.1	0.088	375	381	DR35	0.30	70.9	0.110	0.96	1.23	80%
			A23	0.1000	0.56	0.20	1.00												
Street B	125	127	Δ25	0.0311	0.56	0.38	1.00	11 45	97 1	0 193	525	533	Conc	0.35	61 1	0 265	1 19	0 86	73%
			A26	0.3912	0.56	0.61	1.99		07.1	0.100	020	000	Cono.	0.00	01.1	0.200	1.10	0.00	1070
			A27	0.1042	0.56	0.16	2.15	10.00	00.4			500		0.00	70.0	0.050			
Street B	127	129	A29	0.3162	0.56	0.49	2.64	12.30	93.4	0.247	525	533	Conc.	0.32	72.0	0.253	1.14	1.06	97%
Street A	135	129	A30	0.3435	0.56	0.53	0.53	10.00	104.2	0.095	375	381	DR35	0.40	94.6	0.116	1.01	1.55	83%
			A31	0.2449	0.56	0.38	0.92							50					
					DE 120		2 56	12.26	00.2	0 247									
			A28	0.2532	0.56	0.30	3.00	13.30	09.3	0.317									
Street B	129	131	Δ32	0.2332	0.50	0.33	4 20	13.36	89.3	0.375	600	610	Conc.	0.37	74.9	0.390	1.34	0.93	96%
			7.02	0.1020	0.00	0.20	1.20												
			A33	0.1954	0.56	0.30	4.51												
Street P	121	122	A34	0.1642	0.56	0.26	4.76	1/ 20	95.0	0 4 4 0	675	696	Conc	0.29	75.0	0.464	1.26	0.00	070/
Sueet D	131	155	A35	0.1662	0.56	0.26	5.02	14.29	00.9	0.449	075	000		0.20	75.0	0.404	1.20	0.99	JI 70
			A36	0.1306	0.56	0.20	5.23												
			A38	0.0310	0.56	0.05	5.27												
Street C	133	117	A39	0.0305	0.56	0.05	5.32	15.29	82.6	0.528	675	686	Conc.	0.46	106.6	0.595	1.61	1.10	89%
			A40	0.3664	0.56	0.57	5.89		-	-								-	
			A41	0.3189	0.56	0.50	6.39												

				AT NODE 117															
STREET B					FROM 115		4.91	14.46	85.3										
STREET C					FROM 133		6.39	16.39	79.3										
						TOTAL	11.30												
Street C	117	119 stc	A20	0.0848	0.56	0.13	11.43	16 20	79.3	0.912	900	914	Conc.	0.65	12.4	1.521	2.32	0.09	60%
			A43	0.0477	0.56	0.07	11.50	10.39											
				AT NO	DE 119														
PARK	119	121		0.0000	0.56	0.00	11.50	16.48	79.056	0.909	900	914	Conc.	0.63	23.8	1.497	2.28	0.17	61%
							at outfall	16.656	78.564	0.904									
			CHECK TOTAL CATCHMENT																
			AREA=	7.3885		NOTE: CONCRETE TRAPEZOIDAL CHANNELS COULD BE USED INSTEAD OF CONCRETE PIPES IN PARK AND LEADING													
			I=		TO THE DETENTION POND.														
			C=	0.56															
			Qp=	2.78*C*I*A=	0.904 m³/s														

Definitions:

- Q = Peak Flow in Litres per Second (L/s)
- Q = 2.78 *A*I*R , where
- Q = Peak Flow in Litres per Second (L/s)
- A = Areas in hectares (ha)
- I = Rainfall Intensity (mm/h)

R= Runoff Coefficient

 Q_{full} = 23.976 x D^{8/3} x S^{1/2} (for n = 0.013, D in metres)

Notes:

1- Manning formula used to calculate flow capacities

2- Hydraulic Toolbox software was used to calculate capacities and depths of flows

- 3- No projected carryover flow from east and west sides of the property
- 4- Minimum Tc is 10 min as per Ottawa Design Guidelines
- 5- Minimum permissible velocity in sewer: 0.76 m/s
- 6- Full flow velocity: V_{full} = 30.527 x D^{2/3} x S^{1/2} (for n = 0.013, D in metres)
- 7- The maximum flowing full velocity shall not be greater than 3.65 m/s.

8- Manholes shall be placed at the upstream end of each line, changes in size and material, at pipe 9- Manholes may be either pre-cast or poured/cast-in-place and shall be designed and constructed in accordance with Ontario Provincial Standard Drawings (OPSD) and Specifications. 10- All leads from catchbasins shall be 200 mm diameter PVC pipes

Rainfall Intensity Curves for Ottawa:

5 year rainfall intensity:	$I_5 = (998.071)/((T_c + 6.053)^{0.814})$	
25 year rainfall intensity:	$I_{25} = (1402.884)/((T_c + 6.018)^{0.819})$	
50 year rainfall intensity:	I ₅₀ = (1569.58)/((Tc +6.014) ^{0.82})	
100 year rainfall intensity:	I ₁₀₀ = (1735.688)/((Tc +6.014) ^{0.82})	

Street Names Street A: Balsam St Street B: Lockhouse St Street C: Conifer Ln

Hydraulic Design

Roughness coefficient (n) in Manning equation: PVC Pipe (DR35): n = 0.013 Concrete Pipe: n = 0.013

Concrete Culvert (smooth): n= 0.013

Grassed Channel: n=0.035

APPENDIX - D

CSO/STORMWATER MANAGEMENT



[®] HYDROVEX[®] VHV / SVHV Vertical Vortex Flow Regulator



JOHN MEUNIER
HYDROVEX® VHV / SVHV VERTICAL VORTEX FLOW REGULATOR

APPLICATIONS

One of the major problems of urban wet weather flow management is the runoff generated after a heavy rainfall. During a storm, uncontrolled flows may overload the drainage system and cause flooding. Due to increased velocities, sewer pipe wear is increased dramatically and results in network deterioration. In a combined sewer system, the wastewater treatment plant may also experience significant increases in flows during storms, thereby losing its treatment efficiency.

A simple means of controlling excessive water runoff is by controlling excessive flows at their origin (manholes). John Meunier Inc. manufactures the HYDROVEX[®] VHV / SVHV line of vortex flow regulators to control stormwater flows in sewer networks, as well as manholes.

The vortex flow regulator design is based on the fluid mechanics principle of the forced vortex. This grants flow regulation without any moving parts, thus reducing maintenance. The operation of the regulator, depending on the upstream head and discharge, switches between orifice flow (gravity flow) and vortex flow. Although the concept is quite simple, over 12 years of research have been carried out in order to get a high performance.

The **HYDROVEX**[®] **VHV** / **SVHV** Vertical Vortex Flow Regulators (**refer to Figure 1**) are manufactured entirely of stainless steel, and consist of a hollow body (1) (in which flow control takes place) and an outlet orifice (7). Two rubber "O" rings (3) seal and retain the unit inside the outlet pipe. Two stainless steel retaining rings (4) are welded on the outlet sleeve to ensure that there is no shifting of the "O" rings during installation and use.



FIGURE 1: HYDROVEX[®] VHV-SVHV VERTICAL VORTREX FLOW REGULATORS

ADVANTAGES

- The **HYDROVEX**[®] **VHV** / **SVHV** line of flow regulators are manufactured entirely of stainless steel, making them durable and corrosion resistant.
- Having no moving parts, they require minimal maintenance.
- The geometry of the **HYDROVEX**[®] **VHV** / **SVHV** flow regulators allows a control equal to an orifice plate, having a cross section area 4 to 6 times smaller. This decreases the chance of blockage of the regulator, due to sediments and debris found in stormwater flows. **Figure 2** illustrates the comparison between a regulator model 100 SVHV-2 and an equivalent orifice plate. One can see that for the same height of water, the regulator controls a flow approximately four times smaller than an equivalent orifice plate.
- Installation of the **HYDROVEX**[®] **VHV** / **SVHV** flow regulators is quick and straightforward and is performed after all civil works are completed.
- Installation requires no special tools or equipment and may be carried out by any contractor.
- Installation may be carried out in existing structures.



FIGURE 2: DISCHARGE CURVE SHOWING A HYDROVEX[®] FLOW REGULATOR VS AN ORIFICE PLATE

SELECTION

Selection of a **VHV or SVHV** regulator can be easily made using the selection charts found at the back of this brochure (see **Figure 3**). These charts are a graphical representation of the maximum upstream water pressure (head) and the maximum discharge at the manhole outlet. The maximum design head is the difference between the maximum upstream water level and the invert of the outlet pipe. All selections should be verified by John Meunier Inc. personnel prior to fabrication.

Example:

- ✓ Maximum design head 2m (6.56 ft.)
 - 6 L/s (0.2 cfs)
- ✓ Maximum discharge
 ✓ Using Figure 3 VHV
- 6 L/s (0.2 cfs) model required is a **75 VHV-1**

INSTALLATION REQUIREMENTS

All **HYDROVEX[®] VHV** / **SVHV** flow regulators can be installed in circular or square manholes. Figure 4 gives the various minimum dimensions required for a given regulator. *It is imperative to respect the minimum clearances shown to ensure easy installation and proper functioning of the regulator.*

In order to specify a **HYDROVEX**[®] regulator, the following parameters must be defined:

- The model number (ex: 75-VHV-1)
- The diameter and type of outlet pipe (ex: 6" diam. SDR 35)
- The desired discharge (ex: 6 l/s or 0.21 CFS)
- The upstream head (ex: 2 m or 6.56 ft.) *
- The manhole diameter (ex: 36" diam.)
- The minimum clearance "H" (ex: 10 inches)
- The material type (ex: 304 s/s, 11 Ga. standard)
- * Upstream head is defined as the difference in elevation between the maximum upstream water level and the invert of the outlet pipe where the HYDROVEX[®] flow regulator is to be installed.

PLEASE NOTE THAT WHEN REQUESTING A PROPOSAL, WE SIMPLY REQUIRE THAT YOU PROVIDE US WITH THE FOLLOWING:

- project design flow rate
- > pressure head
- chamber's outlet pipe diameter and type



Typical VHV model in factory



VHV-1-O (standard model with odour control inlet)



VHV with Gooseneck assembly in existing chamber without minimum release at the bottom



FV – SVHV (mounted on sliding plate)



FV – *VHV-O* (mounted on sliding plate with odour control inlet)



VHV with air vent for minimal slopes

A[®] HYDROVEX[®]



JOHN MEUNIER

FIGURE 3 - VHV

Model Number	Regulator Diameter		Minimum Manhole Diameter		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
50VHV-1	150	6	600	24	150	6	150	6
75VHV-1	250	10	600	24	150	6	150	6
100VHV-1	325	13	900	36	150	6	200	8
125VHV-2	275	11	900	36	150	6	200	8
150VHV-2	350	14	900	36	150	6	225	9
200VHV-2	450	18	1200	48	200	8	300	12
250VHV-2	575	23	1200	48	250	10	350	14
300VHV-2	675	27	1600	64	250	10	400	16
350VHV-2	800	32	1800	72	300	12	500	20

FLOW REGULATOR TYPICAL INSTALLATION IN CIRCULAR MANHOLE FIGURE 4 (MODEL VHV)



Model Number	Regulator Diameter		Minimum Chamber Width		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
50VHV-1	150	6	600	24	150	6	150	6
75VHV-1	250	10	600	24	150	6	150	6
100VHV-1	325	13	600	24	150	6	200	8
125VHV-2	275	11	600	24	150	6	200	8
150VHV-2	350	14	600	24	150	6	225	9
200VHV-2	450	18	900	36	200	8	300	12
250VHV-2	575	23	900	36	250	10	350	14
300VHV-2	675	27	1200	48	250	10	400	16
350VHV-2	800	32	1200	48	300	12	500	20

FLOW REGULATOR TYPICAL INSTALLATION IN SQUARE MANHOLE FIGURE 4 (MODEL VHV)

NOTE: In the case of a square manhole, the outlet flow pipe must be centered on the wall to ensure enough clearance for the unit.





INSTALLATION

The installation of a **HYDROVEX**[®] regulator may be undertaken once the manhole and piping is in place. Installation consists of simply fitting the regulator into the outlet pipe of the manhole. **John Meunier Inc.** recommends the use of a lubricant on the outlet pipe, in order to facilitate the insertion and orientation of the flow controller.

MAINTENANCE

HYDROVEX[®] regulators are manufactured in such a way as to be maintenance free; however, a periodic inspection (every 3-6 months) is suggested in order to ensure that neither the inlet nor the outlet has become blocked with debris. The manhole should undergo periodically, particularly after major storms, inspection and cleaning as established by the municipality

GUARANTY

The **HYDROVEX**[®] line of **VHV** / **SVHV** regulators are guaranteed against both design and manufacturing defects for a period of 5 years. Should a unit be defective, **John Meunier Inc.** is solely responsible for either modification or replacement of the unit.

John Meunier Inc. ISO 9001 : 2008 <u>Head Office</u> 4105 Sartelon Saint-Laurent (Quebec) Canada H4S 2B3 Tel.: 514-334-7230 www.johnmeunier.com Fax: 514-334-5070 cso@johnmeunier.com

Ontario Office

2000 Argentia Road, Plaza 4, Unit 430 Mississauga (Ontario) Canada L5N 1W1 Tel.: 905-286-4846 www.johnmeunier.com Fax: 905-286-0488 ontario@johnmeunier.com Page 223 of 465 USA Office 2209 Menlo Avenue Glenside, PA USA 19038 Tel.: 412- 417-6614 www.johnmeunier.com Fax: 215-885-4741 asteele@johnmeunier.com





Page 1





Province:	Ontario		Project Name:	LOCKMASTER'S N	EADOW	
City:	CARDINAL		Project Number:	114		
Nearest Rainfall Station:	KINGSTON		Designer Name:	M Mabrouk		
Climate Station Id:	6104142		Designer Company:	Engineer		
Years of Rainfall Data:	20		Designer Email:	eng.services.ca@	gmail.com	
			Designer Phone:	613-986-9170		
Site Name:	Lockmaster SUBDIVISION		EOR Name:			
Drainage Area (ha):	7.388		EOR Company:			
Runoff Coefficient 'c':	0.56		EOR Email:			
Particle Size Distribution:	Fine			Net Annu	al Sedime	nt
Target TSS Removal (%):	80.0			(TSS) Load	Reductio	n
Required Water Quality Run	off Volume Capture (%):	90.00		Sizing	Summary	
Estimated Water Quality Flo	w Rate (L/s):	120.45		Stormceptor	TSS Rem	oval
Oil / Fuel Spill Risk Site?		Yes		Model	Provideo	l (%)
Upstream Flow Control?		No		EFO4	43	
Peak Conveyance (maximun	n) Flow Rate (L/s):			EFO6	60	
Influent TSS Concentration (mg/L):			EFO8	71	
Estimated Average Annual S	ediment Volume (L/yr):	3080		EFO10	78	
				EFO12	83	
			Recommende	d Stormceptor EFC) Model:	EFO
	Fstimat	ted Net An	nual Sediment	(TSS) Load Reduc	tion (%):	83
		14	latar Quality B			
		vv	aler Quality N	mon volume cap	lure (<i>1</i> 0).	/ 9





THIRD-PARTY TESTING AND VERIFICATION

Stormceptor[®] **EF** and **Stormceptor**[®] **EFO** are the latest evolutions in the Stormceptor[®] oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** and performance has been third-party verified in accordance with the **ISO 14034 Environmental Technology Verification (ETV)** protocol.

PERFORMANCE

► Stormceptor® EF and EFO remove stormwater pollutants through gravity separation and floatation, and feature a patentpending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including highintensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterwavs.

PARTICLE SIZE DISTRIBUTION (PSD)

► The **Canadian ETV PSD** shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV *Procedure for Laboratory Testing of Oil-Grit Separators* for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle	Percent Less	Particle Size	Deserved
Size (µm)	Than	Fraction (µm)	Percent
1000	100	500-1000	5
500	95	250-500	5
250	90	150-250	15
150	75	100-150	15
100	60	75-100	10
75	50	50-75	5
50	45	20-50	10
20	35	8-20	15
8	20	5-8	10
5	10	2-5	5
2	5	<2	5







Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
0.50	8.1	8.1	5.75	345.0	33.0	100	8.1	8.1
1.00	18.9	27.0	11.50	690.0	66.0	100	18.9	27.0
2.00	16.7	43.7	23.00	1380.0	131.0	92	15.4	42.4
3.00	11.6	55.3	34.50	2070.0	197.0	84	9.8	52.2
4.00	10.6	65.9	46.01	2760.0	263.0	80	8.5	60.7
5.00	6.8	72.8	57.51	3450.0	329.0	78	5.3	66.0
6.00	5.2	78.0	69.01	4141.0	394.0	74	3.9	69.9
7.00	3.3	81.3	80.51	4831.0	460.0	71	2.3	72.2
8.00	3.6	84.9	92.01	5521.0	526.0	68	2.5	74.7
9.00	2.1	87.0	103.51	6211.0	592.0	65	1.4	76.0
10.00	2.4	89.4	115.02	6901.0	657.0	64	1.5	77.6
11.00	1.4	90.7	126.52	7591.0	723.0	64	0.9	78.4
12.00	1.9	92.6	138.02	8281.0	789.0	63	1.2	79.6
13.00	1.4	94.0	149.52	8971.0	854.0	63	0.9	80.5
14.00	0.7	94.7	161.02	9661.0	920.0	62	0.4	80.9
15.00	0.7	95.4	172.52	10351.0	986.0	62	0.4	81.4
16.00	0.5	95.9	184.03	11042.0	1052.0	60	0.3	81.7
17.00	0.3	96.2	195.53	11732.0	1117.0	59	0.2	81.8
18.00	0.3	96.4	207.03	12422.0	1183.0	57	0.2	82.0
19.00	0.0	96.4	218.53	13112.0	1249.0	56	0.0	82.0
20.00	0.6	97.1	230.03	13802.0	1314.0	54	0.3	82.3
21.00	0.3	97.4	241.53	14492.0	1380.0	53	0.2	82.5
22.00	0.0	97.4	253.04	15182.0	1446.0	51	0.0	82.5
23.00	0.0	97.4	264.54	15872.0	1512.0	48	0.0	82.5
24.00	0.0	97.4	276.04	16562.0	1577.0	47	0.0	82.5
25.00	0.0	97.4	287.54	17252.0	1643.0	45	0.0	82.5
30.00	0.9	98.3	345.05	20703.0	1972.0	37	0.3	82.8
35.00	1.1	99.4	402.56	24153.0	2300.0	32	0.4	83.2
40.00	0.6	100.0	460.07	27604.0	2629.0	28	0.2	83.4
45.00	0.0	100.0	517.57	31054.0	2958.0	25	0.0	83.4
			Es	timated Ne	t Annual Sedim	ent (TSS) Loa	d Reduction =	83 %

Climate Station ID: 6104142 Years of Rainfall Data: 20



Stormceptor[®]

Stormceptor* EF Sizing Report







Maximum Pipe Diameter / Peak Conveyance										
Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inle Diame	et Pipe eter	Max Outl Diamo	et Pipe eter	Peak Cor Flow	nveyance Rate	
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)	
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15	
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35	
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60	
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100	
EF12 / EFO12	3.6	12	90	1828	72	1828	72	2830	100	

SCOUR PREVENTION AND ONLINE CONFIGURATION

► Stormceptor® EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

DESIGN FLEXIBILITY

► Stormceptor[®] EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

► While Stormceptor[®] EF will capture and retain oil from dry weather spills and low intensity runoff, **Stormceptor[®] EFO** has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid reentrainment testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.













INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

i onutant capacity												
Stormceptor EF / EFO	Moo Diam	del eter	Depth Pipe In Sump	(Outlet vert to Floor)	Oil Vo	lume	Recomr Sedii Maintenan	mended ment Ice Depth *	Maxiı Sediment ^v	num Volume *	Maxin Sediment	ium Mass **
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(ft³)	(kg)	(lb)
EF4 / EFO4	1.2	4	1.52	5.0	265	70	203	8	1190	42	1904	5250
EF6 / EFO6	1.8	6	1.93	6.3	610	160	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	1070	280	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	1670	440	610	24	17790	628	28464	78500
EF12 / EFO12	3.6	12	3.89	12.8	2475	655	610	24	31220	1103	49952	137875

Pollutant Capacity

*Increased sump depth may be added to increase sediment storage capacity ** Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

Feature	Benefit	Feature Appeals To
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer
Third-party verified light liquid capture	Proven performance for fuel/oil hotspot	Regulator, Specifying & Design Engineer,
and retention for EFO version	locations	Site Owner
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer
Minimal drop between inlet and outlet	Site installation ease	Contractor
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner

STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef

STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef





STANDARD PERFORMANCE SPECIFICATION FOR "OIL GRIT SEPARATOR" (OGS) STORMWATER QUALITY TREATMENT DEVICE

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators**

1.3 SUBMITTALS

1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.

1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.

1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 – PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The minimum sediment & petroleum hydrocarbon storage capacity shall be as follows:

- 2.1.1 4 ft (1
 - 4 ft (1219 mm) Diameter OGS Units:
 6 ft (1829 mm) Diameter OGS Units:
 8 ft (2438 mm) Diameter OGS Units:
 10 ft (3048 mm) Diameter OGS Units:
 12 ft (3657 mm) Diameter OGS Units:

 $\begin{array}{l} 1.19 \ m^{3} \ sediment \ / \ 265 \ L \ oil \\ 3.48 \ m^{3} \ sediment \ / \ 609 \ L \ oil \\ 8.78 \ m^{3} \ sediment \ / \ 1,071 \ L \ oil \\ 17.78 \ m^{3} \ sediment \ / \ 1,673 \ L \ oil \\ 31.23 \ m^{3} \ sediment \ / \ 2,476 \ L \ oil \\ \end{array}$

PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall







remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m² to 1400 L/min/m², and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m² and 1400 L/min/m² shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 $L/min/m^2$ shall be assumed to be identical to the sediment removal efficiency at 40 $L/min/m^2$. No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 $L/min/m^2$.

3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m² shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m², and shall be calculated using a simple proportioning formula, with 1400 L/min/m² in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m².

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m².

3.4 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV **Program's Procedure for Laboratory Testing of Oil-Grit Separators,** with results reported within the Canadian ETV or ISO 14034 ETV verification. This reentrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to







Stormceptor[®] EF Sizing Report

assess whether light liquids captured after a spill are effectively retained at high flow rates.

3.4.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m² to 2600 L/min/m²) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators.** However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.





Page 234 of 465

APPENDIX - E







CULVERT OUTLET (BOTH WATERSHEDS)

Drainage Area (km²)	4.952
Shape Factor ()	7.236
Length of Main Channel (km)	5.986
Maximum Channel Elevation (m)	89.450
Minimum Channel Elevation (m)	77.640
Slope of Main Channel (m/km)	1.970
Slope of Main Channel (%)	0,197
Area Lakes/Wetlands (km²)	1.047
Area - Lakes (km²)	0.027
Area - Wetlands (km²)	1.020
Mean Elevation (m)	85.647
Ma×imum Elevation (m)	97.043
Mean Slope (%)	2.005
Annual Mean Temperature (°C)	6.800
Annual Precipitation (mm)	956,000

Watershed Name	On/Off	Delete
Watershed 1	12	x

Powered by Land Information Ontario



SOURCE: OWIT

8

9

WEST WATERSHED

Drainage Area (km²)	0.170
Shape Factor ()	4.308
Length of Main Channel (km)	0.856
Maximum Channel Elevation (m)	89.810
Minimum Channel Elevation (m)	78.410
Slope of Main Channel (m/km)	13.320
Slope of Main Channel (%)	1,332
Area Lakes/Wetlands (km²)	0.000
Area - Lakes (km²)	0.000
Area - Wetlands (km²)	0.000
Mean Elevation (m)	83.914
Maximum Elevation (m)	89.812
Mean Slope (%)	1.872
Annual Mean Temperature ("C)	6.900
Annual Precipitation (mm)	960.000



SOURCE: OWIT



AVERAGE SLOPE: (90.24– Tc= SEE EXCEL SPREADS RUNOFF COEFFICIENT: SEE RAINFALL INTENSITIES: SEE RUNOFF PEAKS: SEE EXCI	81.50)/554= 1.5 HEET E EXCEL SPREADS E EXCEL SPREADS EL SPREADSHEET	98% Sheet Sheet
D DRAWING TITLE:	SCALE:	DRAWING No.:
ASTER SUBDIVISION	1:5000	$\lambda \lambda / C1$
ERSHED PLAN	07-26-2024	

SURFACE EXTRACTED FROM LIDAR FILE ON GEOHUB WATERSHED AREA: A = 9.1795 HECTARE LONGEST PATH : L = 554 m

Time of Concentration:

I/ AIRPORT FORMULA

To be used when C < 0.40

 $t_c = \frac{3.26(1.1 - C)L^{0.5}}{(s^{0.33})}$

where:

t_c is the time of concentration (min) s is the average slope of the watershed (%)

L is the length of the watershed (m)

C is the runoff coefficient

To be used when C < 0.40

S=	1.58
C=	0.30
L=	554 m
t _c =	52.8 min

II/ BRANSBY-WILLIAMS FORMULA

To be used when C > 0.40

tc= 0.057 L/ (A^0.1 S^0.2) where:

t_c is the time of concentration (min)

s is the average slope of the watershed (%)

L is the length of the watershed (m)

A is the area of the watershed (ha)

S (%)= 1.58 A= 9.18 L= 544 m t_c = 22.7 min

WEST WATERCOURSE NEIGHBOURING LAND AREA = 9.17 ha Rational Method $Q_{5-25-100yr} = 2.78 \text{ C} I_{5-25-100yr} \text{ A}$

	5-YEAR	25-YEAR	100-YEAR
Tc (min) =	25	25	25
I ₅₋₂₅₋₁₀₀ (mm/hr) =	60.90	84.22	103.85
A (ha)=	9.1795	9.1795	9.1795
C=	0.250	0.313	0.313
Qp (L/s)	388.5	672.7	829.5

BOTH WATERSHEDS DRAINING INTO CULVERT

	A (ha)	Width (m)	Longest Path (m)
Watershed 1	476.37	1,200	4,480
Watershed 2	17.01	176	750
Watershed 1+2	493.38	1,200	4,480

DRAINAGE EASEMENT 5 Rear Yards Rational Method $Q_{5yr} = 2.78 \text{ C } I_{5yr} \text{ A}$ $Q_{100yr} = 2.78 \text{ C } I_{100yr} \text{ A}$

	5-YEAR	100-YEAR
Tc (min) =	10	10
I 5-100 (mm/hr) =	104.19	178.56
A (ha)=	0.1191	0.1191
C=	0.440	0.550
l (mm/hr) =	104.19	178.56
Qp (L/s)	15.18	32.52



WEST WATERCOURSE DRAIN - CULVERT



WEST WATER 200 M Step RAIN - OPEN CHANNEL



				and the		
Node ID:	D-1	N-1		N-2		OUTFALL
Bim (m):	82.28	82.67		83.00		
Invert (m):	81.50	81.39		80.74		80.08
e Cover (m):	0.18	0.52		1.50		
ax HGL (m):	81.94	81.88		81.23		80.50
Link ID:	DITCH	1-IN-4.5m	P.1		P-2	
ength (m):	29	1.80	65,50		65.90	
Dia ():	0	.60	0.76		0.76	
Slope (%):	0.6	3691	0.9924		1.0015	
Invert (m):	81	.50	81.39	100	80.74	
Invert (m):	81	:39	80.74		80.08	
Max Q (lps):	68	6.15	684.57		684.21	
xVel (m∕s):	0	.83	2,21	1	2.41	
x Depth (m):	0	.47	0.49		0.45	

Autodesk® Storm and Sanitary Analysis 2016 - Version 13.0.94 (Build 0) _____ * * * * * * * * * * * * * * * * * * * Project Description File Name 114-Neighb-Land-RM.SPF Description LOCKMASTER'S MEADOW SUBDIVISION * * * * * * * * * * * * * * * * Analysis Options **** Flow Units LPS Subbasin Hydrograph Method. EPA SWMM Infiltration Method Horton Link Routing Method Hydrodynamic Storage Node Exfiltration.. Constant flow Starting Date MAR-10-2024 00:00:00 Ending Date MAR-10-2024 12:00:00 Antecedent Dry Days 0.0 Report Time Step 00:10:00 Wet Time Step 00:05:00 Dry Time Step 01:00:00 Routing Time Step 5.00 sec * * * * * * * * * * * * * Element Count * * * * * * * * * * * * Number of rain gages 1 Number of subbasins 2 Number of nodes 4 Number of links 3 Number of pollutants 0 Number of land uses 0 * * * * * * * * * * * * * * * * Subbasin Summary * * * * * * * * * * * * * * * *
 Subbasin
 Total
 Equiv.
 Imperv.
 Average
 Raingage

 Area
 Width
 Area
 Slope

 ID
 hectares
 m
 %
 {DA-1}.37 0.12 55.22 34.00 1.0000 -Sub-01 9.18 578.51 0.00 1.5000 -* * * * * * * * * * * * Node Summary ********** NodeElementInvertMaximumPondedExternalIDTypeElevationElev.AreaInflow m ² m m _____ -----
 D-1
 JUNCTION
 81.50
 82.28
 50.00

 N-1
 JUNCTION
 81.39
 82.67
 100.00

 N-2
 JUNCTION
 80.74
 83.00
 15.00

 OUTFALL
 OUTFALL
 80.08
 80.84
 0.00
 N-2 OUTFALL ***** Link Summary * * * * * * * * * * * * * * * From Node To Node Link Element Length Slope Manning's

LOCKMASTER'S MEADOW SUBDIVISION

ID				Туре	I	n %	Roughness
DITCH-IN-4.5m P-1 P-2	D-1 N-1 N-2		N-1 N-2 OUTFALL	CHANNEL CONDUIT CONDUIT	29.8 65.9 65.9	8 0.3691 5 0.9924 9 1.0015	0.0200 0.0130 0.0130
* * * * * * * * * * * * *	* * * * * * *	*					
Cross Section	Summar	Y *					
Link	Shaj	pe	Depth/	Width	No. of	Cross	Full Flow
Design ID			Diameter		Barrels	Sectional	Hvdraulic
Flow						7.000	Dadiua
Capacity						Alea	Radius
LPS			m	m		m²	m
DITCH-IN-4.5m	TRA	PEZOIDAL	0.60	3.70	1	1.32	0.34
P-1	CIR	CULAR	0.76	0.76	1	0.46	0.19
P-2	CIR	CULAR	0.76	0.76	1	0.46	0.19
1162.36							
**************************************	*** ary ***						
Area:	T						
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.0003 .0103 .0347 .0734 .1264 .2043 .3183 .4661 .6370 .8299	0.0011 0.0140 0.0413 0.0828 0.1391 0.2242 0.3455 0.4985 0.6738 0.8711	0.0026 0.0183 0.0484 0.0929 0.1532 0.2455 0.3740 0.5318 0.7115 0.9132	0.0046 0.0232 0.0562 0.1035 0.1688 0.2684 0.4038 0.5660 0.7501 0.9562	0.0072 0.0287 0.0645 0.1146 0.1858 0.2926 0.4345 0.6011 0.7896 1.0000		
Hrad:		0.0460	0.05102	0.0001	2.0000		
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.0231 .1386 .2542 .3697 .4853 .5657 .6149 .7101 .8253 .9265	0.0462 0.1618 0.2773 0.3928 0.5071 0.5765 0.6241 0.7344 0.8465 0.9455	0.0693 0.1849 0.3004 0.4159 0.5253 0.5866 0.6335 0.7581 0.8672 0.9640	0.0924 0.2080 0.3235 0.4390 0.5406 0.5962 0.6590 0.7811 0.8874 0.9822	0.1155 0.2311 0.3466 0.4621 0.5539 0.6056 0.6849 0.8035 0.9072 1.0000		
width: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.0129 .0777 .1424 .2071 .2718 .4334 .5967 .7225 .8216 .9207	0.0259 0.0906 0.1553 0.2201 0.3027 0.4660 0.6294 0.7423 0.8414 0.9405	0.0388 0.1036 0.1683 0.2330 0.3353 0.4987 0.6621 0.7621 0.8612 0.9604	0.0518 0.1165 0.1812 0.2460 0.3680 0.5314 0.6828 0.7820 0.8811 0.9802	0.0647 0.1295 0.1942 0.2589 0.4007 0.5641 0.7027 0.8018 0.9009 1.0000		

LOCKMASTER'S MEADOW SUBDIVISION

Transect	XS-02				
Area:	0.0003 0.0103	0.0011 0.0140	0.0026	0.0046	0.0072
	0.0347 0.0734 0.1264	0.0413 0.0828 0.1391	0.0484 0.0929 0.1532	0.0362 0.1035 0.1688	0.0645
	0.2043 0.3183 0.4661	0.2242 0.3455 0.4985	0.2455 0.3740 0.5318	0.2684 0.4038 0.5660	0.2926 0.4345 0.6011
Hrad:	0.6370 0.8299	0.6738 0.8711	0.7115 0.9132	0.7501 0.9562	0.7896 1.0000
	0.0218 0.1306 0.2395 0.3484 0.4572 0.4675 0.5311	0.0435 0.1524 0.2613 0.3701 0.4529 0.4776 0.5468	0.0653 0.1742 0.2830 0.3919 0.4512 0.4892 0.5631	0.0871 0.1960 0.3048 0.4137 0.4537 0.5022 0.5897	0.1089 0.2177 0.3266 0.4355 0.4593 0.5162 0.6167
	0.6435 0.7743 0.9009	0.6701 0.7999 0.9258	0.6964 0.8253 0.9506	0.7225 0.8506 0.9754	0.7485 0.8758 1.0000
Width:	0.0129 0.0777 0.1424 0.2071 0.2718 0.4334 0.5967 0.7225 0.8216 0.9207	0.0259 0.0906 0.1553 0.2201 0.3027 0.4660 0.6294 0.7423 0.8414 0.9405	0.0388 0.1036 0.1683 0.2330 0.3353 0.4987 0.6621 0.7621 0.7621 0.8612 0.9604	0.0518 0.1165 0.1812 0.2460 0.3680 0.5314 0.6828 0.7820 0.8811 0.9802	0.0647 0.1295 0.1942 0.2589 0.4007 0.5641 0.7027 0.8018 0.9009 1.0000
Transect Area:	XS-04				
Hrad	0.0004 0.0144 0.0484 0.1024 0.1764 0.2704 0.3844 0.5184 0.6724 0.8464	0.0016 0.0196 0.1156 0.1936 0.2916 0.4096 0.5476 0.7056 0.8836	0.0036 0.0256 0.0676 0.2116 0.3136 0.4356 0.5776 0.7396 0.9216	0.0064 0.0324 0.0784 0.1444 0.3364 0.4624 0.6084 0.7744 0.9604	0.0100 0.0400 0.0900 0.1600 0.2500 0.3600 0.4900 0.6400 0.8100 1.0000
Width	0.0200 0.1200 0.2200 0.3200 0.4200 0.5200 0.6200 0.6200 0.7200 0.8200 0.9200	$\begin{array}{c} 0.0400\\ 0.1400\\ 0.2400\\ 0.3400\\ 0.4400\\ 0.5400\\ 0.6400\\ 0.7400\\ 0.8400\\ 0.9400 \end{array}$	0.0600 0.1600 0.2600 0.3600 0.4600 0.5600 0.6600 0.7600 0.8600 0.9600	0.0800 0.1800 0.2800 0.3800 0.4800 0.5800 0.6800 0.7800 0.8800 0.9800	0.1000 0.2000 0.3000 0.5000 0.6000 0.7000 0.8000 0.9000 1.0000
MTGCII:	0.0200 0.1200 0.2200 0.3200 0.4200 0.5200 0.6200	0.0400 0.1400 0.2400 0.3400 0.4400 0.5400 0.6400	0.0600 0.1600 0.2600 0.3600 0.4600 0.5600 0.6600	0.0800 0.1800 0.2800 0.3800 0.4800 0.5800 0.6800	0.1000 0.2000 0.3000 0.4000 0.5000 0.6000 0.7000

LOCKMASTER'S MEADOW SUBDIVISION

	0.7200 0.8200 0.9200	0.7400 0.8400 0.9400	0.7600 0.8600 0.9600	0.7800 0.8800 0.9800	0.8000 0.9000 1.0000
Transect XS	-05				
Area:	0.0004 0.0144 0.0484 0.1024 0.1764 0.2704 0.3844 0.5184 0.6724 0.8464	0.0016 0.0196 0.1576 0.1156 0.2916 0.4096 0.5476 0.7056 0.8836	0.0036 0.0256 0.1296 0.2116 0.3136 0.4356 0.5776 0.7396 0.9216	0.0064 0.0324 0.0784 0.1444 0.2304 0.3364 0.4624 0.6084 0.7744 0.9604	0.0100 0.0400 0.0900 0.1600 0.2500 0.3600 0.4900 0.6400 0.8100 1.0000
nrau:	0.0200 0.1200 0.2200 0.3200 0.4200 0.5200 0.6200 0.7200 0.8200 0.9200	0.0400 0.1400 0.2400 0.3400 0.4400 0.5400 0.6400 0.7400 0.8400 0.9400	0.0600 0.1600 0.2600 0.4600 0.5600 0.6600 0.7600 0.8600 0.9600	0.0800 0.1800 0.2800 0.3800 0.4800 0.5800 0.6800 0.7800 0.8800 0.8800 0.9800	0.1000 0.2000 0.3000 0.5000 0.5000 0.6000 0.7000 0.8000 0.9000 1.0000
Width:	0.0200 0.1200 0.2200 0.4200 0.5200 0.6200 0.7200 0.8200 0.9200	0.0400 0.1400 0.2400 0.3400 0.4400 0.5400 0.6400 0.7400 0.8400 0.9400	0.0600 0.1600 0.2600 0.4600 0.5600 0.6600 0.7600 0.8600 0.9600	0.0800 0.1800 0.2800 0.3800 0.4800 0.5800 0.6800 0.7800 0.8800 0.9800	0.1000 0.2000 0.3000 0.5000 0.6000 0.7000 0.8000 0.9000 1.0000
********** Runoff Quan ********* Total Preci Evaporation Infiltratio Surface Run Final Surfa Continuity	*********** tity Contin ********** pitation Loss of ce Storage Error (%) .	**** uity **** 	Volume hectare-m 0.707 0.000 0.510 0.199 0.000 -0.254	Depth mm 76.023 0.000 54.815 21.400 0.001	
*********** Flow Routin *********	*********** g Continuit ********	* * * * Y * * * *	Volume hectare-m	Volume Mliters	
Dry Weather Wet Weather Groundwater RDII Inflow External In External Ou Surface Flo Evaporation Initial Sto Final Store Continuity	Inflow Inflow flow tflow dding Loss red Volume Error (%) .	····· ····· ····· ·····	$\begin{array}{c} 0.000\\ 0.199\\ 0.000\\ 0.000\\ 0.000\\ 0.199\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ -0.002 \end{array}$	$\begin{array}{c} 0.000\\ 1.990\\ 0.000\\ 0.000\\ 1.990\\ 0.000\\ 1.990\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ \end{array}$	

T ()	= (0.94 ^ (L^0.0.0)	* (n^0.6)) / ((i^0.	4) * (S^0.3	3))			
Whe	re:	(,	, , ((-, (- , ,			
Tc L n i S	= Time of Concent = Flow Length (ft = Manning's Rough = Rainfall Intens = Slope (ft/ft)	ration (min) ness ity (in/hr	n)					
Subbasin {D	A-1}.37							
Flo Per Imp Per Slo Com	w length (m): vious Manning's R ervious Manning's vious Rainfall In ervious Rainfall pe (%): puted TOC (minute	oughness: Roughness tensity (mr Intensity s):	: m/hr): (mm/hr):	21.55 0.20000 0.01500 19.00583 19.00583 1.00000 18.33				
Subbasin Su	 b-01 							
Flo Per Imp Per Slo Com	w length (m): vious Manning's R ervious Manning's vious Rainfall In ervious Rainfall pe (%): puted TOC (minute	oughness: Roughness tensity (mr Intensity s):	: m/hr): (mm/hr):	$158.68 \\ 0.20000 \\ 0.01500 \\ 19.00583 \\ 19.00583 \\ 1.50000 \\ 60.43$				
********** Subbasin Ru	*********** noff Summary **********							
* * * * * * * * * * * *		Total		Total	Total	 Peak	Runoff	
**************************************	Total							
Subbasin ID	Total Rainfall	Runon	Evap.	Infil.	Runoff	Runoff	Coefficient	
************* Subbasin ime of ID oncentration h:mm:ss	Total Rainfall mm	Runon mm	Evap. mm	Infil. mm	Runoff mm	Runoff LPS	Coefficient	days
<pre>************************************</pre>	Total Rainfall mm 	Runon mm	Evap. mm 	Infil. mm 	Runoff mm 41.02	Runoff LPS 	Coefficient	days

LOCKMASTER'S MEADOW SUBDIVISION

Node ID	Average Depth Attained m	Maxii De Attai	mum Maxi pth ned Attai m	.mum T: HGL (.ned m da	ime o: Dccur: ays]	f Max rence hh:mm	s F] N	Total Looded Volume E ha-mm m	Total Time looded	Reten hh:m	tion Time m:ss
D-1 N-1 N-2 OUTFALL ***********************************	0.04 0.04 0.04 0.04 0.04	0 0 0 0	.44 81 .49 81 .49 81 .42 80	.94 .88 .23 .50	0 0 0	02:00 02:00 02:00 02:00)))	0 0 0 0	0 0 0 0	0:0 0:0 0:0 0:0	0:00
Node ID	Elem T	lent Ype	Maximum Lateral Inflow LPS	Peal Inflow LPS	v Pea 0 5 da	Tim ak In ccurr ys h	ne of nflow cence nh:mm	Maximum Flooding Overflow LPS	Time o Fl Occu days	of Peak Looding urrence hh:mm	
D-1 N-1 N-2 OUTFALL	JUN JUN JUN OUT	ICTION ICTION ICTION IFALL	687.28 0.00 0.00 0.00	687.28 686.15 684.5 684.21	 3 5 7 1)2:00)2:00)2:00)2:00	0.00 0.00 0.00 0.00			
Outfall Node ID) F Freque	'low ency (%) .02	Average Flow LPS 200.10	Peak Inflow LPS 684.21							
Outfall Node ID OUTFALL System) F Freque 23 23	'low ency (%) 3.02 8.02	Average Flow LPS 200.10 200.10	Peak Inflow LPS 684.21							
Outfall Node ID OUTFALL System ************************************) Freque Freque 23 23 23	'low . ncy (%) 3.02	Average Flow LPS 200.10 200.10	Peak Inflow LPS 684.21 684.21							
Outfall Node ID OUTFALL System ************************************) F Freque 23 23 23 23 23 23 23 23 23 23 23 23 23	low ency (%) .02 .02 .02	Average Flow LPS 200.10 200.10 Time Peak Fl Occurren days hh:	Peak Inflow LPS 684.21 684.21 0684.21	kimum bocity ained n/sec	Len Fac	ngth Stor	Peak Flo durir Analysi LF	ow Ig .s Ca 2S	Design Flow apacity LPS	Ratio Maxi /Des F
Outfall Node ID OUTFALL System ************************************) F Freque 23 23 23 *** try *** Ele tal Repo Typ me Condi	low ncy (%) .02 .02 .02 .02 ment orted we tion .NNEL .ed	Average Flow LPS 200.10 200.10 200.10 Time Peak Fl Occurren days hh: 0 02: 0 02:	Peak Inflow LPS 684.21 684.21 684.21 06 Ma: .ow Velo .cow Velo	kimum bocity ained n/sec 0.83 2.21	Len Fac	ngth tor	Peak Flc durin Analysi LE 686.1 684.5		Design Flow apacity LPS 1937.31	Ratic Maxi /Des F 0 0

Autodesk Storm and Sanitary Analysis

LOCKMASTER'S MEADOW SUBDIVISION

0.60 0 Calculated

Tink	 	Fractio Up Dru	on of Down	Time i Sub Crit	n Flow Sup	Class Up Crit	Down	Avg. Froude	Avg. Flow
K	y	Y	y						
DITCH-IN-4.5m P-1 P-2	0.13 0.13 0.14	0.49 0.00 0.00	0.00 0.00 0.00	0.38 0.68 0.63	0.00 0.18 0.23	0.00 0.00 0.00	0.00 0.00 0.00	0.11 0.31 0.38	0.0001 0.0001 0.0001

Analysis began on: Wed Aug 07 00:02:51 2024 Analysis ended on: Wed Aug 07 00:02:52 2024 Total elapsed time: 00:00:01

HY-8 Culvert Analysis Report

Crossing Name	Culvert Name	Total Dischar ge (cms)	Culvert Dischar ge (cms)	Headwa ter Elevatio n (m)	Inlet Control Depth (m)	Outlet Control Depth (m)	HW / D (m)	Normal Depth (m)	Critical Depth (m)	Outlet Depth (m)	Outlet Velocity (m/s)
EXIST 1900 CULVER T CTY RD	Culvert 1900mm dia.	12.00	11.08	82.07	3.49	1.863	0.56	1.15	1.67	1.26	5.99

Table 1 - Project Headwater Table

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow Minimum Flow: 5.00 cms Design Flow: 12.00 cms Maximum Flow: 12.00 cms

Headwater Elevation (m)	Total Discharge (cms)	Culvert 1900mm dia. Discharge (cms)	Roadway Discharge (cms)	Iterations
80.15	5.00	5.00	0.00	1
80.29	5.70	5.70	0.00	1
80.45	6.40	6.40	0.00	1
80.61	7.10	7.10	0.00	1
80.78	7.80	7.80	0.00	1
80.96	8.50	8.50	0.00	1
81.15	9.20	9.20	0.00	1
81.36	9.90	9.90	0.00	1
81.55	10.60	10.53	0.07	7
81.66	11.30	10.84	0.46	6
82.07	12.00	11.08	0.92	5
81.51	10.39	10.39	0.00	Overtopping

Table 2 - Summary of Culvert Flows at crossing: EXIST 1900 CULVERT CTY RD



Rating Curve Plot for crossing: EXIST 1900 CULVERT CTY RD

Total Dischar ge	Culvert Dischar ge	Headw ater Elevati	Inlet Control Depth	Outlet Control Depth	HW / D (m)	Flow Type	Normal Depth (m)	Critical Depth (m)	Outlet Depth (m)	Tailwat er Depth	Outlet Velocit v (m/s)	Tailwat er Velocit
(cms)	(cms)	on (m)	(m)	(m)						(m)	5 (7)	y (m/s)
5.00	5.00	80.15	1.57	0.631	0.25	1-S2n	0.69	1.09	0.74	0.59	4.90	2.82
5.70	5.70	80.29	1.71	0.722	0.28	1-S2n	0.74	1.17	0.80	0.65	5.04	2.94
6.40	6.40	80.45	1.87	0.819	0.30	1-S2n	0.79	1.24	0.86	0.70	5.17	3.05
7.10	7.10	80.61	2.03	0.922	0.33	5-S2n	0.84	1.31	0.91	0.75	5.29	3.15
7.80	7.80	80.78	2.20	1.032	0.35	5-S2n	0.89	1.37	0.96	0.80	5.40	3.24
8.50	8.50	80.96	2.38	1.149	0.38	5-S2n	0.93	1.43	1.02	0.85	5.51	3.33
9.20	9.20	81.15	2.57	1.275	0.41	5-S2n	0.98	1.49	1.07	0.90	5.61	3.41
9.90	9.90	81.36	2.78	1.409	0.45	5-S2n	1.02	1.54	1.12	0.95	5.71	3.48
10.60	10.53	81.55	2.97	1.541	0.48	5-S2n	1.06	1.58	1.16	1.00	5.80	3.55
11.30	10.84	81.66	3.08	1.631	0.49	5-S2n	1.08	1.60	1.18	1.04	5.84	3.62
12.00	11.08	82.07	3.49	1.863	0.56	5-S2n	1.15	1.67	1.26	1.09	5.99	3.68
14.18	11.69	81.96	3.38	1.952	0.54	5-S2n	1.13	1.65	1.24	1.23	5.95	3.85

Table 3 - Culvert Summary Table: Culvert 1900mm dia.

Culvert Barrel Data

Culvert Barrel Type: Straight Culvert Inlet Elevation(invert): 78.58 m Outlet Elevation (invert): 77.54 m Culvert Length: 17.53 m Culvert Slope: 0.06 m/m

Culvert Performance Curve Plot: Culvert 1900mm dia.





Water Surface Profile Plot for Culvert: Culvert 1900mm dia.

Site Data - Culvert 1900mm dia.

Site Data Option: Culvert Invert Data Inlet Station: 200.00 m Inlet Elevation: 78.58 m Outlet Station: 217.50 m Outlet Elevation: 77.54 m Number of Barrels: 1

Culvert Data Summary - Culvert 1900mm dia.

Barrel Shape: Circular Barrel Diameter: 1900.00 mm Barrel Material: Corrugated Steel Embedment: 0.00 mm Barrel Manning's n: 0.0240 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall (Ke=0.5) Inlet Depression: None

Tailwater Channel Data for Crossing: EXIST 1900 CULVERT CTY RD

Tailwater Channel Option: Rectangular Channel Bottom Width: 3.00 m Channel Slope: 0.01 m/m Channel Manning's n: 0.0200 Channel Invert Elevation: 78.40 m

Table 4 - Downstream Channel Rating Curve (crossing: EXIST 1900 CULVERT CTY RD)

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
5.00	78.99	0.59	2.82	57.90	1.17
5.70	79.05	0.65	2.94	63.30	1.17
6.40	79.10	0.70	3.05	68.52	1.17
7.10	79.15	0.75	3.15	73.61	1.16
7.80	79.20	0.80	3.24	78.58	1.16
8.50	79.25	0.85	3.33	83.44	1.15
9.20	79.30	0.90	3.41	88.22	1.15
9.90	79.35	0.95	3.48	92.92	1.14
10.60	79.40	1.00	3.55	97.56	1.14
11.30	79.44	1.04	3.62	102.12	1.13
12.00	79.49	1.09	3.68	106.64	1.13

Roadway Data for crossing: EXIST 1900 CULVERT CTY RD

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 5.00 m Crest Elevation: 81.51 m Roadway Surface: Paved Roadway Top Width: 18.00 m

HY-8 Culvert Analysis Report

Table 1 - Project Headwater Table

Crossing Name	Culvert Name	Total Dischar ge (cms)	Culvert Dischar ge (cms)	Headwa ter Elevatio n (m)	Inlet Control Depth (m)	Outlet Control Depth (m)	HW / D (m)	Normal Depth (m)	Critical Depth (m)	Outlet Depth (m)	Outlet Velocity (m/s)
114- WEST WATER COURSE	Culvert7 50 mm Conc.	0.95	0.95	82.46	0.96	0.0*	0.39	0.45	0.60	0.45	3.41

* Full Flow Headwater elevation is below inlet invert.

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow Minimum Flow: 0.75 cms Design Flow: 0.95 cms Maximum Flow: 1.00 cms

/	0			
Headwater Elevation (m)	Total Discharge (cms)	Culvert750 mm Conc. Discharge (cms)	Roadway Discharge (cms)	Iterati
82.30	0.75	0.75	0.00	1
82.32	0.77	0.77	0.00	1
82.34	0.80	0.80	0.00	1
82.36	0.83	0.83	0.00	1
82.38	0.85	0.85	0.00	1
82.40	0.87	0.87	0.00	1
82.42	0.90	0.90	0.00	1
82.44	0.92	0.92	0.00	1
82.46	0.95	0.95	0.00	1
82.49	0.98	0.98	0.00	1
82.51	1.00	1.00	0.00	1
83.50	1.77	1.77	0.00	Overto

Table 2 - Summary of Culvert Flows at crossing: 114-WEST WATERCOURSE



Rating Curve Plot for crossing: 114-WEST WATERCOURSE

Total Dischar ge (cms)	Culvert Dischar ge (cms)	Headw ater Elevati on (m)	Inlet Control Depth (m)	Outlet Control Depth (m)	HW / D (m)	Flow Type	Normal Depth (m)	Critical Depth (m)	Outlet Depth (m)	Tailwat er Depth (m)
0.75	0.75	82.30	0.80	0.0*	0.32	5-S2n	0.39	0.53	0.39	0.20
0.77	0.77	82.32	0.82	0.0*	0.33	5-S2n	0.40	0.54	0.40	0.21
0.80	0.80	82.34	0.84	0.0*	0.33	5-S2n	0.40	0.55	0.40	0.21
0.83	0.83	82.36	0.86	0.0*	0.34	5-S2n	0.41	0.56	0.41	0.22
0.85	0.85	82.38	0.88	0.0*	0.35	5-S2n	0.42	0.57	0.42	0.22
0.87	0.87	82.40	0.90	0.0*	0.36	5-S2n	0.43	0.58	0.43	0.22
0.90	0.90	82.42	0.92	0.0*	0.37	5-S2n	0.43	0.59	0.43	0.23
0.92	0.92	82.44	0.94	0.0*	0.38	5-S2n	0.44	0.59	0.44	0.23
0.95	0.95	82.46	0.96	0.0*	0.39	5-S2n	0.45	0.60	0.45	0.24
0.98	0.98	82.49	0.99	0.020	0.39	5-S2n	0.46	0.61	0.46	0.24
1.00	1.00	82.51	1.01	0.064	0.40	5-S2n	0.46	0.61	0.46	0.24
1.91	1.82	83.56	2.06	2.059	0.83	7-M2c	0.76	0.66	0.66	0.37

Table 3 - Culvert Summary	/ Table: Culvert750 mm Co	nc.
---------------------------	---------------------------	-----

* Full Flow Headwater elevation is below inlet invert.

Culvert Barrel Data

Culvert Barrel Type: Straight Culvert Inlet Elevation(invert): 81.50 m Outlet Elevation (invert): 80.10 m Culvert Length: 124.55 m Culvert Slope: 0.01 m/m

Culvert Performance Curve Plot: Culvert750 mm Conc.







Site Data - Culvert750 mm Conc.

Site Data Option: Culvert Invert Data Inlet Station: 0.00 m Inlet Elevation: 81.50 m Outlet Station: 124.54 m Outlet Elevation: 80.10 m Number of Barrels: 1

Culvert Data Summary - Culvert750 mm Conc.

Barrel Shape: Circular Barrel Diameter: 762.00 mm Barrel Material: Concrete Embedment: 0.00 mm Barrel Manning's n: 0.0110 Culvert Type: Straight Inlet Configuration: Grooved End in Headwall (Ke=0.2) Inlet Depression: None

Tailwater Channel Data for Crossing: 114-WEST WATERCOURSE

Tailwater Channel Option: Rectangular Channel Bottom Width: 4.00 m Channel Slope: 0.01 m/m Channel Manning's n: 0.0350 Channel Invert Elevation: 80.20 m

Table 4 - Downstream Channel Rating Curve (crossing: 114-WEST

WATERCOOKSE)								
Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number			
0.75	80.40	0.20	0.92	19.88	0.66			
0.77	80.41	0.21	0.94	20.29	0.66			
0.80	80.41	0.21	0.95	20.69	0.66			
0.83	80.42	0.22	0.96	21.09	0.66			
0.85	80.42	0.22	0.97	21.49	0.66			
0.87	80.42	0.22	0.98	21.88	0.66			
0.90	80.43	0.23	0.99	22.27	0.66			
0.92	80.43	0.23	1.00	22.66	0.66			
0.95	80.44	0.24	1.01	23.04	0.67			
0.98	80.44	0.24	1.02	23.42	0.67			
1.00	80.44	0.24	1.03	23.79	0.67			

Roadway Data for crossing: 114-WEST WATERCOURSE

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 4.00 m Crest Elevation: 83.50 m Roadway Surface: Gravel Roadway Top Width: 120.00 m

82.00 (EXISTING WATERCOURSE) € CHANNEL 81.00 ≈79.60 ___≈79.20 80.00 79.00 LONGITUDINAL -GRADIENT= 0.45%



DETENTION BASIN – SECTION

* DISTANCES ARE IN METRE SCALE: 1:100



LEGEND:	
EXISTING CULVERT	=======================================
PROPOSED DITCH AND CULVERT	
PROPOSED GRADING ELEVATION	→ 3 ² ,00 → 1 ⁴ ,82,00
EXIST. MAJOR OVERLAND	
PROPOSED SWALE	
SWALE INVERI	7 <u>82.00 INV</u>
CONTOUR	80.00
PROPOSED TERRACING	
PROPOSED SURFACE DRAINAGE PATTERN	<u> </u>
PROPOSED CURB	BARRIER MO
PROP. CHAINLINK FENCE —	
NOISE BARRIER	<u> </u>
	xx.xx
TREES	٠
HEDGES	
PROP. LANDSCAPED AREA ———	+ + + + + + + + + + + + + + + + + + + +







LEGEND:
PROPOSED SILT FENCE
PROPOSED SNOW FENCE
PROPOSED ROCK FLOW CHECK DAM
PROPOSED STRAW BALE BARRIER
PROPOSED STRAW BALE BARRIER
FILTER CLOTH FOR EXISTING STRUCT URE -
PROPOSED RIP RAP TREATMENT
EXISTING CULVERT
DITCH AND CULVERT 5000 CSP
PHASING LIMITS
PROPERTY BOUNDARY
EXIST. MAJOR OVERLAND
PROPOSED SWALE
PROPOSED SWALE INVERT
CONTOUR 80.00
CONTOUR
CONTOUR 80.00 PROPOSED TERRACING TTTT 11111





Page 271 of 465

UNITED COUNTIES OF LEEDS AND GRENVILLE PART OF LOT 7, CONCESSION 1 GEOGRAPHIC TOWN OF EDWARDSBURGH TOWNSHIP OF EDWARDSBURGH/CARDINAL COUNTY OF GRENVILLE

TOPOGRAPHIC INFORMATION TOPOGRAPHIC INFORMATION PROVIDED BY IBW SURVEYORS FILE No. A-026727-TOPO. SURVEY DATED APRIL 28, 2021.

ELEVATIONS SHOWN ON THIS PLAN ARE GEODETIC AND REFERRED TO THE CANADIAN GEODETIC VERTICAL DATUM (CGVD28) BY DIRECT MEASUREMENT TO REAL TIME NETWORK.

REFER TO GEOTECHNICAL SUBSURFACE INVESTIGATION REPORT No. 21C350, DATED MAY 31, 2021, PREPARED BY ST. LAWRENCE TESTING & INSPECTION CO. LTD.. INFORMATION PRESENTED IN THESE DRAWINGS HAS BEEN INTERPOLATED FROM THE GEOTECHNICAL REPORT AND ACCURACY IS NOT GUARANTEED. CONTRACTORS ARE ADVISED TO READ THE GEOTECHNICAL REPORT AND ASSUME THEIR OWN CONCLUSIONS.

USE AND INTERPRETATION OF DRAWINGS UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THIS DRAWING SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE

> 0 10 20

REFER TO DWG D-4 FOR MORE ESC DETAILS

POND BOTTOM ELEVATION CHANGE REVIEW COMMENTS - 10-18-2023 REVIEW COMMENTS - 06-30-2023 SWALE ALTERATION PEER REVIEW COMMENTS OWNER / APPROVAL REVISION / ISSUE Mongi Mabrouk P.Eng. Phone: 613-896-9170 Email: eng.services.ca@gmail.com ENGINEERING PROJECT NAME AND ADDRESS:

LOCKMASTER'S MEADOW SUBDIVISION

COUNTY ROAD No. 22 (SHANLY RD), CARDINAL, ON

Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive

EROSION & SEDIMENT CONTROL PLAN 1:750 0114 02/06/24







	Ontario	Project Name	e: Lockmaster's Mea	dow (County Rd. 22)	
City:	Cardinal	Project Numl	ber: -		
Nearest Rainfall Station	OTTAWA CDA RCS	Designer Nar	ne: Brandon O'Leary		
Climate Station Id:	6105978	Designer Con	npany: Forterra		
Years of Rainfall Data:	20	Designer Ema	ail: brandon.oleary@	forterrabp.com	
		Designer Pho	one: 905-630-0359		
Site Name:	Lockmaster's Meadow (Cou	nty Rd. 22) EOR Name:	22) EOR Name: Mongi Mabrouk		
Drainage Area (ha):	8.5	EOR Compan	iy: Mongi Mabrouk E	ngineering Services	
Runoff Coefficient 'c':	0.56	EOR Email: EOR Phone:	eng.services.ca@g	;mail.com	
Target TSS Removal (%): Required Water Quality Ru	80.0 noff Volume Capture (%): 90.0		(TSS) Load Sizing S	I Reduction Summary	
Oil / Fuel Spill Risk Site?		Yes	Stormceptor Model	TSS Removal Provided (%)	
Linstream Flow Control?		No	EFO4	40	
Opstream Flow Control?			EFO6	57	
Pack Commune (
Peak Conveyance (maximu	ım) Flow Rate (L/s):		EFO8	69	
Peak Conveyance (maximu	ım) Flow Rate (L/s):		EFO8 EFO10	69 76	



info@imbriumsystems.com





THIRD-PARTY TESTING AND VERIFICATION

► Stormceptor® EF and Stormceptor® EFO are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators and performance has been third-party verified in accordance with the ISO 14034 Environmental Technology Verification (ETV) protocol.

PERFORMANCE

► Stormceptor® EF and EFO remove stormwater pollutants through gravity separation and floatation, and feature a patentpending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including highintensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

PARTICLE SIZE DISTRIBUTION (PSD)

► The **Canadian ETV PSD** shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle	Percent Less	Particle Size	Percent
Size (µm)	Than	Fraction (µm)	reitent
1000	100	500-1000	5
500	95	250-500	5
250	90	150-250	15
150	75	100-150	15
100	60	75-100	10
75	50	50-75	5
50	45	20-50	10
20	35	8-20	15
8	20	5-8	10
5	10	2-5	5
2	5	<2	5



www.imbriumsystems.com

Page 2

Stormceptor[•]



Stormceptor EF Sizing Report

Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m ²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
0.5	8.6	8.6	6.62	397.0	38.0	100	8.6	8.6
1	20.3	29.0	13.23	794.0	76.0	100	20.3	29.0
2	16.2	45.2	26.47	1588.0	151.0	89	14.5	43.5
3	12.0	57.2	39.70	2382.0	227.0	82	9.9	53.3
4	8.4	65.6	52.93	3176.0	302.0	78	6.6	60.0
5	5.9	71.6	66.16	3970.0	378.0	75	4.5	64.4
6	4.6	76.2	79.40	4764.0	454.0	72	3.3	67.7
7	3.1	79.3	92.63	5558.0	529.0	68	2.1	69.8
8	2.7	82.0	105.86	6352.0	605.0	65	1.8	71.6
9	3.3	85.3	119.10	7146.0	681.0	64	2.1	73.7
10	2.3	87.6	132.33	7940.0	756.0	63	1.5	75.2
11	1.6	89.2	145.56	8734.0	832.0	63	1.0	76.2
12	1.3	90.5	158.79	9528.0	907.0	62	0.8	77.0
13	1.7	92.2	172.03	10322.0	983.0	62	1.1	78.1
14	1.2	93.5	185.26	11116.0	1059.0	60	0.7	78.8
15	1.2	94.6	198.49	11910.0	1134.0	59	0.7	79.5
16	0.7	95.3	211.72	12703.0	1210.0	57	0.4	79.9
17	0.7	96.1	224.96	13497.0	1285.0	55	0.4	80.3
18	0.4	96.5	238.19	14291.0	1361.0	53	0.2	80.5
19	0.4	96.9	251.42	15085.0	1437.0	51	0.2	80.7
20	0.2	97.1	264.66	15879.0	1512.0	48	0.1	80.8
21	0.5	97.5	277.89	16673.0	1588.0	46	0.2	81.0
22	0.2	97.8	291.12	17467.0	1664.0	44	0.1	81.1
23	1.0	98.8	304.35	18261.0	1739.0	42	0.4	81.5
24	0.3	99.1	317.59	19055.0	1815.0	40	0.1	81.7
25	0.0	99.1	330.82	19849.0	1890.0	39	0.0	81.7
30	0.9	100.0	396.98	23819.0	2268.0	32	0.3	82.0
35	0.0	100.0	463.15	27789.0	2647.0	28	0.0	82.0
40	0.0	100.0	529.31	31759.0	3025.0	24	0.0	82.0
45	0.0	100.0	595.48	35729.0	3403.0	22	0.0	82.0
Estimated Net Annual Sediment (TSS) Load Reduction =								

Climate Station ID: 6105978 Years of Rainfall Data: 20









RAINFALL DATA FROM OTTAWA CDA RCS RAINFALL STATION

INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL





info@imbriumsystems.com





Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inlet Pipe Diameter		Max Out Diam	et Pipe eter	Peak Conveyance Flow Rate	
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100
EF12 / EF012	3.6	12	90	1828	72	1828	72	2830	100

Maximum Pipe Diameter / Peak Conveyance

SCOUR PREVENTION AND ONLINE CONFIGURATION

Stormceptor® EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

DESIGN FLEXIBILITY

► Stormceptor[®] EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

► While Stormceptor[®] EF will capture and retain oil from dry weather spills and low intensity runoff, **Stormceptor[®] EFO** has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid reentrainment testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.







www.imbriumsystems.com

Page 5

Stormceptor[®]





Stormceptor EF Sizing Report

INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

Stormceptor EF / EFO	Mo Diam	del leter	Depth Pipe In Sump	(Outlet overt to Floor)	Oil Vo	olume	Recommended Sediment Maintenance Depth *		Maxi Sediment	mum Volume *	Maxin Sediment	num Mass **
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(#3)	(Kg)	(ID)
EF4 / EFO4	1.2	4	1.52	5.0	265	70	203	8	1190	42	1904	5250
EF6 / EFO6	1.8	6	1.93	6.3	610	160	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	1070	280	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	1670	440	610	24	17790	628	28464	78500
EF12 / EF012	3.6	12	3.89	12.8	2475	655	610	24	31220	1103	49952	137875

*Increased sump depth may be added to increase sediment storage capacity

** Average density of wet packed sediment in sump = $1.6 \text{ kg/L} (100 \text{ lb/ft}^3)$

Feature	Benefit	Feature Appeals To		
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer		
Third-party verified light liquid capture	Proven performance for fuel/oil hotspot	Regulator, Specifying & Design Engineer,		
and retention for EFO version	locations	Site Owner		
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer		
Minimal drop between inlet and outlet	Site installation ease	Contractor		
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner		

STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef

STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef





STANDARD PERFORMANCE SPECIFICATION FOR "OIL GRIT SEPARATOR" (OGS) STORMWATER QUALITY TREATMENT DEVICE

PART 1 - GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators**

1.3 SUBMITTALS

1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.

1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.

1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 – PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The minimum sediment & petroleum hydrocarbon storage capacity shall be as follows:

2.1.1 4 ft (1219 mm) Diameter OGS Units:
6 ft (1829 mm) Diameter OGS Units:
8 ft (2438 mm) Diameter OGS Units:
10 ft (3048 mm) Diameter OGS Units:
12 ft (3657 mm) Diameter OGS Units:

 $\begin{array}{l} 1.19 \ m^{3} \ sediment \ / \ 265 \ L \ oil \\ 3.48 \ m^{3} \ sediment \ / \ 609 \ L \ oil \\ 8.78 \ m^{3} \ sediment \ / \ 1,071 \ L \ oil \\ 17.78 \ m^{3} \ sediment \ / \ 1,673 \ L \ oil \\ 31.23 \ m^{3} \ sediment \ / \ 2,476 \ L \ oil \\ \end{array}$



info@imbriumsystems.com





PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m² to 1400 L/min/m², and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m² and 1400 L/min/m² shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 $L/min/m^2$ shall be assumed to be identical to the sediment removal efficiency at 40 $L/min/m^2$. No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 $L/min/m^2$.

3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m² shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m², and shall be calculated using a simple proportioning formula, with 1400 L/min/m² in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m².

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in



info@imbriumsystems.com





accordance with the Canadian ETV Program's Procedure for Laboratory Testing of Oil-Grit Separators.

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m².

3.4 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV **Program's Procedure for Laboratory Testing of Oil-Grit Separators**, with results reported within the Canadian ETV or ISO 14034 ETV verification. This reentrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to assess whether light liquids captured after a spill are effectively retained at high flow rates.

3.4.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m² to 2600 L/min/m²) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators.** However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.



SCHEDULE "I"

SERVICING PLAN AND PUMPING STATION

For the lands set out in Schedule "A", the Owner agrees to implement the objectives and criteria of the Site Servicing Report, prepared by Advance Engineering Ltd., stamped and dated February 6, 2024; and the General Plan of Services drawings (GSP-1, GSP-2), stamped and dated February 6, 2024;

For the lands set out in Schedule "A", the Owner agrees to implement the works shown in the Street Plan and Profiles (PP-1 to PP-6 inclusive), prepared by Advance Engineering Ltd., stamped and dated February 6, 2024;

For the lands set out in Schedule "A", the Owner agrees to implement the objectives and criteria of the report titled "Wastewater Pumping Station & Forcemain Design", prepared by Advance Engineering, stamped and dated April 15, 2024; and the drawings PS-1 to PS-4 inclusive, A-1, M-1, E-1 stamped and dated April 15, 2024 and November 22, 2023.

AUTO-STANDBY GENERATOR

The Pumping Station shall include an auto-standby generator, installed on Block "B", to the satisfaction of the Municipality.

Attached:

- Site Servicing Report February 6, 2024
- General Services Plan (GSP1, GSP2) February 6, 2024
- Plan and Profiles (PP1 to PP6 inclusive) February 6, 2024
- Wastewater Pumping Station and Forcemain Design April 15, 2024
- Pumping Station Plans
 - o Cover Sheet List of Drawings and Key Plan (CS1) April 15, 2024
 - Site Plan (PS1) April 15, 2024
 - Section and Details (PS2) April 15, 2024
 - Forcemain By-Pass Chamber (PS3) April 15, 2024
 - o Details (PS4) November 22, 2023
 - Plans (A1) November 22, 2023
 - Mechanical (M1) November 22, 2023
 - Electrical (E1) November 22, 2023



SITE SERVICING REPORT

PROJECT: LOCKMASTER'S MEADOW SUBDIVISION (95 Single Family Lots)

ADDRESS: COUNTY ROAD 22 (SHANLY ROAD) CARDINAL, ON

> PREPARED FOR: Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata, Ontario K2T 1C1 (613) 282 5601

PREPARED BY:

Advance Engineering Ltd. (613) 986 9170

Date	Revision / Issue
February 06, 2024	Update FUS 2020- Sanitary Design Sheet
August 03, 2022	Peer Review Comments
March 09, 2022	Issued for Subdivision Application

TABLE OF CONTENTS

1.0 INTRODUCTION	1
1.1 SITE DESCRIPTION	1
1.2 BACKGROUND AND LAND USE	1
1.3 PROPOSED DEVELOPMENT AND PHASING	2
1.4 EXISTING INFRASTRUCTURE	2
1.4.1 WATER	2
1.4.2 WASTEWATER	3
1.4.3 STORMWATER	3
2.0 WATER SERVICING	3
2.1 DESIGN CRITERIA	3
2.2 PROPOSED SERVICING AND CALCULATIONS	4
2.2.1 DOMESTIC WATER DEMAND	4
2.2.2 FIRE FLOW DEMAND	4
2.3 CONCLUSION	6
3.0 SANITARY SERVICING	6
3.1 DESIGN CRITERIA	6
3.2 PROPOSED SERVICING AND CALCULATIONS	6
3.3 CONCLUSION	7
4.0 STORMWATER AND STORMWATER MANAGEMENT	7
5.0 CONCLUSION AND RECOMMENDATIONS	8
List of Appendices:	

A - Location – Figures

B - Draft Plan Agreement Conditions

- Geotechnical Report (2021)
- C Water & Sewer Design Calculations

List of Related Drawings:

S-1 – Draft Plan of Subdivision	ES-1 - Erosion and sediment Control Plan
GSP - General Services Plan	D1 TO D6 – Details
PP-1 TO PP-5 - Plan & Profile - Streets A, B & C	
GR-1&2 - Grading and Drainage Plan	

List of Related Reports:

- Stormwater Management Report & Pumping Station and Forcemain Design Report



1.0 INTRODUCTION

Edwardsburgh Developments Ltd. has retained *Advance Engineering Ltd.* to provide a site servicing study for the proposed residential subdivision of 95 single family lots. The report describes the existing infrastructure in the immediate area and estimates the servicing requirements for the proposed development. The adequacy of the existing sanitary sewer, watermain and stormwater infrastructure to accommodate all required flows and demands associated with the proposed development will be examined. The report also provides information and assumptions used in the design of the sanitary sewer and watermain, and should be read in conjunction with the design drawings prepared by *Advance Engineering Ltd.*.The report is prepared in support of an application for a subdivision draft plan approval by the applicant.

1.1 SITE DESCRIPTION

The proposed development is on a single parcel of land. It is located off the west side of County Road No. 22, village of Cardinal, Township of Edwardsburgh / Cardinal, Ontario (Figure-1, **Appendix A**). The legal description of the property is: "*Part of Lot 7, Concession 1, Geographic Township of Edwardsburgh, Township of Edwardsburgh / Cardinal, County of Grenville*". The subject property is bounded as follows:

- County Road 22 (Shanley Road) and three residential dwelling units to the east,
- CN railway to the north,
- vacant agriculture land to the west, and,
- residential dwellings to the south.

The subject property area is approximately 10.9274 hectares (27 acres) with a rectangular shape of approximately 600 m in length and 180 m in width. The site is currently vacant, undeveloped and covered with short grass and pasture.

1.2 BACKGROUND AND LAND USE

The original draft plan of the proposed subdivision was approved on April 24, 2013 (*File No. 07-T-10005*). In 2021, changes have been applied to the draft plan. A copy of the updated 2021 agreement conditions is attached in **Appendix B**.

The site has never been developed and has always been a green field. The current zoning of the subject property is "Residential First Density R1" that allows single family dwellings of lot areas not less than 465 m² and lot frontages not less than 15 m for fully serviced lots.

The site has been surveyed by *Ron M. Jason Surveying Ltd.*. A topographic survey dated April 28, 2021, has been provided by *IBM surveyors*.

A copy of the report outlining the results of the geotechnical subsurface investigation carried out by *St. Lawrence Testing & Inspection Co. Ltd.* is attached in **Appendix B**.

The Township has provided the following documents pertaining to existing water and sewer infrastructure:

- Uncommitted Reserve Capacity Study by *Stantec* – Dated November, 2022.

- Cardinal drinking water treatment plant flow summary (period: 2018-2021), Cardinal wastewater treatment plant flow summary (2018-2021) and Adelaide St pump station flow data (2018-2021).

- WWTP CofA (includes Adelaide St pump station capacity, dimensions etc.).

- Municipal drinking water system licences 3 and 4 for Cardinal.

The Township had previously approved available wastewater and drinking water capacities for "Edwardsburgh development" that represented 93 lots among a total of 221 of committed lots.

1.3 PROPOSED DEVELOPMENT AND PHASING

The proposed development, as shown in the updated Plan of Subdivision, consists of the construction of paved roadways, curbs and gutters, sanitary and storm sewers, watermains and other utilities (gas, Bell and Hydro) to service the proposed 95 detached lots. All proposed right-of-ways (ROW) are 20 m wide. The subdivision layout has two intersections with County Road No. 22 to the east. Two reserved ROWs for future street extensions are located at the south and north-west of the property. A 6 m wide pathway is planned between Street B and County Rd 22. It will also serve as a watermain easement. The site will be serviced via County Road existing infrastructure. Due to the insufficient elevations for a design of a gravity sewer, a pumping station is proposed downhill of the property (in Block B), and a pressurized forcemain will be used to discharge sewage from the pumping station into the existing sewer within County Rd 22. The sanitary sewer within the site is designed to operate under free flow condition for phase 1 and phase 2.

Storm water is conveyed to a proposed stormwater management detention basin to the north of the property (Block A) before it is discharged into the existing unnamed watercourse that crosses the property. The stormwater facility is designed to achieve mainly the required quantity control.

A noise berm will be constructed in the open space between the subdivision and CN railway.

The two phases of the project are:

• Phase 1: comprises of 59 lots and a dedicated parkland located at the south side of the property.

• Phase 2: consists of developing the remaining 36 lots in the north side of the subdivision.

The total gross area for phase 1 is 4.74 ha and for phase 2 is 2.96 ha. The open space area where the stormwater facility will be constructed is 3.23 ha.

1.4 EXISTING INFRASTRUCTURE

1.4.1 WATER

Existing municipal watermain:

There is an existing 250 mm diameter watermain identified along County Road 22 east side up to Dodge St. At the intersections with Gill St and Dodge St, the approximate elevations of the top of watermain are 83.00 m and 81.60 m respectively. For phase 1, the proposed watermain will be connected to the existing watermain via the proposed Street A and the pathway.

Available Capacities:

Based on a copy of a 2021 Municipal Drinking Water Licence provided by the Township, the treatment plant, located at Legion Way, Cardinal, has a rated capacity of 3548 m³/day. According to 2002 *Stantec* study, the uncommitted reserve capacity of Cardinal's water treatment plant is 701 m³/day, which is the equivalent of an additional population of 800 or 364 units.

The Township has informed us that there are currently 221 committed lots including 93 lots for Edwardsburgh development and 106 lots for Meadowlands North, located to the north of Dodge St. There are also 22 committed vacant lots. Edwardsburgh development is now 95 lots. The additional 2 lots are not expected to impact the available capacity.

An extension of 250 mm diameter watermain is to be extended north along County Rd to serve the future Meadowlands developments and the planned industrial area. Future developments nature is unknown at the time of preparation of this report, therefore their expected demands are not examined. The village water tower is located at 4035 Dishaw St and has a capacity of 1938 m³.

1.4.2 WASTEWATER

Existing municipal sewer: There is a manhole (MH-135) located at the intersection of County Rd 22 and Gill St. From MH-135, a 250 mm dia. PVC DR 35 pipe runs south along County Road 22, and a 250 mm dia. pipe, sloped at 0.94 %, runs east along Gill St. The south and east invert elevations at MH-135 are 82.72 m and 82.11 m respectively. The capacity of Gill St sewer is estimated at 58 L/s using Manning's Formula (Refer to calculations in **Appendix-C**). There is a second manhole (MH-140) at the intersection of County Rd 22 and Dodge St into which are connected two pipes: a 200 mm dia. pipe coming from Dodge St and a 250 mm dia. pipe sloped at 0.28% running south to MH-135. The south invert elevation is 82.42 m and the full capacity of the sewer is estimated at 31 L/s. Also, two 200 mm dia. capped pipes are connected to MH-140; one is directed north along the road and the other west adjacent to the site. The proposed force-main will be connected to the capped pipe at this intersection.

Available Capacities:

The subdivision generated wastewater will be conveyed to Adelaide St pumping station via County Rd, Gill St, and Walker St. According to 2002 *Stantec* study, Adelaide St PS has a reserve capacity of 35 L/s, the equivalent of more than a population of a 1000 persons or 454 dwelling units. The uncommitted reserve capacity of the wastewater treatment plant at John St is 701 m³/day, which is the equivalent of an additional population of 800 or 364 units.

The village has a committed capacity for 201 lots, including 93 lots for Edwardsburgh development and 106 lots for Meadowlands North located to the north of Dodge St. There are also 22 committed vacant lots.

1.4.3 STORMWATER

The site is located in the sub-watershed of *Sawmill Creek*. There is no storm water sewer in the immediate area of the subdivision. Storm water will be captured and conveyed to a detention pond in the open space at the north side of the site. Excess flow will be discharged into existing watercourse running from north to east.

Hydro, Bell telecommunications and gas main were identified at County Rd 22. Utility service connections to the developed site will be coordinated with the appropriate utility companies prior to construction.

2.0 WATER SERVICING

2.1 DESIGN CRITERIA

The water demand for the proposed development was calculated based on *Ottawa Design Guidelines* - *Water Distribution* and subsequent technical bulletins as follows:

- > Population: 323 person (residential occupancy for single family dwelling = 3.4 person per unit)
- Average daily demand per capita per day = 350 L/pers./day
- Peaking factor for maximum daily demand = 3.6

Peaking factor for peak hourly demand = 5.4

Peak factors are calculated by interpolating the values in Table 3-3 of the MOECP "*Design Guidelines for Drinking-Water Systems*", for water systems serving fewer than 500 persons.

- Required Fire Flow (RFF) demand: calculated as per the Ontario Building Code (OBC), A-3.2.5.7 Division B, Building Code Compendium, and cross-referenced with the 2020 version of the Fire Underwriter's Survey (FUS).
- > System pressures requirements:

Brossura Chack	Minim	num Pressure	Maximum Pressure		
Flessule Check	(kPa)	(psi)	(kPa)	(psi)	
Normal Use		50	552	80	
Peak Hour Demand		40	552	80	
Maximum Day and Fire Flow		20	552	80	
Maximum pressure at any point in occupied areas	552	80			
Maximum pressure at any point in unoccupied areas	689	100			

Table -1 System Pressure Requirements

Proposed Watermain:

150 mm diameter PVC Class 150 DR 18 – Roughness Coefficient C = 100

200 mm diameter PVC Class 150 DR 18 – Roughness Coefficient C = 110

2.2 PROPOSED SERVICING AND CALCULATIONS

2.2.1 DOMESTIC WATER DEMAND

Domestic water demands are summarized as follows (Refer to **Appendix C** for full calculations):

	Phase 1	Phase 2	Total
Population Density: 3.4 pers. per unit	3.4	3.4	3.4
Number of homes	59	36	95
Population in capita	200.6	122.4	323.0
Average Demand Volume Per Capita in L/c/day	350	350	350
Total Average Demand Volume in m3/day	70.2	42.8	113.1
Maximum Daily Demand (3.6 x Average) in m3/day*	252.8	154.2	407.0
Maximum Hourly Demand (5.4 x Average Daily) in m3/day*	379.1	231.3	610.5
Maximum Hourly Water Flow Required in L/s	4.39	2.68	7.07

Table -2 Anticipated Domestic Water Demand

2.2.2 FIRE FLOW DEMAND

1- Ontario Building Code (OBC), A-3.2.5.7 Division B, Building Code Compendium:

Minimum water supply required in Litres: Q= K.V.S_{tot} where:

Q: minimum water supply in litres


K: water supply coefficient from Table 1

V: total building volume in cubic metres

S tot: total of spatial coefficient values from property line exposures on all sides as obtained

from the formula: $S_{tot} = 1 + (S_{side1} + S_{side2} + S_{side3} + ... etc.);$ S_{tot} need not exceed 2.0.

A minimum of water supply flow rate for firefighting shall be 2 700 L/min.

2- Required Basic Fire Flow (FUS 2020 – PART II. 1): F = 220 C A^{0.5} where

F: required fire flow in litres per minute

C: coefficient related to the type of construction

A: the total floor area in m²

Adjustments to the calculated fire flow may be made based on occupancy, sprinkler protection and exposure to other structures. The final fire flow shall not exceed 45,000 L/min nor be less than 2,000 L/min.

The specific details of future buildings were not available at the time of preparation for this report, therefore, an estimate for the building materials, fire separations, and contents have been assumed based on experience for typical single home subdivision developments. Combustible wood frame construction with limited combustible occupancy and no sprinkler have been assumed in our calculation. An average lot size with a maximum of 30% lot coverage, as permitted by current zoning By-law, has been considered. Expositions were calculated based on permitted setbacks. Refer to spreadsheets in **Appendix C** for full calculations using both methods.

FUS 2020 calculation method has resulted in fire flow demand of 7,000 L/min (117 L/s).

Proposed Fire Hydrants:

The maximum spacing between the proposed fire hydrants is 125 m as per Table 4.9 of Ottawa Guidelines. All new hydrants are assumed to be Class AA with rated capacity of 5,700 L/min. The critical area for the RFF supply is north zone where elevations are around 85.00. A plan showing 45 m radius circles centered on each hydrants is attached in **Appendix B**.

EPANET Hydraulic Analysis:

Using anticipated domestic water demand and RFF, the software runs simulations to assess headlosses and velocities within the proposed watermain. New fire hydrants have been checked according to Appendix I: "Guidelines on Coordination of Hydrant Placement with Required Fire Flow" of Technical Bulletin ISTB-2018-02, in which the aggregate fire flow capacity of all fire hydrants within 150 m of a building shall not be less than the required fire flow (7,000 L/min). This is done by assigning a 5,700 L/min flow to all hydrants located within 75 m from the test property and a 3,800 L/min flow to all hydrants located within 75 m but less than 150 m. Refer to Appendix B for critical lots and blocks results. For example, Lot 1 has 2 hydrants within 75 m and 2 hydrants within 150 m. Lot 58 has 1 hydrants within 75 m and 3 hydrants within 150 m.

EPANET models under maximum day and RFF demand condition and assuming a pressure of 350 kPa at County Rd watermain are exhibited in (**Appendix C**). The results of the hydraulic simulation remain comparable to the existing watermain in the area. Residual pressure is kept above 140 kPa and velocities less than 5 m/s.

We recommend hydrant flow tests for two hydrants within County Rd. Also, a pressure check shall be conducted at the completion of phase 2 in order to determine if pressure control is required for lots located at low elevations.



2.3 CONCLUSION

	Phase 1	Phase 2	Total
Maximum Day Demand in L/s	2.9	1.8	4.7
Peak Hour Demand in L/s	4.4	2.7	7.1
Fire Flow Demand in L/s **	117.0	117.0	117.0
Maximum Day Demand plus Fire Flow Demand in L/s	119.9	118.8	121.7

The anticipated water demand is summarized as follows:

Table -3 Summary of Anticipated Water Demand

It is proposed to provide water supply within the subdivision through a new 150 and 200 mm diameter PVC Class 150 DR 18 in the shape of two loops. The proposed watermain will be connected to the existing 250 mm diameter watermain at County Rd 22 at two locations as shown in the General Services Plan. Water supply for fire fighting will be delivered to the fire hydrants through the municipal system.

Under normal use, pressure shall be kept between 345 kPa (50 psi)and 552 kPa (80 psi). For peak hour demand pressure shall be greater than 276 kPa (40 psi) and lower than 552 kPa (80 psi). Residual pressure for fire flow and maximum day demand shall be kept greater than 140 kPa (20 psi).

An isolation valve will be installed at the intersection of County Rd and the pathway.

3.0 SANITARY SERVICING

3.1 DESIGN CRITERIA

Using the *Ottawa Sewer Design Guidelines,* sanitary sewage flow for the proposed development is estimated as follows:

- Population: Residential occupancy for single family housing = 3.4 persons per unit (Ottawa Guidelines, Table 4.2) 95 units x 3.4 pers. /unit = 323 persons (Phases 1 & 2)
- > Peak Flow Design Calculation:
 - Average daily flow per capita = 350 L/pers./day
 - Average daily flow Dry weather = 323 pers. x 350 L/pers./day = 1.69 L/s
 - Harmon's Residential Peaking Factor = 1 + (14 / (4 + (P / 1000)^{0.5})) (Max.= 4; Min.= 2)
 - Wet weather infiltration contribution (Extraneous): 0.28 L/s/effective gross ha
 - Dry weather infiltration contribution (Extraneous): 0.05 L/s/effective gross ha

Gross residential area includes lots, roadways and pumping station. Block A (open space, park and pond) is not included.

3.2 PROPOSED SERVICING AND CALCULATIONS

The total peak design flow rate is the sum of the peak dry weather flow rate as generated by population and land use for the design contributing area plus all extraneous flow allowances. Detailed calculations for sanitary flows are exhibited in **Appendix C**. Results are summarized in the following table 4:



Design Parameter	Flow (m³/day)	Flow (L/s)
Average Dry Weather Flow Rate	146.2	1.69
Peak Dry Weather Flow Rate	423.2	4.90
Peak Wet Weather Flow Rate	608.6	7.04

Table -4 Summary of Sanitary Flows

The total peak sanitary flow rate from the proposed development represents 22.4 % of the capacity of the existing 250 mm diameter sewer (31.5 L/s) running north to south along County Road.

3.3 CONCLUSION

1200 mm manholes and 200 mm diameter PVC DR 35 sanitary sewer with a minimum pipe slope of 0.32% are proposed within the subdivision. Refer to **Appendix C** for the sanitary sewer design sheet. The gravity sewer will outlet into the pumping station (Block B). A proposed 150 mm diameter forcemain will discharge into the existing municipal sanitary sewer at County Rd 22 as shown in General Plan of Services.

The maximum distance between manholes is 120 m. The hydraulic grade line is at least 0.3 m below footings.

All sanitary laterals shall be 135 mm diameter DR 28 PVC pipes with minimum 1% slopes. Backwater valves shall be installed on all sanitary and storm laterals.

The sanitary design is also able to accommodate the servicing of second dwelling units in all lots.

Sewage discharges will be domestic in type and in compliance with the *City of Ottawa Sewer Use Bylaw* and *Ontario Building Code (OBC)*.

4.0 STORMWATER AND STORMWATER MANAGEMENT

The quantity control target is to limit the maximum post-development runoff rate discharged from the site for all storm events, up to and including the 100-year design storm, to that of the 5-year pre-development flow rate for a 5-year design storm event. Runoff in excess of the 5-year pre-development flow rate will be temporarily stored on site in a detention basin and discharged gradually into the existing watercourse that outlets into *Sawmill Creek*. The pond is designed to function for both phases.

The quality control consists of an enhanced level of treatment (80% of TSS removal) by on-site measures to protect receiving waters.

Refer to the "Stormwater Management Report" for detailed analysis and calculations of quantity, quality and storage requirements.

5.0 CONCLUSION AND RECOMMENDATIONS

The preceding report has been prepared to support the development of a subdivision composed of 95 single family lots. The conclusions are as follows:

• Based on estimated water demand, and upon confirmation by the Village of Cardinal of acceptable boundary conditions, the existing 250 mm diameter watermain within County Road 22 has sufficient water supply capacity to support the proposed development.

• The watermain system is able to maintain a minimum pressure of 140 kPa at ground level at all points in the distribution system under maximum day demand plus fire flow conditions. The Village fire department must review the fire flow requirement design.

• The proposed watermain within the subdivision will be of 150 mm and 200 mm diameter PVC DR 18. Water services shall be 25 mm diameter Type K soft copper or Cross-linked Polyethylene.

• The proposed extension of 250 mm diameter watermain north along County Rd 22 will be used to connect the future development of Meadowlands North.

◆ The proposed sanitary sewer will be a 200 mm diameter DR 35 and 1200 mm diameter manholes as per OPSD 701.010. The sewage will be conveyed gravitationally to the pumping station from which it will be pumped through a proposed 150 mm diameter forcemain into the existing sewer within County Rd 22. The existing sanitary sewer has adequate capacity to convey the estimated wastewater generated from the development.

• Stormwater will be conveyed via a proposed separate storm sewer within the right-of-ways to a proposed on-site stormwater management structure where quality and quantity control will be achieved. Discharge flow rates will match the pre-development levels.

• Service connections shall comply with the OPSD standards.

♦ Hydro, gas main and telecommunication lines have been identified at the intersection of County Rd 22 and Gill St. Connections to the development will be coordinated with authorities having jurisdictions prior to construction.

Respectfully submitted,

Mongi Mabrouk M.Eng., P.Eng.

Advance Engineering Ltd.

Phone: 613-986-9170





APPENDICES

Appendix A

- Figure 1: Site Location
- Zoning By-law Schedule

Appendix **B**

- Draft Plan Agreement

Appendix C

- Domestic Water Supply Calculations
- Fire Flow Calculations
- Sanitary Sewer Calculations

APPENDIX - A





APPENDIX - B



Applicant:Edwardsburgh Developments Inc.File:07-T-10005 (Lockmaster's Meadow)Municipality:Township of Edwardsburgh CardinalLocation:Lot 7, Con. 1, County Road 22

Date of Original Decision: April 24, 2013 Date of Revised Decision: February 24, 2022 Date of Notice: February 25, 2022 Last Date of Appeal: March 17, 2022 Lapsing Date: February 25, 2025

Conditions of Draft Approval

- 1. That this approval applies to the Draft Plan of Subdivision in Lot 7, Concession 1, Township of Edwardsburgh Cardinal, County of Grenville, prepared by Advance Engineering dated December 7, 2021 which shows a total of 95 residential lots, Block A for open space, a safety fence, a stormwater retention pond, noise attenuation barrier and safety barrier, Block B for a sanitary pumping station, Blocks C, D, and Da for 0.3 m reserves, Block E for future road purposes, Block F for parkland, Block G for future road purposes and Block H for a walkway and utility corridor.
- 2. That a minimum of 10 metres from both sides of the centre line of the Streets shown on the draft plan shall be shown and dedicated as public highways on the final plan.
- 3. That Block E and Block G, as shown on the draft plan, shall be conveyed to and held in trust, by the Township of Edwardsburgh Cardinal until the extension of the road allowance.
- 4. That Block A, as shown on the draft plan, shall be conveyed to the Township of Edwardsburgh Cardinal subject to the terms and conditions of the Township.
- 5. That the streets shall be named to the satisfaction of the Township.
- 6. The subdivision shall be built in two phases. Phase 1 consists of Block A including the safety fence, stormwater management pond, noise barrier and safety barrier, Street A, Street B south-east of Street A, a total of fifty-nine (59) residential lots, being lots 9-37, 57-61 and 71-95, including Blocks C, D and Da as 0.3 m reserves, Block E as a future roadway block, Block F as parkland dedication, and Block H as a walkway and utility corridor, as shown on the draft plan. Phase 2 consists of Street C, the remainder of Street B, the remaining thirty-six (36) units, being lots 1-8, 38-56 and 62-70, Block B for a sanitary pumping station and Block G as a future roadway connection.
- 7. That the Owner enter into a subdivision agreement between the Owner and the Township to the satisfaction of the Township and that the Owner covenants and agrees that the executed subdivision agreement between the Owner and the Municipality shall be registered against the lands to which it applies once the plan of subdivision has been registered. It is noted that the subdivision agreement



will be prepared when the final design plans (i.e. servicing, stormwater management, road design, berm design, etc.) have been reviewed and accepted and/or are in the final stages of review and acceptance by the Township.

<u>Parkland</u>

- 8. That Block F, as shown on the draft plan, shall be conveyed to the Township of Edwardsburgh Cardinal as part of Parkland Dedication subject to the terms and conditions of the Township.
- 9. That the developer, as part of Parkland Dedication, convey a cash-in-lieu payment to the Township.
- 10. All Owner obligations associated with Block F must be completed in Phase 1 to the satisfaction of the Township of Edwardsburgh Cardinal.
- 11. It is the responsibility of the Owner to fill with clean earth fill, compact and level Block F accordingly, providing for positive surface drainage to the satisfaction of the Township of Edwardsburgh Cardinal.
- 12. The Owner shall grade areas of parkland where necessary to the satisfaction of the Township of Edwardsburgh Cardinal, so as to provide a uniform surface, free of debris, necessary to establish a safe clean and maintainable surface. Block F shall be graded in accordance with the approved Grading Plan for the Plan of Subdivision. No storage of building materials, including granular or topsoil will be permitted on Block F.

<u>Zoning</u>

13. That prior to final approval by the Counties, the Counties is to be advised by the Township of Edwardsburgh Cardinal that this proposed subdivision conforms to the zoning by-law in effect and that any zoning issues identified are appropriately satisfied through an amendment to the Township Zoning By-Law. It is noted that the Township is currently preparing a new Zoning By-Law. To clear this condition, a plan noting lot area and lot frontage for each proposed lot will be required based on the definitions of the Zoning By-law in effect at the time of final approval.

Servicing - General

- 14. That the Owner agrees in writing to satisfy all the requirements, financial and otherwise, of the Township of Edwardsburgh Cardinal concerning the provision of roads, installation of services, drainage and other relevant features (such as lighting, etc.).
- 15. That such easements as may be required for utility or drainage purposes shall be granted to the appropriate authority.



- 16. The Owner acknowledges their responsibility to obtain all of the required approvals for the pumping station to be constructed on Block B.
- 17. Notwithstanding what may be illustrated on the approved draft plan, that the final subdivision agreement plans show and subdivision agreement contain a clause whereby the Owner agrees to provide two lifts of asphalt, concrete curbs and gutters, in accordance with OPSS, on Streets A, B and C to the satisfaction of the Township of Edwardsburgh Cardinal.
- 18. That the plans show and subdivision agreement contain a clause whereby the Owner agrees to provide underground electrical servicing to the satisfaction of the Township of Edwardsburgh Cardinal.
- 19. That the subdivision agreement include terms satisfactory to the Township indicating Block H, as shown on the draft plan, shall be conveyed to the Township upon Township acceptance of the underground services, walkway, landscaping and fencing.

Water and Sewer Works

- 20. The Owner shall submit detailed municipal servicing plans, prepared by a Civil Engineer licensed in the Province of Ontario, to the Township of Edwardsburgh Cardinal and the United Counties of Leeds and Grenville (Counties'). All water and sewer works to be located on the County Road right-of-way shall be subject to approval from the Counties' Roads Department at the time of detailed design.
- 21. The Owner acknowledges and agrees that building permits will not be issued for the development of individual Lots in Phase 2 until the pumping station has been installed and placed in service to the satisfaction of the Township of Edwardsburgh Cardinal.
- 22. The Owner shall design and construct all necessary watermains and the details of services and meters to the satisfaction of the Township of Edwardsburgh Cardinal. The Owner acknowledges that the servicing plan shall include a watermain stub to Block E and Block G. The Owner shall pay all related costs, including the cost of connection, inspection and sterilization by Township personnel, as well as the supply and installation of water meters by the Township.
- 23. Upon completion of the installation of all watermains, hydrants and water services, the Owner shall provide the Township with mylar(s) of the "as-built" plan(s), certified under seal by a Professional Engineer, showing the location of the watermains, hydrants and services. Electronic files are also required in order for them to be added to the Township GIS system. The United Counties require digital files in .dwg and pdf format.



Stormwater Management

- 24. That prior to final plan approval, the Owner shall prepare a final stormwater site management plan and lot grade and drainage plan which shall be consistent with the report entitled "Preliminary Stormwater Management Report" prepared by Eastern Engineering Group Inc. signed July 13, 2010. The final stormwater site management plan shall address the South Nation Conservation review comments dated October 12, 2010. The Plan shall describe how stormwater management is to be implemented in accordance with the current Stormwater Management Best Management Practices and should address both water quality and quantity concerns. Models, assumptions and calculations of pre-and post-development runoff are to be included in this submission. The final report shall be prepared to the satisfaction of the Township of Edwardsburgh Cardinal, South Nation Conservation and the United Counties of Leeds and Grenville. Consideration shall be had to condition 41.
- 25. Post-development stormwater flows at the County Road culvert shall equal pre-development flows.
- 26. That prior to final plan approval, the Owner shall prepare and submit a Sediment and Erosion Control Plan, appropriate to the site conditions, prior to undertaking any site alterations (filling, grading, removal of vegetation, etc.) and indicate how it is to be implemented during all phases of the site preparation and construction in accordance with the current Best Management Practices for Erosion and Sediment Control to the satisfaction of the Township of Edwardsburgh Cardinal and South Nation Conservation.
- 27. That the Subdivision Agreement contain a clause whereby the Owner agrees that upon completion of all stormwater works, to provide certification to the Township of Edwardsburgh Cardinal and South Nation Conservation, through a professional engineer, that all measures have been implemented in conformity with the approved stormwater site management plan.
- 28. That the Subdivision Agreement contains a clause whereby prior to the commencement of construction of any phase of the subdivision (roads, utilities and off-site works, etc.), the Owner agrees to:
 - a. have a professional engineer prepare an erosion and sediment control plan appropriate for site conditions in accordance with the current best management practices;
 - b. have this plan reviewed and approved by the Township of Edwardsburgh Cardinal and South Nation Conservation;
 - c. monitor the effectiveness of and maintain the erosion and sedimentation control works as necessary, and;
 - d. provide certification to the Township of Edwardsburgh Cardinal and South Nation Conservation through a professional engineer that the plan has been implemented.



Fisheries

- 29. The Owner acknowledges that the unnamed watercourse is considered either direct or indirect Fish Habitat as per Section 35 of the *Fisheries Act*.
- 30. The Owner shall establish a 30 metre "no touch/no development" setback of the unnamed watercourse, on both sides, measured from the top of the average annual highwater mark. The final approved plan of subdivision shall clearly show this setback. The berm required under condition 32.a. shall be located outside of this 30 metre setback. Any deviation from this setback shall be to the satisfaction of the Township of Edwardsburgh Cardinal and South Nation Conservation.
- 31. The subdivision agreement with the Township will indicate that in accordance with Section 35 of the *Fisheries Act*, the Harmful Alteration, Disruption or Destruction (HADD) of fish habitat is prohibited. The impacts that any such works may have on a fish habitat, whether directly adjacent to the site or downstream, may require approval of the Department of Fisheries and Oceans Canada.

Noise Attenuation and Warnings

- 32. That the subdivision agreement between the Owner and the Township contain the following provisions with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the Owner agrees to install a noise barrier for Phase 1 in accordance with subsection a. below and further that for Phase 2 for lots 1, 46-52 and 66-70 inclusive that the noise attenuation and warning requirements be in accordance with subsections b. to d. inclusive:
 - a. A treed earth berm for noise attenuation purposes shall be constructed as part of Phase 1. Notwithstanding what may be illustrated in the approved draft plan, the berm shall be designed and constructed to the satisfaction of the Township of Edwardsburgh Cardinal. No portion of the noise attenuation berm shall be located on the County Road right-of-way.

Note: This berm may be designed in such a way as to also meet condition 37.

- b. All units shall be equipped with forced air heating with central air conditioning.
- c. That Warning Clause Type D, in accordance with the following, shall be included on all Lease and Purchase and Sale Agreements.

Type D: "This dwelling has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the Municipality's and the Ministry of Environment's noise criteria."



- d. Bedroom windows facing north will require a minimum Sound Transmission Class (STC), being outdoor noise levels minus the targeted indoor noise level, of 26. Living room windows facing north will require a minimum STC of 21. Exterior wall components of north facades will require a minimum STC of 45, which will be achieved with brick cladding or an acoustical equivalent according to NRC test data. Detailed STC calculations will be completed prior to building permit application for each unit type and submitted to the Township with the building permit application.
- 33. That the subdivision agreement between the Owner and the Township contain provisions with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the owner agrees for Phase 2 for Lots 46-52 inclusive that Warning Clause Type A, as follows, will be included in all Lease and Purchase and Sale Agreements. This provision is in addition to those noise attenuation and warning requirements detailed in condition 32:

Type A: "Purchasers/tenants are advised that sound levels due to increasing rail traffic may occasionally interfere with some outdoor activities as the sound levels may exceed the sound level limits of the Township and the Ministry of the Environment, Conservation and Parks."

- 34. That the subdivision agreement between the Owner and the Township contain the following provision with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the Owner agrees where structural mitigation measures are required the Owner shall provide, prior to final building inspection, certification to the Township of Edwardsburgh Cardinal, through a Professional Engineer, that the noise control measures have been implemented in accordance with the approved study.
- 35. That the subdivision agreement between the Owner and the Township contain provisions with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the Owner agrees for all lots that rooftop HVAC equipment shall be prohibited.
- 36. The Owners acknowledges and agrees that building permits will not be issued for the development of individual lots in Phase 2 until the treed earth berm has been constructed to the satisfaction of the Township of Edwardsburgh Cardinal.

<u>CN Rail</u>

For Phase 1, conditions 37 and 42 shall apply:

37. A safety berm parallel to the railway rights-of-way with returns at the ends shall be installed between any publically accessible open space lands and the railway. The berm shall be 2.5 metres above



grade at the property line, with side slopes not steeper than 2.5 to 1. The location may be moved and height of the berm may be reduced proportionally to the distance separating the designated open space area from the north property line. Past the 120m setback from the property line there will be no requirements for a berm. For example, if the park area accessible to the public is to be located at 60 metres from the CN right of way, the required berm should be 1.25 metres tall. The safety berm and its characteristics and the limits of the park area accessible to the public shall be appropriately illustrated on the plan.

Note: This berm may be designed in such a way as to also meet condition 32.

For Phase 2, conditions 38 to 44 shall apply:

- 38. The Owner shall install and maintain a chain link fence of minimum 1.83 metre height along the mutual property line (being the north-west lot line of Block A). The safety fence and its characteristics must be illustrated in the plan.
- 39. Since the development is partially located within 300 metres of the CN main line, the Owner shall engage a consultant to undertake an analysis of noise. Subject to the review of the noise report, the Railway may consider other measures recommended by an approved Noise Consultant. CN will review the Noise report and will determine if mitigation measures will be required to be implemented by the Owner.
- 40. The following clause should be inserted in all development agreements, offers to purchase, and agreements of Purchase and Sale or Lease of each dwelling unit within 300 m of the railway right-of-way:

"Warning: Canadian National Railway Company or its assigns or successors in interest has or have a rights-of-way within 300 metres from the land the subject hereof. There may be alterations to or expansions of the railway facilities on such rights-of-way in the future including the possibility that the railway or its assigns or successors as aforesaid may expand its operations, which expansion may affect the living environment of the residents in the vicinity, notwithstanding the inclusion of any noise and vibration attenuating measures in the design of the development and individual dwelling(s). CNR will not be responsible for any complaints or claims arising from use of such facilities and/or operations on, over or under the aforesaid rights-of-way."

41. Any proposed alterations to the existing drainage pattern affecting railway property must receive prior concurrence from the Railway and be substantiated by a drainage report to the satisfaction of the Railway. The drainage plan indicates that all storm waters from the developments will be



directed to a pond and then into an existing ditch flowing away from CN property. However, CN will require a technical memo prepared by the project engineer explaining the design concept and confirming that all storm waters will be directed away from the CN right of way.

- 42. The Owner shall through restrictive covenants to be registered on title and all agreements of purchase and sale or lease provide notice to the public that the safety berm, fencing and noise isolation measures implemented are not to be tampered with or altered and further that the Owner shall have sole responsibility for and shall maintain these measures to the satisfaction of CN.
- 43. The Owner shall enter into an Agreement with CN stipulating how CN's concerns will be resolved and will pay CN's reasonable costs in preparing and negotiating the agreement.
- 44. The Owner shall be required to grant CN an environmental easement for operational noise and vibration emissions, registered against the subject property in favour of CN (within 300 metres from CN right of way).

Landscaping/Streetscaping

45. The Owner agrees to provide additional planting where necessary to provide a buffer between the existing properties and Lots 13-20 inclusive on the draft plan of subdivision, to the satisfaction of the Township of Edwardsburgh Cardinal.

Street Lighting

- 46. The Owner shall design and construct all necessary street lighting, interior and exterior to the subdivision, to the satisfaction of the Township of Edwardsburgh Cardinal. The Owner shall pay all related costs, including the cost of connection and inspection by Township personnel and/or the hydro authority.
- 47. The Owner agrees to provide streetlights on Street A and C, where the streets intersect with the Counties Road. Lighting shall be designed and installed under the guidance, requirements and to the satisfaction of the Counties. The Owner shall pay all related costs.

Grass Cutting, Ditch Maintenance and Schools

48. That the subdivision agreement between the Owner and the municipality and the Offers of Purchase and Sale Agreements and Deeds contain the following provisions with wording acceptable to the Township of Edwardsburgh Cardinal, wherein the Owner agrees:



- a. That the general maintenance and upkeep of all ditches and drains within the subdivision be the responsibility of the property owner.
- b. That grass cutting along the roadside within the subdivision be the responsibility of the property owner.
- 49. That the subdivision agreement between the Owner and the Township contain a provision that Agreements of Purchase and Sale indicate that it will not be possible to guarantee which school children residing in this subdivision may attend, and that transportation will be provided in accordance with the policy of the governing school board.

County Road Access and Widening

- 50. The Owner covenants and agrees that the subdivision agreement will contain clauses whereby the Owner covenants and agrees:
 - a. that they will design and construct the intersection of all roads within the Plan of Subdivision that intersect the County Road to the satisfaction of the United Counties of Leeds and Grenville.
 - b. to pay all expenses including those for drawing preparation, utility relocations, fees, security, road work, construction supervision, engineering and administrative costs for the modification of any intersection.
 - c. to obtain an entrance permit and/or enter into an agreement with the United Counties of Leeds and Grenville, to the satisfaction of the United Counties of Leeds and Grenville respecting the conditions of accessing the Counties road/road allowance prior to undertaking any work within the Counties road allowance.
 - d. to transfer Blocks C, D and Da to the United Counties of Leeds and Grenville at the Owner's cost for the purpose of a reserve to restrict access onto the Counties road. The lands shall be free of any encumbrances.
- 51. Road widening shall be deeded to the United Counties of Leeds and Grenville along the lot frontage which abuts County Road 22 as per Section 6.2.2 (d) of the Counties Official Plan. The road allowance should be 26.2 metres. Should sufficient allowance exist, a letter from a surveyor would meet the Counties' needs. Should the allowance not meet minimum desired right-of-way, an appropriate dedication (1/2 the desired allowance width, measured from the centerline of the current road) will be required to be incorporated into the final plan. All lands transferred for road purposes shall be free and clear from any encumbrances.



Hydro Installations

- 52. The Owner shall request a connection cost assessment from Hydro One and from Rideau St. Lawrence Distribution Inc. Should the cost assessment result in Hydro One supporting a Service Area Amendment, the Owner shall arrange for Rideau St. Lawrence Distribution Inc. to be the Hydro Electric Commission (i.e., provider).
- 53. The Owner shall arrange with the relevant Hydro Electric Commission for the installation of such services to the subdivision and for the provision of easements with respect to such installations. The Owner shall pay any cost involved in relocating any existing services required by the construction of works in the subdivision.
- 54. That prior to final plan approval by the Counties, the Owner shall enter into a Servicing Agreement with the relevant Hydro Electric Commission.

Enbridge Gas

- 55. That the subdivision agreement between the Owner and the Township contain the following to the satisfaction of the Township:
 - a. The developer is responsible for preparing a composite utility plan that allows for the safe installation of all utilities, including required separation between utilities;
 - b. Streets are to be constructed in accordance with composite utility plans previously submitted and approved by all utilities;
 - c. The developer shall grade all streets to final elevation prior to the installation of the gas lines and provide Enbridge Gas Distribution Inc. with the necessary field survey information for the installation of the gas lines; and
 - d. It is understood that the natural gas distribution system will be installed within the proposed road allowance. In the event this is not possible, easements will be provided at no cost to Enbridge Gas Distribution Inc.

Canada Post

56. The Owner shall consult with Canada Post to determine the locations of lay-bys for postal boxes outside of the County road allowance. The location of lay-bys, as agreed between the Owner and Canada Post, will be subject to the final approval of the Township.



Subdivision Agreement

57. That the subdivision agreement between the Owner and the Township contain wording acceptable to South Nation Conservation.

Traffic Impact Study

58. That prior to final approval by the Counties', the Owner shall submit a Traffic Impact Study addressing the impact of traffic from this development. The Traffic Impact Study shall be written to the satisfaction of the Township of Edwardsburgh Cardinal.

Clearance of Conditions

- 59. That prior to registration of the final plan, the United Counties of Leeds and Grenville is to be advised by the Township of Edwardsburgh Cardinal that Conditions 2-58, inclusive, have been satisfied.
- 60. That prior to registration of the final plan, the United Counties of Leeds and Grenville is to be advised by South Nation Conservation that Conditions 24, 26-28 inclusive, 30 and 57 have been satisfied.
- 61. That prior to registration of the final plan, the United Counties of Leeds and Grenville is to be advised by CN Rail that Conditions 37-44 have been satisfied.
- 62. That prior to final approval, the United Counties' subdivision approval authority is to be advised by the United Counties' Public Works Department that Conditions 20, 24, 25, 47, 50 and 51 have been satisfied.

NOTES TO DRAFT APPROVAL

- 1. It is the applicant's responsibility to fulfill the conditions of draft approval and to ensure that the required clearance letters are forwarded by the appropriate agencies to the United Counties of Leeds and Grenville and copied to the Township of Edwardsburgh Cardinal guoting File No. **07-T-10005**.
- 2. It is suggested that the Township register the subdivision agreement as provided by Section 51(26) of the Planning Act, R.S.O. 1990 against the land to which it applies, as notice to prospective purchasers.
- 3. All measurements in subdivision final plans must be presented in metric units.



- 4. If final approval is not given by the lapsing date, and no extensions have been granted pursuant to Section 51(33), then draft approval shall lapse pursuant to Section 51(32) of the *Planning Act*.
- 5. It is the responsibility of the Owner to request an extension of the draft plan approval. A request for extension should be made at least 60 days before the draft plan approval lapses. No extension can be given after the lapsing date. The request should include the reasons for requesting the extension, progress/status and the applicable fees.

Clearances Are Required From the Following Agencies

Township of Edwardsburgh Cardinal 18 Centre Street, P.O. Box 129 Spencerville, ON, K0E 1X0

South Nation Conservation 38 Victoria Street, P.O. Box 29 Finch, ON, KOC 1K0

Director of Public Works United Counties of Leeds and Grenville 25 Central Ave. W., Suite 100 Brockville, ON, K6V 4N6

CN Business Development and Real estate 1 Administration Road Concord, ON, L4K 1B9 c/o WSP proximity@cn.ca T : 1-438-459-9190 1600. René-Lévesque Ouest. 11e étage

1600, René-Lévesque Ouest, 11e étage Montreal (Quebec) H3H 1P9 CANADA

APPENDIX - C

PROPOSED SINGLE FAMILY SUBDIVISION – PHASES 1 & 2 ANTICIPATED WATER DEMAND

I- DESIGN CRITERIA

	Phase 1	Phase 2	Total
Population Density: 3.4 pers. per unit	3.4	3.4	3.4
Number of homes	59	36	95
Population in capita	200.6	122.4	323.0
Average Demand Volume Per Capita in L/c/day	350	350	350
Total Average Demand Volume in m3/day	70.2	42.8	113.1
Maximum Daily Demand (3.6 x Average) in m3/day*	252.8	154.2	407.0
Maximum Hourly Demand (5.4 x Average Daily) in m3/day*	379.1	231.3	610.5
Maximum Hourly Water Flow Required in L/s	4.39	2.68	7.07

* Peak factors of 3.6 and 5.4 for maximum daily demand and maximum hourly demand from Table 3-3 of the MOE Design Guidelines for Drinking-Water Systems for population fewer than 500 persons.

II- SUMMARY

	Phase 1	Phase 2	Total
Maximum Day Demand in L/s	2.9	1.8	4.7
Peak Hour Demand in L/s	4.4	2.7	7.1
Fire Flow Demand in L/s **	117.0	117.0	117.0
Maximum Day Demand plus Fire Flow Demand in L/s	119.9	118.8	121.7

** Refer to Fire Flow Calculation Sheet

III- PRESSURE REQUIREMENTS

Brossuro Chock	Minimu	Maximun	Maximum Pressure	
Flessule Check	(kPa)	(psi)	(kPa)	(psi)
Normal Use	345	50	552	80
Peak Hour Demand	276	40	552	80
Maximum Day and Fire Flow	140	20	552	80
Maximum pressure at any point in occupied areas				80
Maximum pressure at any point in un	689	100		

* Proposed watermain pipes: 150 mm and 200 mm diameter DR 18

* C_{hazen} is 100 and 110 for 150 mm and 200 mm respectively

* Proposed 10 fire hydrants; maximum distance between fire hydrants= 125 m



AS PER ZONING BY-LAW (R1): MAXIMUM BUILDING FOOTPRINT: 30% OF LOT AREA MINIMUM SETBACKS: AS SHOWN LOT 86 AREA = 487.42 m^2 30% OF LOT AREA = 146.23 m^2 ZONING: R1 MIN. LOT AREA: 465 m² MIN. FRONTAGE: 15 m MIN. FRONT YARD: 6 m MIN. REAR YARD: 7.5 m MIN. SIDE YARD: 2 OR 3 m (EXT. SY: 6 m) MAX. HEIGHT: 10 m MAXIMUM BUILDING FOOTPRINT = 30% OF LOT AREA

<u>NOTES</u>

* DISTANCES ARE IN METRE * PLAN NORTH SHOWN IS NOT THE GEOGRAPHIC NORTH

TYPICAL SINGLE FAMILY LOT LAYOUT USED FOR FIRE FLOW DEMAND ESTIMATION (1:500)

 $Q = K.V.S_{tot}$

Ontario Building Code 2012 (OBC), Appendix A, division B, A-3.2.5.7

Water supply for firefighting:

Q = minimum supply of water available in litres (L)

K = water supply coefficient for residential occupancy C and combustible construction A-3.2.5.7 Table 1

V = total building volume in cubic metres

Stot = total of spatial coefficient values from property line exposure on all sides, to a maximum of 2.0

 $S_{tot} = 1 + (S_{side1} + S_{side2} + S_{side3} + ... etc.)$

Typical single family house

Average Building Height =	9.0 m
Building Footprint =	146 m²
Total Building A Volume V =	1 314 m³

K from A-3.2.5.7 Table 1 = 23 Building of combustible construction. Floor assemblies are fire separations but with no fire-resistance rating.

* S _{tot} = 1+ (S _{side1} + S _{side2} + S _{side3} + etc.)		As per fi	gure 1
			S side i
Exposure Distance	N =	15.0 m	0
Exposure Distance	S =	32.0 m	0
Exposure Distance	E =	4.0 m	0.5
Exposure Distance V	V =	6.0 m	0.5
Total Spa	tial Co	pefficient =	2

Total Spatial Coefficient =

Minimum supply of water in litres Q = 60 444 L

For Q < 108 000 L

Required Minimum Water Supply Flow Rate as per Table 2, A-3.2.5.7 :

2 700 L/min at a minimum pressure of 140 kPa



Figure 1 Spatial Coefficient vs Exposure Distance

Further clarification of intent and sample problems and solutions are contained in the "Fire Protection Water Supply Guideline for Part 3 in the Ontario Building Code". This guideline may be obtained through the Office of the Fire Marshal's web site at: "www.ofm.gov.on.ca"

Fire Flow Protection according to the Fire Underwriters Survey (FUS) Guidelines 2020

Typical single family lot – Lot width 15 m

Required Basic Fire Flow (FUS – PART II)

w (FUS – PART II) $RFF = 220C\sqrt{A}$

Where: **RFF**: required fire flow in litres per minute; **C**: construction coefficient related to the type of construction **A**: total effective floor area (effective building area) in sq.m

		Option	Charge		
		Type V Wood Frame Construction	1.5		
		Type IV-A Mass Timber Construction	0.8		
		Type IV-B Mass Timber Construction	0.9		
Α	Type of Construction	Type IV-C Mass Timber Construction	1.0	Type V Wood Frame	4 5
		Type IV-D Mass Timber Construction	1.5	Construction	1.5
		Type III Ordinary Construction	1.0		
		Type II Noncombustible Construction	0.8		
		Type I Fire Resistive Construction	0.6		
	Ground Floor Area				146.0 m³
В	Second Floor Area				146.0 m³
	Total Effective Floor Area	A			292.0 m ³
С	Fire Flow F = 220 C A).5			5 639 L/min
		Rounde	ed to the n	earest 1.000 L/min RFF =	6 000 L/min

D		Option	Charge		
		Non-Combustible	-25%		
	Occupancy Adjustment	Limited-Combustible	-15%	Limited Combustible	-15%
	Occupancy Adjustment	Combustible	0%	Linnied-Compustible	
		Free Burning	15%		
		Rapid Burning	20%		
	Occupancy Adjustment				- 900 L/min
	Fire Flow				5 100 L/min

E		Option	Charge		0%
		None	0%		
	Sprinklar Protection	Automatic Sprinkler Protection (NFPA 13)	30%	Nono	
	Sprinkler Protection	Water Supply is Standard for System & Hose Lines	10%	None	
		Fully Supervised System	10%		
		Additional Reduction	0%		
				Sprinkler Reduction	000 L/min

F Exposures

North Side	Subject Building and Exposed Building Fully Protected with Automatic Sprinkler Systems		No
	Exposed Building Fully Protected with Automati	c Sprinkler Systems	No
	Exposed Wall Length		10.0 m
	Exposed Wall Height in Number of Storeys		2
	Length-Height Factor of Exposed Wall		20
	Distance to the Exposure		15.0 m
	Opti	ions	Charge
Construction Type of	Type V Wood Frame Construction		
Exposed Wall	Type III-IV w/ unprotected openings	Type V Wood Frame	
(FUS 2020 – Table 6 –	Type III-IV w/o protected openings	Construction	10%
page 31)	Type I-II w/ unprotected openings		
	Type I-II w/o protected openings		

	Subject Building and Exposed Building Fully Protected with Automatic Sprinkler Systems		No
	Exposed Building Fully Protected with Automat	ic Sprinkler Systems	No
East Side	Exposed Wall Length		20.0 m
East Side	Exposed Wall Height in Number of Storeys		2
	Length-Height Factor of Exposed Wall		40
	Distance to the Exposure		4.0 m
	Options		Charge
Construction Type of	Type V Wood Frame Construction		
Exposed Wall	Type III-IV w/ unprotected openings		
(FUS 2020 – Table 6 –	Type III-IV w/o protected openings		16%
page 31)	Type I-II w/ unprotected openings	Construction	
	Type I-II w/o protected openings		

South Side Subject Building and Exposed Building Fully Protected with Automatic Sprinkler Systems Exposed Building Fully Protected with Automatic Sprinkler Systems Exposed Wall Length Exposed Wall Height in Number of Storeys Length-Height Factor of Exposed Wall Distance to the Exposure Construction Type of Exposed Wall (FUS 2020 – Table 6 – page 31) Type I-II w/ unprotected openings Type III w/ unprotected openings Type III w/ oprotected openings Type I-II w/ oprotected openings	Subject Building and Exposed Building Fully Pr	No	
	No		
		10.0 m	
South Side	Exposed Wall Height in Number of Storeys		2
South Side Exposed Building Fully Protected with Automatic Sprinkler Syste South Side Exposed Wall Length Exposed Wall Height in Number of Storeys Length-Height Factor of Exposed Wall Distance to the Exposure Options Construction Type of Exposed Wall Type V Wood Frame Construction Type III-IV w/ unprotected openings Type Type III-IV w/ protected openings Type		20	
	Distance to the Exposure	32.0 m	
	Opt	Charge	
Construction Type of	Type V Wood Frame Construction		
Exposed Wall	Type III-IV w/ unprotected openings		
(FUS 2020 – Table 6 – page 31)	Type III-IV w/o protected openings		0%
	Type I-II w/ unprotected openings	Construction	
	Type I-II w/o protected openings		

	Subject Building and Exposed Building Fully Pr	otected with Automatic Sprinkler Systems	No		
West Side Subject Building and Exposed Building Fully Protected with Automatic Sprinkler Systems Exposed Building Fully Protected with Automatic Sprinkler Systems Exposed Building Fully Protected with Automatic Sprinkler Systems Exposed Wall Length Exposed Wall Length Exposed Wall Height in Number of Storeys Length-Height Factor of Exposed Wall Distance to the Exposure Distance to the Exposure Construction Type of Exposed Wall Type V Wood Frame Construction (FUS 2020 – Table 6 – page 31) Type III-IV w/ unprotected openings Type I-II w/ unprotected openings Type V Wood Frame Construction Type I-II w/ oprotected openings Type IV Wood Frame Construction	No				
	20.0 m				
west Side	Exposed Wall Height in Number of Storeys		2		
	Length-Height Factor of Exposed Wall		40		
West Side Exposed Building Fully F Exposed Wall Length Exposed Wall Length Exposed Wall Height in I Length-Height Factor of Distance to the Exposure Distance to the Exposure Construction Type of Type V Wood F Exposed Wall Type III-IV w/ un (FUS 2020 – Table 6 – page 31) Type III-IV w/ un	Distance to the Exposure	ce to the Exposure			
	Opt	Charge			
Construction Type of	Type V Wood Frame Construction				
Exposed Wall	Type III-IV w/ unprotected openings	Tune V Wood Frome			
(FUS 2020 – Table 6 –	Type III-IV w/o protected openings		21%		
page 31)	Type I-II w/ unprotected openings	Construction			
	Type I-II w/o protected openings				

Total charge for exposures = 47%

Total adjustment for exposures = 2 397 L/min

Adjusted Fire Flow (D)-(E)+(F) = 7 497 L/min

Rounded to the nearest 1,000 L/min RFF = 7 000 L/min

Notes:

G

1. Fire flow calculations have been prepared in accordance with Fire Underwriters Survey (v. 2020)

2. Second storey assumed to have floor area equal to first floor area.

Page 2/2

HYDRANT SAPCING

LOT/BLOCK	Number of FH WITHIN 75 m 5 700 L/min	Number of FH WITHIN 150 m 3 800 L/min	Available Fire Flow
1	2	2	19,000
8	2	3	22,800
15	2	2	19,000
20	2	1	15,200
24	2	1	15,200
36	2	2	19,000
46	2	2	19,000
58	1	3	17,100
75	2	2	19,000

Fire Hydrant Spacing and Required Fire Flow

* 5,700 and 3,800 L/min from Table 1 – Annex I – Technical Bulletin ISTB-2018-02



<u>NOTES</u>

* DISTANCES ARE IN METRE

PROPSOED SUBDIVISION

FIRE HYDRANT LAYOUT (SCALE: 1:2000)

CLOW CANADA - M-67 / M93 BRIGADIER FIRE HYDRANT SPECIFICATION

TESTING AND DESIGN SPECIFICATIONS (PER AWWA C502 / NSF /ULC & FM)

- 1. Hydrant shall be manufactured in accordance with AWWA C502 latest revision
- Hydrant Has been certified by UL in accordance with the ANSI/NSF 61 and ANSI/NSF 372 (LEAD CONTENT VERIFICATION OF PRODUCTS INCONTACT WITH POTABLE WATER)
- Hydrant shall be designed for 250 PSI working pressure and tested to 500 PSI hydrostatic pressure.
- 4. Hydrant shall be rated for 250 PSI. FM working pressure and 200 PSI. ULC working pressure.
- 5. Hydrant shall be a compression type, dry barrel design with centre operating stem construction.
- 6. The O-ring seating surface on the upper stem shall be constructed of stainless steel.
- 7. Epoxy coating to be applied to interior and exterior of hydrant shoe for corrosion protection.
- Hydrant shall be manufactured with operating nut and integral thrust collar made of bronze. A Delrin washer bearing shall be located above thrust collar for ease of hydrant operation.
- Hydrant shall have a lower valve assembly that fully encapsulates the lower operating rod threads. This allows for increased corrosion resistance and ease of disassembly.
- 10. Intermediate section shall be ductile iron. (AWWA C110-08)

STANDARD HYDRANT FEATURES

- 1. Body style: Round
- Hydrant shall have an internally lubricated bronze operating nut with O-ring seals. Operating nut shall be of the Hydra-lubeTM design to ensure self lubrication during operation.
- Hydrant hose nozzles shall be mechanically locked into place by an external allen screw, and have O-ring seals.
- 4. Hydrant Lower rod shall be 1-1/4" in sq.
- Hydrant shall have a main valve opening of 5-1/4".
- Hydrant shall be a traffic model, complete with safety flanges and stem coupling. Upper body can be rotated 360 degrees to adjust pumper direction.
- Hydrant shall be manufactured with a lower valve plate that bottoms out in the shoe for maximum opening.
- 8. Hydrant shall be backed by manufacturer's 12 year limited warranty
- 9. Hydrant shall be the Clow Canada Brigadier as manufactured by Clow Canada.



CLOW A division of Canada Pipe Company Ltd. CONCORD

OPTIONAL HYDRANT FEATURES M Eel/AIKOC 1. 2hose or 2hose & one pumper upper body M Eel/AIKOC 2. AVAILABLE INLETS: INCLUDING TRUST BLOCKST RESTRANT 150mm (6") Mechanical Joint (ANSI A-21.11) INCLUDING TRUST BLOCKST RESTRANT 150mm (6") Online chamber flanged (ANSI B16.1 Class 125) for (AWWA C110 - 08) tee 200mm (8") Online chamber flanged (ANSI B16.1 Class 125) for (AWWA C110 - 08) tee 150mm (6") flanged (ANSI B16.1 Class 125) for (AWWA C110 - 08) tee 150mm (6") flanged (ANSI B16.1 Class 125) 150mm (6") flanged (ANSI B16.1 Class 125) 150mm (6") flanged (ANSI B16.1 Class 250) 150mm (6") Tyton (AWWA C111/A21.11) 1000000000000000000000000000000000000
 All standard inlets available in CAST IRON ASTM A126 Class B Or Ductile Iron ASTM A536 (65-45-12) Hydra-lube operating nut – see standard shapes on submittal drawing Two 65mm (2.5") hose nozzles - threads on nozzle ends to suit national, provincial or municipal standard or STORZ quick connect One 114mm (4.5") pumper nozzle - threads on nozzle ends to suit national, provincial or municipal standard 100mm (4") or 125mm (5") CTORZ quick connect pumper nozzle. Nozzle caps to suit – see standard Shapes on submittal drawing. Two external .375" NPT plugs in inlet @ 180 degrees / one internal .25" NPT plug Hodrants painted / coated to suit national, provincial or municipal standard per AWWA C502 / AWWA C550
MisArity CLOW Consort A division of Conada Pipa Company Ltd.

ink ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Unit Headloss m/km	Friction Factor
pe P131	21.86	204	110	0.00	0.00	0.00	0.000
pe P116	10.88	155	100	1.42	0.08	0.10	0.053
pe P115	70.34	155	100	1.42	0.08	0.10	0.053
pe P125	79.39	155	100	-7.83	0.41	2.33	0.041
pe P124	70.48	155	100	-8.23	0.44	2.55	0.041
pe P128	20.39	250	110	38.41	0.78	3.62	0.029
pe P127	130.20	250	110	-38.41	0.78	3.62	0.029
pe P122	84.45	204	110	29.73	0.91	6.06	0.029
pe P121	16.61	200	110	29.48	0.94	6.57	0.029
pe P123	13.82	200	110	29.73	0.95	6.67	0.029
pe P126	63.58	204	110	38.41	1.18	9.74	0.028
pe P118	87.21	250	110	65.91	1.34	9.83	0.027
pe P117	64.11	155	100	27.50	1.46	23.85	0.034
pe P119	47.26	155	100	28.83	1.53	26.03	0.034
pe P120	86.05	155	100	29.28	1.55	26.79	0.034
pe P113	82.93	155	100	36.20	1.92	39.68	0.033
pe P114	14.95	155	100	-36.20	1.92	39.68	0.033
pe P106	33.18	204	110	-69.72	2.13	29.38	0.026
pe P105	9.29	204	110	-69.87	2.14	29.50	0.026
pe P104	36.44	204	110	-70.02	2.14	29.62	0.026
pe P103	84.21	204	110	-70.32	2.15	29.85	0.026
pe P102	30.00	204	110	72.19	2.21	31.34	0.026
pe P101	45.89	204	110	72.19	2.21	31.34	0.026
pe P0	0.1	250	110	-138.10	2.81	38.70	0.024
pe P111	91.09	155	100	64.38	3.41	115.27	0.030
pe P112	37.51	155	100	64.73	3.43	116.43	0.030
pe P110	69.91	155	100	-69.52	3.68	132.90	0.030
pe P109	9.46	155	100	-69.72	3.70	133.61	0.030
pe P108	19.53	155	100	-69.72	3.70	133.61	0.030
pe P107	5.63	155	100	-69.72	3.70	133.61	0.030
						-	



Pi

Node ID	Elevation m	Demand LPS	Head m	Pressure m	
Resvr R1	120	-138.10	120.00	0.00	
June J11	84.48	133.90	98.86	14.38	
Junc J10	84.83	0.20	108.15	23.32	
June J9	84.92	0.00	109.41	24.49	
June J12	83.84	0.35	109.36	25.52	
June J8	85.06	0.00	112.02	26.96	
June J7	84.91	0.00	112.78	27.87	
June J6	84.95	0.15	113.75	28.80	
June J5	84.92	0.15	114.02	29.10	
June J13	83.51	0.30	113.73	30.22	
Junc J4	84.85	0.30	115.10	30.25	
June J19	83.15	0.45	114.96	31.81	
June J14	83.76	0.00	117.02	33.26	
June J3	84.29	0.45	117.62	33.33	
June J16	84.21	0.00	117.62	33.41	
June J15	83.87	0.55	117.61	33.74	
June J2	84.48	0.00	118.56	34.08	
Junc J24	83.19	0.40	117.79	34.60	
June J20	82.52	0.20	117.26	34.74	
June J27	82.52	0.00	117.37	34.85	
June J21	82.41	0.25	117.37	34.96	
June J17	84.11	0.00	119.14	35.03	
Junc J1	84.92	0.00	120.00	35.08	
June J18	83.92	0.00	119.06	35.14	
June J22	82.09	0.00	117.88	35.79	
June J23	81.99	0.45	117.97	35.98	
June J25	82.11	0.00	118.59	36.48	



Network Table - Links





Link ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Unit Headloss m/km	Friction Factor
Pipe P131	21.86	204	110	0.00	0.00	0.00	0.000
Pipe P106	33.18	204	110	-19.69	0.60	2.83	0.031
Pipe P105	9.29	204	110	-19.84	0.61	2.86	0.031
Pipe P104	36.44	204	110	-19.99	0.61	2.91	0.031
Pipe P103	84.21	204	110	-20.29	0.62	2.99	0.031
Pipe P112	37.51	155	100	-18.54	0.98	11.49	0.036
Pipe P111	91.09	155	100	-18.89	1.00	11.90	0.036
Pipe P110	69.91	155	100	-19.49	1.03	12.61	0.036
Pipe P107	5.63	155	100	-19.69	1.04	12.85	0.036
Pipe P108	19.53	155	100	-19.69	1.04	12.85	0.036
Pipe P109	9.46	155	100	-19.69	1.04	12.85	0.036
Pipe P117	64.11	155	100	22.07	1.17	15.88	0.035
Pipe P124	70.48	155	100	22.75	1.21	16.78	0.035
Pipe P125	79.39	155	100	23.15	1.23	17.34	0.035
Pipe P114	14.95	155	100	-23.24	1.23	17.47	0.035
Pipe P113	82.93	155	100	23.24	1.23	17.47	0.035
Pipe P116	10.88	155	100	24.87	1.32	19.80	0.035
Pipe P115	70.34	155	100	24.87	1.32	19.80	0.035
Pipe P101	45.89	204	110	45.61	1.40	13.39	0.028
Pipe P102	30.00	204	110	45.61	1.40	13.39	0.028
Pipe P127	130.20	250	110	-70.42	1.43	11.12	0.027
Pipe P128	20.39	250	110	70.42	1.43	11.12	0.027
Pipe P118	87.21	250	110	92.49	1.88	18.42	0.025
Pipe P126	63.58	204	110	70.42	2.15	29.93	0.026
Pipe P120	86.05	155	100	-41.03	2.17	50.05	0.032
Pipe P119	47.26	155	100	-41.48	2.20	51.07	0.032
Pipe P0	0.1	250	110	-138.10	2.81	38.70	0.024
Pipe P122	84.45	204	110	92.72	2.84	49.81	0.025
Pipe P121	16.61	200	110	92.47	2.94	54.58	0.025
Pipe P123	13.82	200	110	92.72	2.95	54.86	0.025

Network Table - Nodes

R1

Node ID	Elevation m	Demand LPS	Head m	Pressure m
Resvr R1	120	-138.10	120.00	0.00
Junc J20	82.52	133.50	108.94	26.42
Junc J27	82.52	0.00	109.85	27.33
Junc J21	82.41	0.25	109.85	27.44
Junc J19	83.15	0.45	113.25	30.10
June J22	82.09	0.00	114.05	31.96
June J13	83.51	0.30	115.66	32.15
Junc J12	83.84	0.35	116.09	32.25
June J11	84.48	0.60	117.18	32.70
June J24	83.19	0.40	116.00	32.81
June J23	81.99	0.45	114.81	32.82
June J10	84.83	0.20	118.06	33.23
June J9	84.92	0.00	118.18	33.26
June J14	83.76	0.00	117.11	33.35
June J8	85.06	0.00	118.43	33.37
June J15	83.87	0.55	117.37	33.50
June J7	84.91	0.00	118.50	33.59
June J6	84.95	0.15	118.60	33.65
June J5	84.92	0.15	118.62	33.70
Junc J4	84.85	0.30	118.73	33.88
June J18	83.92	0.00	118.16	34.24
June J17	84.11	0.00	118.39	34.28
June J16	84.21	0.00	118.76	34.55
June J25	82.11	0.00	116.72	34.61
June J3	84.29	0.45	118.98	34.69
June J2	84.48	0.00	119.38	34.90
June J1	84.92	0.00	120.00	35.08

FIRE HYDRANTS ARE LOCATED AT J4, J8, J11, J12, J14, J16, J19, J20, J22, J24

Page 321 of 465



Link ID	Length m	Diameter mm	Roughness	Flow LPS	Velocity m/s	Unit Headloss m/km	Friction Factor
Pipe P131	21.86	204	110	0.00	0.00	0.00	0.000
Pipe P119	47.26	155	100	0.30	0.02	0.01	0.066
Pipe P111	91.09	155	100	0.50	0.03	0.01	0.062
Pipe P124	70.48	155	100	-0.93	0.05	0.05	0.056
Pipe P125	79.39	155	100	1.21	0.06	0.07	0.054
Pipe P106	33.18	204	110	-3.78	0.12	0.13	0.040
Pipe P121	16.61	200	110	3.78	0.12	0.15	0.040
Pipe P112	37.51	155	100	2.37	0.13	0.26	0.049
Pipe P105	9.29	204	110	-4.58	0.14	0.19	0.039
Pipe P120	86.05	155	100	2.71	0.14	0.33	0.048
Pipe P110	69.91	155	100	-2.71	0.14	0.33	0.048
Pipe P116	10.88	155	100	2.72	0.14	0.33	0.048
Pipe P115	70.34	155	100	2.72	0.14	0.33	0.048
Pipe P122	84.45	204	110	5.12	0.16	0.23	0.038
Pipe P123	13.82	200	110	5.12	0.16	0.26	0.038
Pipe P104	36.44	204	110	-5.38	0.16	0.26	0.038
Pipe P128	20.39	250	110	8.46	0.17	0.22	0.036
Pipe P127	130.20	250	110	-8.46	0.17	0.22	0.036
Pipe P113	82.93	155	100	3.69	0.20	0.58	0.046
Pipe P114	14.95	155	100	-3.69	0.20	0.58	0.046
Pipe P108	19.53	155	100	-3.78	0.20	0.60	0.046
Pipe P107	5.63	155	100	-3.78	0.20	0.60	0.046
Pipe P109	9.46	155	100	-3.78	0.20	0.60	0.046
Pipe P103	84.21	204	110	-6.99	0.21	0.41	0.036
Pipe P126	63.58	204	110	8.46	0.26	0.59	0.035
Pipe P117	64.11	155	100	5.12	0.27	1.06	0.044
Pipe P118	87.21	250	110	13.58	0.28	0.53	0.034
Pipe P101	45.89	204	110	12.12	0.37	1.15	0.034
Pipe P102	30.00	204	110	12.12	0.37	1.15	0.033
Pipe P0	0.1	250	110	-25.70	0.52	1.67	0.030

Network

k	Table	-]	Links

PROPOSED SINGLE FAMILY SUBDIVISION – PHASE 1&2 SANITARY SEWER DESIGN

1- DESIGN FLOW CALCULATION

 $Q_d = (M . q . P / 86.4) + I . A$ Where: Q_d = Peak Design Flow (L/s) M = Peaking Factor (Max = 4; Min = 1.5)q = Average Daily Flow per capita per day (L/c/day) P = Population = 2.7 capita per townhouse I = Infiltration Contribution (0.28 L/s/eff. gross ha) A = Gross Drainage Area (ha) A (ha) = **7.6677** ha (Phase 1&2 covered) q (L/c/day) = 350L/c/day Number of Lots 95 Units Single Family Population = 3.4 Capita per unit Population = 323 Capita M (Harmon's Peaking Factor) = 3.45 M= 1+(14/(4+P^0.5))k = 3.45 k: Correction Factor (0.8) L/s Extraneous Flow 0.28 x A (L/s) = 2.15Extraneous Flow $0.05 \times A (L/s) = 0.38$ As per Technical Bulletin L/s Average Dry Weather Flow Rate ADWF = 1.69 L/s Peak Dry Weather Flow Rate PDWF = 4.90 L/s Peak Wet Weather Design Flow Rate

ow Rate **Q**₄ (**L/s) = <u>7.04</u> L/s Q₄ (m³/day) = 608.64** m³/day

2- EXISTING SEWER CAPACITY CALCULATION – COUNTY RD a- PIPE AT COUNTY RD 22 / GILL ST

Manning's Equation	D (mm) =	250				
Q=1/n.A.R ^{2/3} .S ^{1/2}	A (m²) =	0.0491				
	n =	0.013	Manni	ng Co	oefficie	ent
	R (m) =	0.06	Hydra	ulic R	Radius	(m)
	S =	0.96%	Slope	(%)		
		Q=1/n *A	*R ^{2/3} *	S ^{1/2}		
Full Pipe Capacity	Q _f (m ³ /s)=	0.0583	m³/s	=	58.3	L/s
	V _f (m/s)=	1.19	m/s			
- Anticipated sewage flow from	subdivision c	ontributio	on repre	esent	s:	

12.1% of the existing sewer capacity.

b- PIPE AT COUNTY RD 22 / DODGE ST

$$\begin{array}{c|c} \mathsf{D}(\mathsf{mm}) = & \mathbf{250} \\ \mathsf{A}(\mathsf{m}^2) = & \mathbf{0.0491} \\ \mathsf{n} = & \mathbf{0.013} \\ \mathsf{R}(\mathsf{m}) = & \mathbf{0.06} \\ \mathsf{B}(\mathsf{m}) = & \mathbf{0.06} \\ \mathsf{S} = & \mathbf{0.28\%} \\ \mathsf{Slope}(\%) \\ \mathsf{Q=1/n} * \mathsf{A} * \mathsf{R}^{2/3} * \mathsf{S}^{1/2} \\ \mathsf{Full} \ \mathsf{Pipe} \ \mathsf{Capacity} \quad \mathsf{Q}_{\mathsf{f}}(\mathsf{m}^3/\mathsf{s}) = & \mathbf{0.0315} \\ \mathsf{V}_{\mathsf{f}}(\mathsf{m}/\mathsf{s}) = & \mathbf{0.64} \\ \mathsf{m/s} \\ \mathsf{r} \\ \mathsf{Anticipated} \ \mathsf{sewage} \ \mathsf{flow} \ \mathsf{from} \ \mathsf{subdivision} \ \mathsf{contribution} \ \mathsf{represents} : \end{array}$$

22.4% of the existing sewer capacity.
NOTES:

Refer to sanitary sewer calculation sheet for all sewer segments within the subdivision Minimum diameter for sanitary main sewer: 200 mm (8") Maximum velocity = 3 m/s Minimum velocity = 0.6 m/s Minimum depth of cover 2.5 m from crown of sewer to finished grade Minimum vertical clearance between sewer and watermain is 0.5 m if sewer above Minimum horizontal clearance between sewer and watermain is 2.5 m Special treatment of manholes and pipe if high groundwater level Maximum spacing of manholes 120 m Drops at manholes: 30 mm (straight sewer) and 0.6 (45 to 90 deg sewer)

Pipe material: PVC DR of 35 320 kPa or equivalent

Manholes: precast or poured concrete as per OPSD standards

Bedding: as per OPSD standards and geotechnical

GRAPH USED TO DETERMINE ACTUAL FLOW DEPTH AND VELOCITY

Q/Q _{fun}	h/D	v/van	R/D	Q/Q _{bult}	h/D	V/V _{full}	R/D
0.095	0.205	0.64	0.1233	0.610	0.568	1.04	0.2697
0.100	0.211	0.65	0.1265	0,620	0.575	1.04	0.2715
0.105	0.216	0.66	0.1291	0.630	0.581	1.05	0.2731
0.110	0.221	0.67	0.1317	0.640	0.587	1.05	0.2745
0.115	0.226	0.68	0.1343	0.650	0.594	1.05	0.2762
0.120	0.231	0.69	0.1369	0.660	0.600	1.05	0.2776
0.125	0.236	0.69	0.1395	0.670	0.607	1.06	0.2793
0.130	0.241	0.70	0.1421	0.680	0.613	1.06	0.2806
0.135	0.245	0.71	0.1441	0.690	0.620	1.06	0.2821
0.140	0.250	0.72	0.1466	0.700	0.626	1.06	0.2834
0.145	0.255	0.72	0.1491	0.710	0.633	1.06	0.2848
0.150	0.259	0.73	0.1511	0.720	0.640	1.07	0.2862
0.155	0.263	0.74	0.1531	0.730	C.646	1.07	0.2874
0.160	0.268	0.74	0.1556	0.740	C.653	1.07	0.2887
0.165	0.272	0.75	0.1575	0.750	0.660	1.07	0.2900
0.170	0.276	0.76	0.1595	0.760	C.667	1.07	0.2912
0.175	0.281	0.76	0.1619	0.770	C.675	1.07	0.2925
0.180	0.285	0.77	0.1638	0.780	C.682	1.07	0.2936
0.190	0.293	0.78	0.1676	0.790	C.689	1.07	0.2947
0.200	0.301	0.79	0.1714	0.800	C.697	1.07	0.2958
0.210	0.309	0.80	0.1751	0.805	C.701	1.08	0.2964
0.220	0.316	0.81	0.1784	0,810	C.705	1.08	0.2969
0.230	0.324	0.82	0,1820	0.815	0.709	1.08	0.2974
0.240	0.331	0.83	0.1851	0.820	0.713	1.08	0.2979
0.250	0.339	0.84	0.1887	0.825	0.717	1.08	0.2984
0.260	0.346	0.85	0.1919	0.830	0.721	1.08	0.2989
0.270	0.353	0.86	0.1948	0.835	0.725	1.08	0.2993
0.280	0.360	0.86	0,1978	0.840	0.729	1.07	0.2997
0.290	0.367	0.87	0.2007	0.845	0.734	1.07	0.3002
0.300	0.374	0.88	0.2037	0.850	0.738	1.07	0.3006
0.310	0.381	0.89	0,2066	0.855	0.742	1.07	0.3010
0.320	0.387	0.89	0.2090	0.850	0.747	1.07	0.3014
0.330	0.394	0.90	0.2118	0.865	0.751	1.07	0.3018
0.340	0.401	0.91	0.2146	0.870	0.756	1.07	0.3022
0.350	0.407	0.92	0.2170	D.875	0.761	1.07	0.3025
0.360	0.414	0.92	0.2197	0.880	0.766	1.07	0.3028
0.370	D.420	0.93	0.2220	0.885	0.770	1.07	0.3031
0.380	0.426	0.93	0.2243	0.890	0.775	1.07	0 3033
0.390	0.433	0.94	0.2269	0.895	0.781	1 07	0 3036
0.400	0.439	0.95	0.2291	0.900	0.786	1.07	0.3038
0.410	0.445	0.95	0.2313	0.905	0.791	1.07	0.3040
0.420	0.451	0.96	0.2334	0.910	0.797	1.07	0.3041
0.430	0.458	0.96	0.2359	0.915	0.803	1.06	0.3042
0-440	0.464	0.97	0.2380	0.920	0.808	1.06	0.3043
0.450	0.470	0.97	0.2401	0.925	0.814	1.06	0.3043
0.460	0.476	0.98	0.2420	0.930	0.821	1.06	0 3043
0.470	0.482	0.99	0.2441	0.935	0.827	1.06	0.3042
0.480	0.488	0.99	0.2461	0.940	0.834	1.05	0.3040
0.490	0.494	1.00	0.2481	0.945	0.841	1.05	0 3037
0.500	0.500	1.00	0.2500	0,950	0.849	1.05	0.3033
0.510	0.506	1.00	0.2519	0.955	0.856	1.05	0.3029
0.520	0.512	1.01	0.2538	0.960	0.865	1.04	0.3022
0.530	0.519	1.01	0.2559	0.965	0.874	1.04	0.3014
0.540	0.525	1.02	0.2577	0.970	0.883	1.04	0.3004
0.550	0.531	1.02	0.2595	0.975	0.894	1.03	0.2989
0.560	0.537	1.02	0.2612	0.980	0.905	1.03	0.2972
0.570	0.543	1.03	0.2629	0.985	0.919	1.02	0.2946
0.580	0.550	1.03	0.2649	0.990	0.935	1.02	0.2908
0.590	0.556	1.03	0.2665	0.995	0.956	1.01	0.2844
	0.500	1.04	0.0000	1 000	1.000	1.01	0.2044

COUNTY ROAD No. 22



PH-2 PH-1



VACANT LAND (RURAL)

	TITLE:	SCALE: 1:1250	DRAWING No.:
ON ., ON	SANITARY DRAINAGE AREAS	DRAFTED BY: PROJECT No.: 0114 DATE: 02/06/2024	SA-1

SANITARY SEWER DESIGN CALCULATION SHEET

										Refer to D	rawing SA-1 for sanitary sewer system layout Manning's n = 0.013													
l		TION			RESID	ENTIAL A	REA AN	D PO	PULATIO	N		INFIL	TRATION	FLOW		PI	ROPO	SED S	ANITARY	SEW	R DES	IGN		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25
	Man N	hole o.		Number of Uni	Dwelling ts	Indivi	dual	Cun	nulative		Pop. Peak	Acc.	Peak Infiltration	Peak Design	Pipe Length	Pipe Diameter		Slope	Pipe Capacity	Full Flow Velocity	Flow	% Full	Flow	Actual Flow Velocity
Location Street		-	Catch- ment	Semi-	Single	Рор.	Area	Рор.	Area	Peaking Factor	Q P	Alea	Flow Q i	d d	L	d	Pipe Type	3	Q f	V f	>0.6 m/s		Deptil	V _p @Q _d
	MH	MH		Detached (2.7)	Family (3.4)	(Cap)	(ha)	(Cap)	(ha)	(M)	(L/s)	(ha)	0.33*Area	(L/s)	(m)	(mm)	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	%	(L/s)	(m/s)	<3.0 m/s	%	(mm)	(m/s)
			102 Erom	Euturo Dovo	lonmont (S	outh):		24.0	0.7200	4.00	0.44	0 7200	0.24	0.69										<u> </u>
Street B	102		SAN 1			7 0	0 2227	<u> </u>	0.7200	4.00	0.44	0.7200	0.24	0.00	36.1	203	DR35	1 60	/3.2	1 3 3	OK	2.0%	20	0.53
Street B	102	104	SAN 2		1	4.0	0.1286	45.0	1.0713	4.00	0.58	1.0713	0.35	0.94	13.1	203	DR35	1.20	37.4	1.16	OK	2.5%	20	0.49
Street B	106	108	SAN 3		7	24.0	0.4797	69.0	1.551	4.00	0.89	1.5510	0.51	1.41	56.0	203	DR35	1.00	34.1	1.05	OK	4.1%	28	0.52
Street B	108	110	SAN 4		7	24.0	0.4796	93.0	2.0306	4.00	1.21	2.0306	0.67	1.88	63.3	203	DR35	0.65	27.5	0.85	ОК	6.8%	36	0.50
Street B	110	112	SAN 5		5	17.0	0.4512	110.0	2.4818	4.00	1.43	2.4818	0.82	2.24	44.4	203	DR35	0.65	27.5	0.85	ОК	8.2%	39	0.51
Street B	112	114	SAN 6		2	7.0	0.2689	117.0	2.7507	4.00	1.52	2.7507	0.91	2.42	41.3	203	DR35	0.60	26.4	0.82	OK	9.2%	42	0.51
Street B	114	116	SAN 7		6	21.0	0.5478	138.0	3.2985	4.00	1.79	3.2985	1.09	2.88	74.4	203	DR35	0.80	30.5	0.94	ОК	9.4%	42	0.61
Street B	116	118	SAN 8		6	21.0	0.5384	159.0	3.8369	4.00	2.06	3.8369	1.27	3.33	75.5	203	DR35	1.26	38.3	1.18	ОК	8.7%	41	0.73
																								L
Street B	122	124	SAN 9		1	4.0	0.1337	4.0	0.1337	4.00	0.05	0.1337	0.04	0.10	12.7	203	DR35	2.00	48.3	1.49	OK	0.2%	8	0.30
Street B	124	126	SAN 10		9	31.0	0.5923	35.0	0.726	4.00	0.45	0.726	0.24	0.69	68.2	203	DR35	1.00	34.1	1.05	OK	2.0%	20	0.42
Street B	126	128	SAN 11		8	28.0	0.5122	63.0	1.2382	4.00	0.82	1.2382	0.41	1.23	61.1	203	DR35	0.80	30.5	0.94	OK	4.0%	28	0.46
Street B	128	130	SAN 12		1	24.0	0.4881	87.0	1.7263	4.00	1.13	1.7263	0.57	1.70	72.5	203	DR36	0.65	27.5	0.85	UK	6.2%	34	0.47
Street A	136	130	SAN 13		10	34.0	0 7187	34.0	0 7187	1 00	0.44	0 7187	0.24	0.68	Q1 1	203	DR35	1 00	3/1 1	1.05	OK	2.0%	20	0.42
OlleelA	100	100			10	04.0	0.7107	04.0	0.7107	+.00	0.77	0.7107	0.24	0.00	31.1	200		1.00	04.1	1.00		2.070	20	0.42
			At Node I	MH 130 From	MH 128 a	nd MH 136:					1.57	2.4450	0.81	2.38										<u> </u>
Street B	130	132	SAN 14		7	24.0	0.5132	145.0	2.9582	4.00	1.88	2.9582	0.98	2.86	78.4	203	DR35	0.43	22.4	0.69	ОК	12.8%	49	0.48
Street B	132	134	SAN 15		6	21.0	0.4593	166.0	3.4175	4.00	2.15	3.4175	1.13	3.28	71.5	203	DR35	0.40	21.6	0.67	ОК	15.2%	54	0.48
	At No	de MH	134 From	Future Deve	lopment S	treet C:		34.0	0.72	4.00	0.44	0.7200	0.24	0.68										
Street C	134	118	SAN 16		11	38.0	0.7999	238.0	4.9374	4.00	3.09	4.9374	1.63	4.71	103.6	203	DR35	0.40	21.6	0.67	OK	21.8%	65	0.54
			At Node I	MH 118 From	MH 116 a	nd MH 134:					5.15	8.7743	2.90	8.04										
Street B	118	120	SAN 17		0	0.0	0.0942	397.0	8.8685	4.00	10.29	8.8685	2.93	13.22	24.4	203	DR35	1.00	34.1	1.05	OK	38.7%	88	0.99
		PS		Total	95	329																		

Design Parameters:

q = Average daily per capita flow 280 L/day per capita (Ottawa Sewer Guidelines) q_i = Unit of peak extraneous flow 0.28 + 0.05 = 0.33 L/effect. Gross ha.s M = Residential peaking factor $M = 1 + (14 / (4 + \sqrt{P})) * K$ (Harmon Equation Max.=4) P: Population in 1000 K: Correction factor = 0.8 Q_p = Peak population flow (L/s) $Q_{p} = P x q x M / 86.4 (L/s)$ Q_i = Peak extraneous flow (L/s) $Q_i = q_i x A (L/s)$ A = Area in hectares Q_d = Peak design flow (L/s) $Q_d = Q_p + Q_i (L/s)$ Dry weather flow (DWF): Average DWF = AWF (all land uses) + DWGWI (all land uses) Peak DWF = AWF (res) x M + AWF (ICI) + DWGWI (all land uses) Where: AWF = Average Wastewater Flow DWGWI = Dry Weather Ground Water Infiltration

Notes:

1. Minimum diameter for sanitary gravity sewer: 200 mm (8")

- 2. Minimum velocity = 0.6 m/s
- 3. Maximum velocity = 3 m/s

4. Minimum depth of cover 2.5 m from crown of sewer to finished grade

5. Minimum vertical clearance between sewer and watermain is 0.15 m and 0.5 m if sewer above

6. Minimum horizontal clearance between sewer and watermain is 2.5 m

7 . Pipe material: PVC DR 35 320 KPa or equivalent

8. Sewer bedding: As per OPSD standard 802.010 or as specified by the geotechnical engineer

9. Special treatment of manholes and pipe if high groundwater level

- 10 . Manhole inner diameter: 1200 mm
- 11 . Maximum spacing between manholes: 120 m

12 . Drops at manholes: 30 mm for straight sewer and 60 mm for sewer at 45 to 90 deg

- 13 . Manholes: Precast or poured concrete as per OPSD
- 14. Minimum diameter for individual service connections (PVC DR 28): 100 mm (4") w/ min grade 1% (preferred 2%)
- 15. Use tees or wyes, strap-on-saddles for connections to main sewer

Population per single family house 3.4 (Ottawa Sewer Guidelines)

Res = Residential ICI = Institutional Commercial Industrial

SANITARY SEWER DESIGN CALCULATION SHEET

DESIGN CONSIDERING 2 DWELLING UNITS PER LOT

										Refer to D	rawing	SA-1 for	r sanitary sew	ver system l	ayout				Manr	ning's n =	0.013			
L	OCA1	ΓΙΟΝ			RES	IDENTIAL	AREA	AND F	OPULAT	ION		INFIL	TRATION	FLOW		P	ROPO	SED S	ANITAR	Y SEWE	R DES	IGN		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25
	Manl No	hole o.		Numl Dwellin	ber of Ig Units	Individ	dual	Cun	nulative	Posking	Pop. Peak Flow	Acc. Area	Acc. Peak Infiltration	Peak Design	Pipe Length	Pipe Diameter		Slope s	Pipe Capacity	Full Flow Velocity	Flow Check	% Full	Flow Depth	Actual Flow Velocity
Location Street			Catch-	Semi-	Single	Pop.	Area	Pop.	Area	Factor	Q₽		Flow Q i	Flow Q d	L	d	Pipe Type		Qf	V f	>0.6 m/s			V _p @ Q _d
0.1001	From MH	To MH		Detach ed (2.7)	Family (3.4)	(Cap)	(ha)	(Cap)	(ha)	(M)	(L/s)	(ha)	0.33*Area	(L/s)	(m)	(mm)		%	(L/s)	(m/s)	<3.0 m/s	%	(mm)	(m/s)
			102 Erom	Euturo	Dovolopr	nont (South	\.	68.0	0 7200	4.00	0.88	0 7200	0.24	1 1 2										
Street B	102			rulure		14 0). ∩ 2227	82.0	0.7200	4.00	1.06	0.7200	0.24	1.12	36.1	203	DR35	1 60	13.2	1 3 3	OK	3.2%	25	0.61
Street B	102	104	SAN 2		2	8.0	0.2227	90.0	1 0713	4.00	1.00	1 0713	0.35	1.57	13.1	203	DR35	1.00	37.4	1.55	OK	<u> </u>	28	0.01
Street B	104	108	SAN 3		14	48.0	0.1200	138.0	1.571	4 00	1 79	1.5510	0.51	2.30	56.0	203	DR35	1.00	34.1	1.10	OK	6.7%	36	0.60
Street B	108	110	SAN 4		14	48.0	0.4796	186.0	2.0306	4.00	2.41	2.0306	0.67	3.08	63.3	203	DR35	0.65	27.5	0.85	OK	11.2%	46	0.56
Street B	110	112	SAN 5		10	34.0	0.4512	220.0	2.4818	4.00	2.85	2.4818	0.82	3.67	44.4	203	DR35	0.65	27.5	0.85	OK	13.3%	50	0.60
Street B	112	114	SAN 6		4	14.0	0.2689	234.0	2.7507	4.00	3.03	2.7507	0.91	3.94	41.3	203	DR35	0.60	26.4	0.82	OK	14.9%	53	0.60
Street B	114	116	SAN 7		12	42.0	0.5478	276.0	3.2985	4.00	3.58	3.2985	1.09	4.67	74.4	203	DR35	0.80	30.5	0.94	OK	15.3%	54	0.68
Street B	116	118	SAN 8		12	42.0	0.5384	318.0	3.8369	4.00	4.12	3.8369	1.27	5.39	75.5	203	DR35	1.26	38.3	1.18	OK	14.1%	52	0.84
Street B	122	124	SAN 9		2	8.0	0.1337	8.0	0.1337	4.00	0.10	0.1337	0.04	0.15	12.7	203	DR35	2.00	48.3	1.49	OK	0.3%	8	0.34
Street B	124	126	SAN 10		18	62.0	0.5923	70.0	0.726	4.00	0.91	0.7260	0.24	1.15	68.2	203	DR35	1.00	34.1	1.05	OK	3.4%	26	0.50
Street B	126	128	SAN 11		16	56.0	0.5122	126.0	1.2382	4.00	1.63	1.2382	0.41	2.04	61.1	203	DR35	0.80	30.5	0.94	OK	6.7%	36	0.54
Street B	128	130	SAN 12		14	48.0	0.4881	174.0	1.7263	4.00	2.26	1.7263	0.57	2.83	72.5	203	DR36	0.65	27.5	0.85	OK	10.3%	44	0.55
Street A	136	130	SAN 13		20	68.0	0.7187	68.0	0.7187	4.00	0.88	0.7187	0.24	1.12	91.1	203	DR35	1.00	34.1	1.05	OK	3.3%	25	0.49
			At Node	MH 130	From MH	128 and M	H 136:				3.14	2.4450	0.81	3.94										
Street B	130	132	SAN 14		14	48.0	0.5132	290.0	2.9582	4.00	3.76	2.9582	0.98	4.74	78.4	203	DR35	0.43	22.4	0.69	OK	21.2%	64	0.55
Street B	132	134	SAN 15		12	42.0	0.4593	332.0	3.4175	4.00	4.30	3.4175	1.13	5.43	71.5	203	DR35	0.40	21.6	0.67	OK	25.2%	70	0.56
	At Nod	e MH	134 From	Future I	Developr	nent Street	C:	68.0	0.72	4.00	0.88	0.7200	0.24	1.12										
Street C	134	118	SAN 16		22	76.0	0.7999	476.0	4.9374	4.00	6.17	4.9374	1.63	7.80	103.6	203	DR35	0.40	21.6	0.67	OK	36.1%	85	0.62
			At Node	MH 118	From MH	116 and M	134:				10.29	8.7743	2.90	13.19										
Street B	118	120	SAN 17		0	0.0	0.0942	794.0	8.8685	4.00	20.59	8.8685	2.93	23.51	24.4	203	DR35	1.00	34.1	1.05	OK	68.9%	125	1.14
		PS		Total	190	658																		

Design Parameters:

- q = Average daily per capita flow q_i = Unit of peak extraneous flow M = Residential peaking factor
- Q_{p} = Peak population flow (L/s) Q_i = Peak extraneous flow (L/s) Q_{d} = Peak design flow (L/s)

Dry weather flow (DWF):

Average DWF = AWF (all land uses) + DWGWI (all land uses)

Peak DWF = AWF (res) x M + AWF (ICI) + DWGWI (all land uses)

- Where: AWF = Average Wastewater Flow
 - DWGWI = Dry Weather Ground Water Infiltration

Res = Residential ICI = Institutional Commercial Industrial

K: Correction factor = 0.8 $Q_{p} = P x q x M / 86.4 (L/s)$

P: Population in 1000

 $Q_i = q_i x A (L/s)$ A = Area in hectares

0.28 + 0.05 = 0.33 L/effect. Gross ha.s

 $Q_d = Q_p + Q_i (L/s)$

280 L/day per capita (Ottawa Sewer Guidelines)

 $M = 1 + (14 / (4 + \sqrt{P})) * K$ (Harmon Equation Max.=4)

Notes:

4. Minimum depth of cover 2.5 m from crown of sewer to finished grade 5. Minimum vertical clearance between sewer and watermain is 0.15 m and 0.5 m if sewer above

2. Minimum velocity = 0.6 m/s

3 . Maximum velocity = 3 m/s

- 6. Minimum horizontal clearance between sewer and watermain is 2.5 m
- 7 . Pipe material: PVC DR 35 320 KPa or equivalent
- 8. Sewer bedding: As per OPSD standard 802.010 or as specified by the geotechnical engineer
- 9. Special treatment of manholes and pipe if high groundwater level

1. Minimum diameter for sanitary gravity sewer: 200 mm (8")

- 10 . Manhole inner diameter: 1200 mm
- 11 . Maximum spacing between manholes: 120 m
- 12 . Drops at manholes: 30 mm for straight sewer and 60 mm for sewer at 45 to 90 deg
- 13 . Manholes: Precast or poured concrete
- 14. Minimum diameter for individual service connections (PVC DR 28): 100 mm (4") w/ min grade 1% (preferred 2%)
- 15. Use tees or wyes, strap-on-saddles for connections to main sewer

Manning's n = 0.013





EXISTING CULVERT

		C		ERT SCHEDU	ILE		
D	DIA (mm)	LENGTH (m)	SLOPE	MATERIAL	INV. IN	INV. OUT	COVER (m)
C1	450	9.1	-0.50%	REINFORCED CONCRETE	83.87	83.92	0.50 m
22	450	13.5	2.06%	REINFORCED CONCRETE	83.32	83.04	0.40 m
23	600	14.5	5.00%	REINFORCED CONCRETE	80.11	79.39	0.95 m

IANHOLE	DETAILS	HEIGHT (m)
102	RIM = 84.44 SUMP = 82.00 INV IN = 82.00 INV OUT = 82.94	RIM TO SUMP = 2.44
104	RIM = 84.57 SUMP = 82.34 INV IN = 82.36 INV OUT = 82.34	RIM TO SUMP = 2.23
106	RIM = 84.56 SUMP = 82.15 INV IN = 82.18 INV OUT = 82.15	RIM TO SUMP = 2.41
108	RIM = 84.32 SUMP = 81.57 INV IN = 81.59 INV OUT = 81.57	RIM TO SUMP = 2.75
110	RIM = 84.01 SUMP = 81.14 INV IN = 81.16 INV OUT = 81.14	RIM TO SUMP = 2.88
112	RIM = 83.79 SUMP = 80.83 INV IN = 80.85 INV OUT = 80.83	RIM TO SUMP = 2.97
114	RIM = 83.53 SUMP = 80.56 INV IN = 80.58 INV OUT = 80.56	RIM TO SUMP = 2.97
116	RIM = 82.70 SUMP = 79.95 INV IN = 79.97 INV OUT = 79.95	RIM TO SUMP = 2.75
118	RIM = 81.95 SUMP = 78.95 INV IN = 79.00 INV IN = 79.00 INV OUT = 78.95	RIM TO SUMP = 3.00
122	RIM = 84.28 SUMP = 82.14 INV OUT = 82.14	RIM TO SUMP = 2.14
124	RIM = 84.20 SUMP = 81.87 INV IN = 81.89 INV OUT = 81.87	RIM TO SUMP = 2.33
126	RIM = 83.83 SUMP = 81.17 INV IN = 81.19 INV OUT = 81.17	RIM TO SUMP = 2.66
128	RIM = 83.46 SUMP = 80.65 INV IN = 80.68 INV OUT = 80.65	RIM TO SUMP = 2.81
130	RIM = 83.05 SUMP = 80.11 INV IN = 80.18 INV IN = 80.18 INV OUT = 80.11	RIM TO SUMP = 2.94
132	RIM = 82.66 SUMP = 79.75 INV IN = 79.77 INV OUT = 79.75	RIM TO SUMP = 2.91
134	RIM = 82.42 SUMP = 79.41 INV IN = 79.46 INV IN = 79.43 INV OUT = 79.41	RIM TO SUMP = 3.01
136	RIM = 83.38 SUMP = 81.09	RIM TO SUMP = 2.29

0 _{5.0} 10 20 1:500 _____ Metres

STREET NAMES:

PART OF LOT 7, CONCESSION 1

TOPOGRAPHIC INFORMATION

GEOTECHNICAL REPORT

USE AND INTERPRETATION OF DRAWINGS

CONSTRUCTION DOCUMENT.

COUNTY OF GRENVILLE

ELEVATIONS:

NETWORK.

CONCLUSIONS.

		STORM MANHO	DLE TABLE			
MANHOLE	ELEVATIONS	HEIGHT (m)	INNER DIA. (mm)	TYPE	DETAILS	MAX. HGL (m)
101	RIM = 84.38 ; SUMP = 82.43 INV OUT (NE)= 82.73	RIM TO SUMP = 1.95	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.87
103	RIM = 84.52 ; SUMP = 82.15 INV IN (SW)= 82.48 INV OUT (N)= 82.45	RIM TO SUMP = 2.37	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.60
105	RIM = 84.51 ; SUMP = 81.90 INV IN (S)= 82.37 INV OUT (NW)= 82.20	RIM TO SUMP = 2.61	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.43
107	RIM = 84.29 ; SUMP = 81.70 INV IN (SE)= 82.03 INV IN (E)= 82.89 INV OUT (N)= 82.00	RIM TO SUMP = 2.59	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.23
109	$\begin{array}{rcl} RIM &=& 83.95 \hspace{0.1cm} ; \hspace{0.1cm} SUMP \hspace{0.1cm} = \hspace{0.1cm} 81.19 \\ & INV \hspace{0.1cm} IN \hspace{0.1cm} (S) \hspace{0.1cm} = \hspace{0.1cm} 81.58 \\ & INV \hspace{0.1cm} IN \hspace{0.1cm} (E) \hspace{0.1cm} = \hspace{0.1cm} 82.56 \\ & INV \hspace{0.1cm} IN \hspace{0.1cm} (SW) \hspace{0.1cm} = \hspace{0.1cm} 82.51 \\ & INV \hspace{0.1cm} OUT \hspace{0.1cm} (N) \hspace{0.1cm} = \hspace{0.1cm} 81.49 \end{array}$	RIM TO SUMP = 2.76	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.87
111	RIM = 83.74 ; SUMP = 80.96 INV IN (S)= 81.36 INV OUT (NW)= 81.26	RIM TO SUMP = 2.78	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.71
113	RIM = 83.47 ; SUMP = 80.80 INV IN (SE)= 81.13 INV IN (NE)= 81.58 INV OUT (NW)= 81.10	RIM TO SUMP = 2.67	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.65
115	RIM = 82.77 ; SUMP = 80.26 INV IN (SE)= 80.66 INV IN (E)= 81.27 INV IN (SW)= 81.21 INV IN (NE)= 81.05 INV OUT (NW)= 80.56	RIM TO SUMP = 2.51	1350	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.54
117	RIM = 81.90 ; SUMP = 79.48 INV IN (SE)= 80.03 INV IN (SW)= 80.06 INV IN (E)= 80.38 INV IN (NE)= 80.50 INV OUT (NW)= 79.78	RIM TO SUMP = 2.42	1800	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.41
119 STC	RIM = 81.30 ; SUMP = 79.40 INV IN (SE)= 79.70 INV OUT (NW)= 79.70	RIM TO SUMP = 1.90	2550	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.35
121	RIM = 84.23 ; SUMP = 82.05 INV OUT (W)= 82.35	RIM TO SUMP = 2.17	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.35
123	RIM = 84.15 ; SUMP = 81.86 INV IN (E)= 82.26 INV OUT (NW)= 82.16	RIM TO SUMP = 2.29	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.38
125	RIM = 83.77 ; SUMP = 81.55 INV IN (SE)= 81.95 INV OUT (NW)= 81.85	RIM TO SUMP = 2.22	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.13
127	RIM = 83.41 ; SUMP = 81.20 INV IN (SE)= 81.64 INV OUT (NW)= 81.50	RIM TO SUMP = 2.21	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.78
129	RIM = 83.00 ; SUMP = 80.87 INV IN (SE)= 81.27 INV IN (NE)= 81.23 INV IN (SW)= 81.61 INV OUT (NW)= 81.17	RIM TO SUMP = 2.13	1500	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.63
131	RIM = 82.62 ; SUMP = 80.52 INV IN (SE)= 80.89 INV IN (E)= 81.18 INV IN (S)= 81.24 INV OUT (NW)= 80.82	RIM TO SUMP = 2.10	1500	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.56
133	RIM = 82.38 ; SUMP = 80.25 INV IN (SE)= 80.61 INV IN (W)= 81.51 INV OUT (NE)= 80.55	RIM TO SUMP = 2.13	1800	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.51
135	RIM = 83.35 ; SUMP = 81.31 INV OUT (SW)= 81.61	RIM TO SUMP = 2.04	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.45

PLANS UPDATE- ELEVATIONS CHANGE TOWNSHIP COMMENTS - 06-30-23 TOWNSHIP COMMENTS TOWNSHIP COMMENTS PEER REVIEW COMMENTS - ADD STM SEWER OWNER / APPROVAL REVISION / ISSUE PARED BY: ongi Mabrouk P.Eng. one: 613-896-9170 nail: eng.services.ca@gmail.com ADVANCE ENGINEERING

OJECT NAME AND ADDRESS:

LOCKMASTER'S **MEADOW SUBDIVISION**

DUNTY ROAD No. 22 (SHANLY RD), CARDINAL, ON

LICANT:

vardsburgh Developments Ltd. 4-300 Earl Grey Drive nata, ON -282-5601

GENERAL SERVICES PLAN PHASE 1 DRAWING No .: 1:500 TED BY: JECT No.: 0114 DATE:

02-06-2024





MH-140		ID	
T/G=84.32 INV. S=82.42		3	Т/
INV. N=82.45 INV. E=82.45		4	т/
		5	Т/
		6	Т/(
		7	т/
BLOCK Da		8	Т/(
		9	т/
		10	т/
9) (10)		11	T/O
		12	т/(
		13	т/
		14	т/
1.6 • 0.32%		15	т/
™STM svisNNSANS (112)		16	Т/(
200Ø PVC SAN 11 41.2 @ 0.60% EL		17	Т/
		18	т/
95			
		ID	
	S-1	19	т/(
	NG S	20	Т/(
93		21	т/
	ER	22	Т/(
	REF	23	т/(
92		24	т/(
		25	т/(
(91)		26	т/(
		27	Т/(
		28	Т/(
		29	т/(
VC SAN /2.5 @ 0.65% → → → → → → → → → → → → → → → → → → →		30	Т/(
525¢ CONC STM		31	Т/
		32	т/(
36 35			

36			35	
<u>-xxxx-</u> 10"W	X	xx	—×—>	<u>x</u> 15

	CATCHBASIN /	CATCHBASIN-N	IANHOLE T	ABLE	
ID	ELEVATIONS	HEIGHT (m)	TYPE	DETAILS	ICD DIA (mm)
3	T/G = 84.24 ; SUMP = 82.33 INV OUT (W)= 82.93	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
4	T/G = 84.24 ; SUMP = 82.33 INV OUT (NE)= 82.93	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
5	T/G = 83.90 ; SUMP = 82.00 INV OUT (W)= 82.60	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
6	T/G = 83.91 ; SUMP = 82.00 INV OUT (NE)= 82.60	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
7	T/G = 83.50 ; SUMP = 81.59 INV OUT (SW)= 82.19	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
8	T/G = 83.46 ; SUMP = 81.55 INV OUT (NE)= 82.15	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
9	T/G = 83.49 ; SUMP = 81.58 INV OUT (NW)= 82.18	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	55
10	T/G = 83.46 ; SUMP = 81.20 INV IN (SE)= 82.05 INV OUT (SW)= 81.80	RIM TO SUMP = 2.26	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	55
11	T/G = 84.14 ; SUMP = 82.23 INV OUT (SW)= 82.83	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
12	T/G = 84.11 ; SUMP = 82.20 INV OUT (NE)= 82.80	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
13	T/G = 83.56 ; SUMP = 81.65 INV OUT (SW)= 82.25	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
14	T/G = 83.57 ; SUMP = 81.66 INV OUT (NE)= 82.26	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
15	T/G = 82.98 ; SUMP = 81.07 INV OUT (SW)= 81.67	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
16	T/G = 82.95 ; SUMP = 81.04 INV OUT (NE)= 81.64	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
17	T/G = 82.93 ; SUMP = 81.02 INV OUT (NW)= 81.62	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
18	T/G = 82.89 ; SUMP = 80.99 INV OUT (SE)= 81.59	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
			-		

CATCHBASIN /	CATCHBASIN-N	IANHOLE T	ABLE	
ELEVATIONS	HEIGHT (m)	TYPE	DETAILS	ICD DIA (mm)
T/G = 82.61 ; SUMP = 80.70 INV OUT (W)= 81.30	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 82.61 ; SUMP = 80.70 INV OUT (NE)= 81.30	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 81.86 ; SUMP = 79.95 INV OUT (SW)= 80.55	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 81.86 ; SUMP = 79.95 INV OUT (NE)= 80.55	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 82.58 ; SUMP = 80.67 INV OUT (W)= 81.27	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 82.58; SUMP = 80.68 INV OUT (N)= 81.28	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 82.26 ; SUMP = 80.68 INV OUT (SW)= 81.28	RIM TO SUMP = 1.59	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 82.26 ; SUMP = 80.66 INV OUT (NE)= 81.24	RIM TO SUMP = 1.60	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 81.85 ; SUMP = 79.95 INV OUT (W)= 80.55	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	83
T/G = 81.86 ; SUMP = 79.96 INV OUT (SW)= 80.56	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	55
T/G = 81.86 ; SUMP = 79.95 INV OUT (NW)= 80.55	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	102
T/G = 81.88 ; SUMP = 79.97 INV OUT (SE)= 80.57	RIM TO SUMP = 1.91	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	102
T/G = 82.77 ; SUMP = 81.27 INV OUT (NW)= 81.87	RIM TO SUMP = 1.50	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	55
T/G = 82.79; SUMP = 81.10 INV IN (SE)= 81.74 INV OUT (E)= 81.70	RIM TO SUMP = 1.69	OPSD 705.010	GRATE: 400.010 SUMP: 0.600 m	55

CATCHBASIN / CATCHBASIN-MANHOLE TABLE

ID	ELEVATIONS	HEIGHT (m)	TYPE	DETAILS	ICD DIA (mm)
RYCB1	T/G = 83.47 ; SUMP = 82.76 INV OUT (NW)= 83.06	RIM TO SUMP = 0.71	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	152
RYCB2	T/G = 84.62 ; SUMP = 82.64 INV IN (SE)= 83.00 INV IN (NW)= 83.10 INV OUT (SW)= 82.94	RIM TO SUMP = 1.98	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	83
RYCB3	T/G = 84.02 ; SUMP = 82.56 INV IN (SE)= 82.86 INV OUT (NE)= 82.86	RIM TO SUMP = 1.46	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	83
RYCB4	T/G = 83.95 ; SUMP = 82.34 INV IN (SE)= 82.64 INV OUT (NE)= 82.64	RIM TO SUMP = 1.61	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	83
RYCB5	T/G = 83.27 ; SUMP = 82.08 INV OUT (NE)= 82.38	RIM TO SUMP = 1.19	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	83
RYCB6	T/G = 84.50 ; SUMP = 82.82 INV OUT (NE)= 83.12	RIM TO SUMP = 1.68	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	83
RYCB8	T/G = 83.97 ; SUMP = 82.43 INV OUT (NE)= 82.73	RIM TO SUMP = 1.54	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	55
RYCB9	T/G = 82.57 ; SUMP = 81.17 INV IN (NW)= 81.47 INV OUT (SW)= 81.47	RIM TO SUMP = 1.40	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	83
RYCB10	T/G = 82.70 ; SUMP = 81.41 INV OUT (NE)= 81.71	RIM TO SUMP = 1.29	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	83
RYCB11	T/G = 82.38 ; SUMP = 81.37 INV OUT (NE)= 81.67	RIM TO SUMP = 1.01	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	127
RYCB12	T/G = 82.50 ; SUMP = 81.59 INV OUT (NE)= 81.89	RIM TO SUMP = 0.91	OPSD 705.010	GRATE: 400.020 SUMP: 0.300 m	83

PART OF LOT 7, CONCESSION 1 COUNTY OF GRENVILLE

ELEVATIONS: ŇETWORK.

CONCLUSIONS. USE AND INTERPRETATION OF DRAWINGS



8	PLANS UPDATE- ELEVATIONS CHANGE
6	TOWNSHIP COMMENTS - 06-30-23
5	TOWNSHIP COMMENTS
4	TOWNSHIP COMMENTS
3	PEER REVIEW COMMENTS - ADD STM SE
1	OWNER / APPROVAL
No.	REVISION / ISSUE
PREP	ARED BY:
Mo Phc Ema	ngi Mabrouk P.Eng. one: 613-896-9170 ail: eng.services.ca@gmail.com



434-300 Earl Grey Drive Kanata, ON 613-282-5601







STREET A PROFILE STA. 0+000 TO STA. 0+170 SCALE: H = 1:500 / V = 1:50

SANITAR	Y MANHOLE TABLE - INNER	DIAMETER = 1200mm
MANHOLE	DETAILS	HEIGHT (m)
102	RIM = 84.44 SUMP = 82.00 INV IN = 82.00 INV OUT = 82.94	RIM TO SUMP = 2.44
104	RIM = 84.57 SUMP = 82.34 INV IN = 82.36 INV OUT = 82.34	RIM TO SUMP = 2.23
106	RIM = 84.56 SUMP = 82.15 INV IN = 82.18 INV OUT = 82.15	RIM TO SUMP = 2.41
108	RIM = 84.32 SUMP = 81.57 INV IN = 81.59 INV OUT = 81.57	RIM TO SUMP = 2.75
110	RIM = 84.01 SUMP = 81.14 INV IN = 81.16 INV OUT = 81.14	RIM TO SUMP = 2.88
112	RIM = 83.79 SUMP = 80.83 INV IN = 80.85 INV OUT = 80.83	RIM TO SUMP = 2.97
114	RIM = 83.53 SUMP = 80.56 INV IN = 80.58 INV OUT = 80.56	RIM TO SUMP = 2.97
116	RIM = 82.70 SUMP = 79.95 INV IN = 79.97 INV OUT = 79.95	RIM TO SUMP = 2.75
118	RIM = 81.95 SUMP = 78.95 INV IN = 79.00 INV IN = 79.00 INV OUT = 78.95	RIM TO SUMP = 3.00
122	RIM = 84.28 SUMP = 82.14 INV OUT = 82.14	RIM TO SUMP = 2.14
124	RIM = 84.20 SUMP = 81.87 INV IN = 81.89 INV OUT = 81.87	RIM TO SUMP = 2.33
126	RIM = 83.83 SUMP = 81.17 INV IN = 81.19 INV OUT = 81.17	RIM TO SUMP = 2.66
128	RIM = 83.46 SUMP = 80.65 INV IN = 80.68 INV OUT = 80.65	RIM TO SUMP = 2.81
130	RIM = 83.05 SUMP = 80.11 INV IN = 80.18 INV IN = 80.18 INV OUT = 80.11	RIM TO SUMP = 2.94
132	RIM = 82.66 SUMP = 79.75 INV IN = 79.77 INV OUT = 79.75	RIM TO SUMP = 2.91
134	RIM = 82.42 SUMP = 79.41 INV IN = 79.46 INV IN = 79.43 INV OUT = 79.41	RIM TO SUMP = 3.01
136	RIM = 83.38 SUMP = 81.09 INV OUT = 81.09	RIM TO SUMP = 2.29

Ø		DODGE ST	CILL ST	
	COUNTY ROAD	No. 22		
	000000		0 0 0	EXISTING
		┰╺╦╦╤╋╇╲╷╷╭╼┺╴		0000
© (0000
© ©			- ° ° ° ° °	PHASE I Image: Image of the second
©	STREET "B"	·		<u>STREET_"B"</u>
PARK	000000	0 0 0 0	0 0 0 0 0	0 0 0 0
		V	ACANT LAND (RUR	RAL)

1.200	0 ⊢	5.0	10	2
1:50	0 	0.5	1	

		STORM MANHO	DLE TABLE			
MANHOLE	ELEVATIONS	HEIGHT (m)	INNER DIA. (mm)	TYPE	DETAILS	MAX. HGL (m)
101	RIM = 84.38 ; SUMP = 82.43 INV OUT (NE)= 82.73	RIM TO SUMP = 1.95	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.87
103	RIM = 84.52 ; SUMP = 82.15 INV IN (SW)= 82.48 INV OUT (N)= 82.45	RIM TO SUMP = 2.37	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.60
105	RIM = 84.51 ; SUMP = 81.90 INV IN (S)= 82.37 INV OUT (NW)= 82.20	RIM TO SUMP = 2.61	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.43
107	RIM = 84.29 ; SUMP = 81.70 INV IN (SE)= 82.03 INV IN (E)= 82.89 INV OUT (N)= 82.00	RIM TO SUMP = 2.59	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.23
109	$\begin{array}{llllllllllllllllllllllllllllllllllll$	RIM TO SUMP = 2.76	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.87
111	RIM = 83.74 ; SUMP = 80.96 INV IN (S)= 81.36 INV OUT (NW)= 81.26	RIM TO SUMP = 2.78	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.71
113	RIM = 83.47 ; SUMP = 80.80 INV IN (SE)= 81.13 INV IN (NE)= 81.58 INV OUT (NW)= 81.10	RIM TO SUMP = 2.67	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.65
115	RIM = 82.77 ; SUMP = 80.26 INV IN (SE)= 80.66 INV IN (E)= 81.27 INV IN (SW)= 81.21 INV IN (NE)= 81.05 INV OUT (NW)= 80.56	RIM TO SUMP = 2.51	1350	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.54
117	RIM = 81.90 ; SUMP = 79.48 INV IN (SE)= 80.03 INV IN (SW)= 80.06 INV IN (E)= 80.38 INV IN (NE)= 80.50 INV OUT (NW)= 79.78	RIM TO SUMP = 2.42	1800	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.41
119 STC	RIM = 81.30 ; SUMP = 79.40 INV IN (SE)= 79.70 INV OUT (NW)= 79.70	RIM TO SUMP = 1.90	2550	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.35
121	RIM = 84.23 ; SUMP = 82.05 INV OUT (W)= 82.35	RIM TO SUMP = 2.17	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.35
123	RIM = 84.15 ; SUMP = 81.86 INV IN (E)= 82.26 INV OUT (NW)= 82.16	RIM TO SUMP = 2.29	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.38
125	RIM = 83.77 ; SUMP = 81.55 INV IN (SE)= 81.95 INV OUT (NW)= 81.85	RIM TO SUMP = 2.22	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	82.13
127	RIM = 83.41 ; SUMP = 81.20 INV IN (SE)= 81.64 INV OUT (NW)= 81.50	RIM TO SUMP = 2.21	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.78
129	RIM = 83.00 ; SUMP = 80.87 INV IN (SE)= 81.27 INV IN (NE)= 81.23 INV IN (SW)= 81.61 INV OUT (NW)= 81.17	RIM TO SUMP = 2.13	1500	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.63
131	RIM = 82.62 ; SUMP = 80.52 INV IN (SE)= 80.89 INV IN (E)= 81.18 INV IN (S)= 81.24 INV OUT (NW)= 80.82	RIM TO SUMP = 2.10	1500	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.56
133	RIM = 82.38 ; SUMP = 80.25 INV IN (SE)= 80.61 INV IN (W)= 81.51 INV OUT (NE)= 80.55	RIM TO SUMP = 2.13	1800	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.51
135	RIM = 83.35 ; SUMP = 81.31 INV OUT (SW)= 81.61	RIM TO SUMP = 2.04	1200	OPSD 701.010	COVER: 401.010 SUMP: 0.300 m	81.45



8	PLANS UPDATE- ELEVATIONS CHANGE
6	TOWNSHIP COMMENTS - 06-30-23
5	TOWNSHIP COMMENTS
4	TOWNSHIP COMMENTS
3	PEER REVIEW COMMENTS - ADD STM SEV
1	OWNER / APPROVAL
No.	REVISION / ISSUE
PREP	ARED BY:
Mo Pho Ema	ngi Mabrouk P.Eng. one: 613-896-9170 ail: eng.services.ca@gmail.com ADVANCE ENGINEERING
N co	LOCKMASTI IEADOW SUBE
	CARDINAL, C
APPL	ICANT:
Edw 434- Kan 613-	ardsburgh Developments Ltd. 300 Earl Grey Drive ata, ON 282-5601

PLAN & I	PR
STRE	EET
STA. 0+000 T	O ST
SCALE: 1:500-1:50	DRAWING

PROJECT No.: 0114









TOWNSHIP COMMENTS	
TOWNSHIP COMMENTS	
PEER REVIEW COMMENTS - ADD S	stm se
OWNER / APPROVAL	
REVISION / ISSUE	
ARED BY:	
ngi Mabrouk P.Eng. one: 613-896-9170 ail: eng.services.ca@gmail.c	om
ADVANCE ENGINEERING	REGISTER
	TOWNSHIP COMMENTS TOWNSHIP COMMENTS PEER REVIEW COMMENTS - ADD S OWNER / APPROVAL REVISION / ISSUE ARED BY: ngi Mabrouk P.Eng. one: 613-896-9170 ail: eng.services.ca@gmail.c

Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata, ON 613-282-5601

.AN	&	PR
ST	R	EET

SCALE:	[
1.500-1.50	
DRAFTED BY:	
PROJECT No .:	
0114	
DATE:	
00 06 0001	

R	OAD STRUCTURE					K = 41.199 A = -1.09%		-
ACE AND mm – GR IULAR B 1	75mm HL3 BINDER COURSE) ANULAR A BASE TYPE II SUBBASE			20 27 0 27 20 27 20 27 20 20 20 20 20 20 20 20 20 20 20 20 20	VCE: 84.55	4.51	84.52 14.57 ◀	- 86
)		/6: 84:29 108 1/6: 84.32		÷ Š		1/G: 8, 1/G: 8, 1/G: 8, 1/G: 8, 1/G: 9	103 1/G: 8 104 1/G: 8	- 85
		рания 	266 0CK			200	 TOPSOL	
			ELEV=\$1.9	RYCB6 LEAD 250mmø @ 1.5% INV= 82.54				- 84
	IN. 2.40r M COVEF		3+21.59 E	/ RYCB2 LEAD 250mmø @ 1.5% INV= 82.38			-CLAYED SILT	- 83
a <u>0.62</u> 9	≥ ≥ 		STA =		30% STM			
50-DR-18.	WM.	5	6.0m-200mm @ 1.00% SA	ø	13.1m-200 @ 1.20%	Dmmø_		VATION
)mmø SAN						 4	SAND AND GRAVEL TILL	
						1 · ·		- 80
								-
								- 79
								- 78
								-
								+ 77
			+0+325		+0+350			
84,66	84.19 84.78	84.32	84.79	84.44	84.51 84.56		84.45	84.59
01 70		ୟ1.୪6 	81.97		82.09		82.12	- - - - -
		1	+					
		02.36-			[58.08- Reet B)	70.64- Reet B)	-
0.65%		1.57 <u>3</u> 1.59 (sī		1.00%		2.18 2.18 5.18 5.18	2.34 (ST	
I.30 - ЕТ В)			2.20 - EET B)			4 7 82 7 82 82 82	.36 .94	
27 . (STRE	C	03 - 130 (STRE	322 (STRE	0.30%		1.6 1.6 20 21 20 20 20	45 37(STR	-
	C 0	82				82.	82.48	-
1	8	;2.23 		1	-	82.43	82873.60 0.65%	-
50%					CU	IRVE LENGTH=4 K= 41.199 HP STA.= 0+30 EL.= 84.60	-5.00m 67.4	
	L=41.61m - R=150 DELTA = 15.895			1 = 3750m		L=23.56m - DELTA = 9	R=15.00m 90.0000	1
	PI LASTING= 469194 PI NORTHING= 495975	i5.3007		2-07.02111	F	PI NORTHING=	4959692.1064	

PVI STA:0+369.53 PVI ELEV:84.66









STREET B PROFILE STA. 0+670 TO STA. 0+796 SCALE: H = 1:500 / V = 1:50







	C	OUN	TY	RO	 No. 2	22		NDGE SU	4					GILLSI	l.				, ,	
Image: State of the state of t		©			O B B B B B B B B B B B B B B B B B B B		© L STREET "A"				© 0	0					STII © E © REE	NG	RI 0 0 0 0	
					 				V	AC	'AN'	ΓL	AN) (R	UR	AL)	 			



75.5 @ 1.26% 75.9 🔮 0.70% 2









BH-7

		CHAINA
€ RO/ Existing	ADE ;/	ELEVATION PROPOSI
TOP	OF	WATERMA

SCALE: H = 1:500 / V = 1:50









COUNTY ROAD No. 22 (SHANLY RD), CARDINAL, ON

APPLICANT:

Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata, ON 613-282-5601



PATHWAY 1 PROFILE STA. 0+000 TO STA. 0+078













Ø								DOPO							2						
			OUNTY	RO	AD N	No. 2	22)/\ 	57J			1								<u>`</u>	_
	╞╸╤╺┥╺ │			6	-					5 -	6	╞╺		, 		_	EXI	ISTII	NG	RI	ES
				<u>STR</u>	<u>EET</u>	<u>"В"</u> нн	 + + -				 			4	◎ / /	/•	0	0	ø	0	Ĺ
© 		0	00	۲	SE 2 ©	SE 1	0 0 0	- _ _ _		0	e e) @	°	0	0			0			
0 0	STREET	o P I	H A S H	°	© PHA	Hd J	0 0 0	STREET		0 0) @		0	0	PH ©	AS Ø	E	1 ©	0	
0	`	. – . –	STR	EET	"B"		+++			+ -	•						<u>_\$T</u>]	RĘE	<u>T_'</u> B	<u> </u>	
PARK		9 0	00	0	6	0	•	0	©		»	0	@	» (© (• •	٥	ø	۲	۲	
										VA	CA	NT	LAI	ND (RUR	AL)					



Township of Edwardsburgh/Cardinal



PROJECT: LOCKMASTER'S MEADOW SUBDIVISION (95 Single Family Lots)

ADDRESS: COUNTY ROAD 22 (SHANLY ROAD) CARDINAL, ON

WASTEWATER PUMPING STATION & FORCEMAIN DESIGN REPORT

PREPARED FOR: Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata, Ontario K2T 1C1 (613) 282 5601

> PREPARED BY: Advance Engineering Ltd. (613) 986 9170

Date	Revision / Issue
April 15, 2024	Comments by Township Dated April 12, 2024
December 06, 2023	Concrete Wet Well Instead of FRP
July 27, 2022	Issued for a Subdivision Application

TABLE OF CONTENTS

1
1
1
1
2
2
2
4
4
6
6

List of Appendices:

Appendix A - Figure 1 – Pump station layout Appendix B- Wet well and pumps design calculation Proposed wet well, pump and generator details

List of Related Drawings:

S-1 – Draft Plan of Subdivision GSP2 - General Services Plan GR-2 - Grading and Drainage Plan CUP 1,2&3 – Composite Utility Plan <u>Pumping Station Plans:</u> CS-1, PS-1, PS-2, PS-3, PS-4, A-1, M-1 and E-1

Related Report:

- Site Servicing Report
- Stormwater Management Report



1.0 INTRODUCTION

Edwardsburgh Developments Ltd. has retained *Advance Engineering Ltd.* to provide a design report for a new wastewater pumping station and a forcemain to be constructed to service a proposed residential subdivision composed of 95 single-detached lots located off County Rd 22 in the Village of Cardinal, Ontario. *Ottawa Sewer Design Guidelines* has been used in the design of the forcemain, pumping station and associated appurtenances and controls.

The proposed development, as shown in the draft plan of subdivision, consists of:

- Phase 1: 59 lots in the south side of the property.
- Phase 2: the remaining 36 lots in the north side of the subdivision.

The pumping station is required for both phases. It is located in "Block B" at the north side of the site.

The equipment installed in the Village other pumping stations has been taken in consideration in the design of the new pumping station with the goal of harmony and reducing operation and maintenance costs.

1.1 EXISTING INFRASTRUCTURE

Existing municipal sewer: There is a manhole (MH-135) located at the intersection of County Rd 22 and Gill St. From it, a 250 mm dia. PVC DR 35 pipe runs south along County Road 22 and a 250 mm dia. pipe, sloped at 0.94 %, runs east along Gill St. The south and east invert elevations at MH-135 are 82.72 m and 82.11 m respectively. The capacity of Gill St sewer is estimated at 58 L/s using Manning's Formula. There is a second manhole (MH-140) at the intersection of County Rd 22 and Dodge St to which are connected two pipes: a 200 mm dia. pipe coming from Dodge St and a 250 mm dia. pipe sloped at 0.28% running south toward MH-135. The south invert elevation is 82.42 m and the full capacity of the sewer is estimated at 31 L/s. Two 200 mm dia. capped end pipes are connected to MH-140; one is directed north along the road and the other west adjacent to the site. Wastewater from MH-135 and MH-140 flows south through Walker St to Adelaide St pumping station.

1.2 REASON FOR PUMPING STATION

Due to insufficient elevation for a gravity-based-system sewer, an underground sewage pumping station, designed for continuous operation, is proposed downstream of the property.

A pressurized forcemain will be constructed to discharge sewage effluent from the pumping station into the existing municipal sewer within County Rd 22 as shown in the servicing plans.

The sanitary sewer within the site is designed to operate under free flow condition for both phases. County Rd pavement elevation at the proposed forcemain connection is 84.12 approximately. The finished grade elevation at the pumping station wet well is 82.20.

2.0 PROPOSED WET WELL SUBMERSIBLE STATION

The proposed pumping station consist of a wet well equipped with two submersible pumps interchangeable of the same pumping capacity and each unit, operating independently, is capable of pumping at the design peak flow rate.



2.1 REQUIREMENTS

In addition to meeting the requirements of *Ottawa Sewer Design Guidelines*, the design and construction of the wastewater pumping facility must meet all the current requirements of other governmental authorities having jurisdiction, including, but not limited to, the following:

- Ontario Ministry of the Environment, Conservation and Parks
- Ontario Ministry of Labour
 - i. Occupational Health and Safety Branch
 - ii. Workplace Hazardous Materials Information System (WHMIS)
- Ontario Ministry of Municipal Affairs and Housing
 - i. Ontario Building Code
 - ii. Ontario Plumbing Code
- Ontario Gas Code
- Ontario Electrical Safety Code

Testing and commissioning plan and procedures shall be approved by the Township of Edwardsburgh/Cardinal.

2.2 DESIGN CRITERIA

2.2.1 ANTICIPATED FLOWS

- Design period: 50-year design life period for the facility structure. The pumping equipment is assumed to receive a major overhaul, involving renewal of the wearing components, at 10 year intervals or a replacement every 15 years, dependent on service conditions.
- Station design flows targets: the station is designed to handle the peak sewage flows for a 20year development period.
- A future 5 ha hectare development has been included in the estimation of the various flows.
- Firm capacity requirement: the station must be able to pump the expected peak design flow with the largest pump out of operation.
- Using 10-year development intervals up to build-out condition, typical anticipated sanitary sewage flows, including infiltration and extraneous flow allowances are estimated as follows:



STAGING	INITIAL 2024	10 YEAR 2034	20 YEAR 2044	BUILD-OUT
DEVELOPMENT	100 % OF FLOW OF EDWARDSBURGH DEVELOPMENT	100 % OF FLOW EDWARDSBURGH DEVELOPMENT	100 % OF FLOW EDWARDSBURGH DEV. + FUTURE DEVELOP. (5 ha)	ULTIMATE DE- VELOPMENTS MAX CAPACITY
AWF (L/s)	1.31	1.31	2.52	2.52
ADWF (L/s)	1.69	1.69	3.16	3.16
PDWF (L/s)	4.90	4.90	9.34	9.34
WWF (L/s)	7.04	7.04	12.89	12.89
AWWF (L/s)	4.09	4.09	7.26	7.26
RWWF (L/s)	6.01	6.01	10.43	10.43

Table 1: SUMMARY OF PROJECTED DESIGN FLOWS BASED

ON ANTICIPATED DEVELOPMENT STAGING

- AWF: Average Wastewater Flow Rate.
- ADWF: Average Dry Weather Flow Rate.
- PDWF: Peak Dry Weather Flow Rate.
- WWF: Peak Wet Weather Design Flow Rate Q_d.
- AWWF: Annual Wet Weather Flow.
- RWWF: Rare Wet Weather Flow.

The values of residential wastewater design flows are provided in Table 1 in *Ottawa Guidelines*. However, *Technical Bulletin ISTB-2018-01* has reduced the average residential flow from 350 to 280 L/c/day. For a conservative estimate we have used: 350 L/c/day, 4 for M and a correction factor of 1. Wet weather and dry weather infiltration contribution (extraneous) are respectively 0.28 and 0.05 L/s/effective gross ha.

The above-listed flow ranges of projected average, peak, and minimum daily dry weather flow, related to anticipated developments has been used to provide design guidance to address operational issues including:

- i. Wastewater detention times, forcemain velocities, odour and corrosion potential: average DWF.
- ii. Typical pumping requirements: average and peak DWF.
- iii. Firm capacity requirements for various stages of development: peak WWF.
- iv. Realistic emergency pumping requirements: annual WWF or peak WWF for rare event.

2.2.2 PUMPING SYSTEM DESIGN

- Pump type: *Flygt.*
- Number of pumps: 2 (one duty, one stand-by).
- Pump power: less than 5 kW.
- Pumps rated at: 16 L/s.
- Total Dynamic Headloss (TDH): 9.2 m.
- Net positive suction head (NPSH) required: as per manufacturer's specifications.
- Operating depth: 0.50 m.
- Number of pump starts per hour: maximum 30.
- Hazen-Williams C-V for internal piping and forcemain: as per Table 7.3 Ottawa Guidelines.
- Pump motor: 3-phase, 1745 RPM, 60 Hz.
- Pump impellers: shall be of a non-clog design and be capable of passing spherical solids of 75 mm diameter.
- Pump cycling: T= V/(Q-Qin) + V/Qin

T = Time between pump starts (minutes)

V = Effective wet well volume (Litres) between lead pump start and lead pump stop

Q = Pump/station discharge capacity (L/minute), and,

Qin = Station inflow rate (L/minute)

2.2.3 WET WELL DESIGN

- Wet well cross-sectional area: 4.52 m² (2.4 m diameter) using D-65 reinforced concrete pipes.
- Wet well retention time: maximum 30 minutes. Proposed 24.4 min for average DWF of 1.69 L/s.
- Wet well and forcemain total retention time: maximum 4 hours.
- Wet well operating levels: 0.50 m.
- Wet well benching: wet well floors shall have a minimum slope of 1:1 to a hopper-type bottom.
- Height of wet well: 5.0 m.
- Total wet well volume: 22.6 m³.
- Precast concrete material.
- Inlet sewer diameter: 200 mm.
- Top wet well elevation: 82.40.
- Bottom wet well elevation: 77.10.
- Inlet sewer elevation: 78.75.
- High liquid level inside wet well: 77.90.
- Low liquid level inside wet well: 77.40.

- Outlet forcemain elevation: 80.10.
- Lowest basement elevation: 81.00,
- Corrosion Consideration: epoxy coating, aluminum, ductile iron and stainless steel.
- Vortex prevention: provided.
- Personnel opening to the wet well: minimum 0.90 x 0.75 m. The opening should give access to level controls, floats, equipment, etc.
- Access hatches and stairways: access hatch cover for all roof openings to wet well must be sealed or have sufficient overhang to prevent rainwater inflow. Equipment hatch floor openings shall be adequately sized for all intended uses. Access hatch to the pump, when open, must be protected by posts and surrounding chains. Doors and access hatches shall have suitable locking devices. Odour-tight aluminum hatch covers should be used. Non-protruding extension ladders are to be provided for entry hatch, and must be located far enough away from the walls to be able to be pulled up through the access opening and extended to a height of at least 1.0 m above the roof.
- Wet well submersible station valve vault design: a separate by-pass chamber shall house the pump check valves, surge relief valves, flow meter, force main isolating valve, bypass valve, and associated piping.
- Wet wells safety considerations: typically classified as Class I, Group D, Division I (Zone 1), or Division II (Zone 2) Hazardous Locations.
- Air Monitoring System inside the wet well: no continuous monitoring provided; the Township will use portable devises to detect the presence of gases before and during entries.
- Ventilation: natural venting. To be achieved through two 100 mm diameter vent pipes equipped with a gooseneck at the top, extending 900 mm above the top slab of the wet well. One vent pipe should extend down to within 300 mm of the obvert of the inlet pipe and the second should terminate on the underside of the roof of the wet well. Insect screens shall be provided on the vents.
- Wet Well Level Measurements and Control: Two float switches are to be provided with alarms: i. A high level alarm.

ii. A low level (shut-off) alarm.

Other Considerations:

- Automated supervisory control and data acquisition (SCADA) systems with remote sensing and telemetry equipment to be provided.
- Pump and equipment removal: vehicle access via the driveway. Access hatch to be provided to allow the use of exterior mobile cranes.
- Emergency conduit to the stormwater sewer is designed using the annual wet weather flow condition and shall be above the 25-year stormwater elevation and equipped with backwater valve.
- Emergency stand-by power: natural gas.
- An external underground vault separate from the wet well and control building containing the discharge piping, valves and flow/pressure monitoring equipment.

 Wet well structural design: the wet well structure shall be designed for all anticipated loads and the walls must be designed for lateral soil and hydrostatic loads with appropriate factors of safety. The maximum allowable wet well level under emergency conditions must be indicated. In floodplains, the structure shall be checked for the 100-year flood with an allowable stress increase of 1.33. The structure shall be sized with an appropriate flotation safety factor considering only the weight of the structure and soil on its haunches with maximum groundwater levels. All conduit and pipe penetrations to the wet well shall be made watertight and corrosion proof. All forcemain, re-circulation, drain, and gravity sewer piping shall have a flexible pipe joint within 0.9 m of the wet well wall. All construction joints below grade shall be built with a water stop.

3.0 PROPOSED FORCEMAIN

Forcemain design:

- Proposed PVC DR 26 150 mm (6") diameter.
- Velocity: 0.9 to 1.5 m/s at the time of commissioning. 0.8 to 2.5 m/s over the full operating range. Proposed 0.9 m/s under average dry weather flow.
- A minimum positive slope of 0.5 %.
- Approximate length: 219 m.
- Internal length: 5 m.
- A minimum depth cover of 2 m.
- No 90-degree bends.
- A minimum horizontal clearance from watermain of 3 m.
- Tracing wires for location.
- Two isolation valves at the both ends in two valve chambers.
- Air release valve at high point.
- Forcemain outlet condition: enter the receiving manhole with a smooth flow transition to the gravity sewer system at a point not more than 0.30 m above the flow line of the receiving sewer.

4.0 CONCLUSIONS

- It is proposed to construct a concrete wet well submersible station to pump the wastewater generated by the new development into the existing sanitary sewer at County Rd/Dodge St intersection. The wet well is designed to receive and store wastewater as well as to house the submersible pumps and level monitoring equipment.

- Two pumps rated 16 L/s and TDH of 8.5 m are proposed at the commissioning and until 2034. In 2034, depending on actual development staging, upgrade to 25 L/s may be required, otherwise 16 L/s pumps remain sufficient.

- A proposed 236 m long 150 mm diameter PVC forcemain DR 18 will connect the pumping station to the receiving manhole that shall be re-benched.

- An above-grade building housing the power, control and communications equipment as well as the stand-by natural gas generator shall be built as per drawings provided.



- An external underground chamber separate from the wet well and control building containing the discharge piping, valves and flow/pressure monitoring equipment.

- An automated supervisory control and data acquisition (SCADA) system with remote sensing and telemetry equipment shall be provided as per the Township specifications.

- The existing Adelaide pumping station capacity is able to accommodate the proposed pumped flow generated from the new pumping station.

- Sewage discharges will be domestic in type and in compliance with the latest *Ontario Building Code (OBC).*

Respectfully submitted,

Mongi Mabrouk M.Eng., P.Eng.

Advance Engineering

Phone: 613-986-9170

E-mail : <u>eng.services.ca@gmail.com</u>

APPENDICES

Appendix A

- Figure 1: Site location and site plan

Appendix B

- Wet well and pumping design

APPENDIX - A





APPENDIX - B

PROJECTED DESIGN FLOWS BASED ON ANTICIPATED DEVELOPMENT STAGING

STAGING	INITIAL 2023	10 YEAR 2033	20 YEAR 2043	BUILD-OUT
DEVELOPMENT	100 % OF FLOW EDWARDSBURGH DEVELOPMENT	100 % OF FLOW EDWARDSBURGH DEVELOPMENT	100 % OF FLOW EDWARDSBURG H DEV. + FUTURE DEV. (5 ha)	ULTIMATE DEVELOPMENTS MAX CAPACITY
AWF (L/s)	1.31	1.31	2.52	2.52
ADWF (L/s)	1.69	1.69	3.16	3.16
PDWF (L/s)	4.90	4.90	9.34	9.34
WWF (L/s)	7.04	7.04	12.89	12.89
AWWF (L/s)	4.09	4.09	7.26	7.26
RWWF (L/s)	6.01	6.01	10.43	10.43

AWF: Average Wastewater Flow Rate

ADWF: Average Dry Weather Flow Rate

PDWF: Peak Dry Weather Flow Rate

WWF: Peak Wet Weather Design Flow Rate Qd

AWWF: ANNUAL WET WEATHER FLOW

RWWF: RARE WET WEATHER FLOW

* Values of residential flows as per Table 1 of Ottawa Guidelines.

** Residential flow: 350 L/c/day

Page 1

HEAD LOSS Hazen-Williams Formula in Metric Units

$$h = 10.67 \ q^{1.852} / (c^{1.852} \ d_h^{4.8704})$$

where:

where:

h = head loss per unit pipe (m_{h20}/m pipe)

c = design coefficient determined for the type of pipe - the higher the factor, the smoother the pipe

q = flow rate (m³/s)

d_h = inside hydraulic diameter (m)

Pressure drop in Pa can be calculated from the head loss by multiplying the head loss with

the specific weight of liquid: $p = h \gamma$

p = pressure loss (N/m², Pa) Specific weight of water at 4°C is 9810 N/m³.

 γ = specific weight (N/m³)

	For	cemain	
	PVC	Ductile Iron	
D =	0.150	0.100	m
A =	0.0177	0.0079	m²
Q =	0.016	0.016	m³ /s
L =	219	5	m
$\gamma =$	12,000	12,000	N/m ³
С _{нw} =	130	100	Table 7.3 For pump selection
*Energy Slope h _f (m) =	0.00631	0.07389	m _{h20} /m pipe
h total = hf L (m) =	1.382	0.369	m Total=1.8 m
P drop =	16.58	4.43	kPa
V =	0.91	2.04	

II/ MINOR LOSSES: h_m= KV²/ 2g

Minor Losses Coefficients (source SHEA)

	/					
Discharge	k Value	Qty	Sum			
45° Bend	0.35	3	1.05			
90º Bend	0.75	2	1.5			
Tee, Run Through	0.4	0	0			
Tee, as Elbow	1	1	1			
Expansion	0.5	1	0.5			
Coupling	0.04	2	0.08			
Check Valve	3	2	6			
Gate Valve Open	0.2	2	0.4			
Exit	1	1	1			
		Total k	11.53			
	<i>g</i> =	9.81	m/s ²			
	V =	0.91	m/s			
I	$m_m = KV^2 / 2g =$	0.48	т			

III/ TOTAL DYNAMIC HEADLOSS

 $h_{dynamic} = h_{static} + h_f + h_m$

H_{static} = 6.9 m

 $h_{dynamic} = 9.2 m$

1/1

PUM	PING STATI	ON DESIGN
I/ Detention Times	Using ADWF	
Wet well:		
Wet well cross-sectional area:	4.500 m ²	
Operational height:	0.50 m	
Operational Volume:	2.250 m³	
Forcemain:		
Forcemain diameter:	0.150 m	
Pipe area:	0.0177 m²	
Qp=	16.00 L/s	
Velocity:	0.9 m/s	2.0 m/s inside wet well piping
Length:	220.0 m	
Pipe Volume:	3.888 m³	
Volume of wet well and forcemain:	6.138 m³	
Retention Time in wet well:	22 mn	under average dry weather flow of 1.69 L/s
Retention Time in wet well:	3 mn	under peak wet weather flow of 12.89 L/s
II/ Pumping Cycling:		

T= V/(Qp-Qin) + V/Qin where:

T = Time between pump starts (minutes)

V = Effective wet well volume (Litres) between lead pump start and lead pump stop Qp = Pump/station discharge capacity (L/minute), and,

Qin = Station inflow rate (L/minute)

 Operational volume V=
 2250 L

 Qp=
 960.0 L/mn

 Qin=
 104.1 L/mn
 (1.69 L/s)
 ADWF

 T=
 24 mn
 Start frequency:
 2.5
 per hour

III/ Elevations

Top wet well elevation:	82.40
Inlet sewer elevation:	78.75
High liquid level inside wet well:	77.90
Low liquid level (pump shut-down):	77.40
Bottom level:	77.10
Forcemain outlet level:	80.10
Emergency outlet level:	80.60
Total height of wet well:	5.0 m
Total volume:	22.5 m³
Forcemain Invert elevation at Cty Rd:	84.00

FLOTATION OF WET WELL CHECK

Weight of the Structure Force

Internal Diameter	2.4	m
Well Wall Thickness	0.23	m
Wall Height	5	m
Well Base Thickness	0.3	m
Well Top Thickness	0.3	m
g=	9.8	m/s2
Water Ro=	1000	kg/m3
Concrete Density	23	kN/m3
Well Wall Section Perimeter at CL	8.3	m
Well Wall Section Area	1.9	m2
Well Wall Volume	9.502	m3
Base and Top Area	6.42	m2
Base Volume	1.927	m3
Top Volume	1.927	m3
Mall - Ross - Ton Volume	10 256	
Wall + Base + Top Volume	13.300	m3
vvali + Base + Top vveight	307.2	KN
Upward Buoyant Force		
Elevation of GWT	79.65	Geotech
Well Bottom Elevation	76.795	m
Submorged Height	2 0 5 5	

Elevation of GWT**79.65** Geotechnical report BH#5Well Bottom Elevation76.795 mSubmerged Height2.855 mSubmerged Section6.42 m2Submerged Volume18.341 m3Submerged Equivalent Weight**179.7** kN

1.71

Safety Factor

Notes: Cohesion friction ignored.

Maximum groundwater level taken as per Geotechnical report may vary.



Mon, Aug 8, 2022 at 9:41 AM

Lockmaster's Subdivision - Pumping Station

Wendy Van Keulen < wvankeulen@twpec.ca>

To: Eng Services <eng.services.ca@gmail.com>

Cc: "elaine.mallory@uclg.on.ca" <elaine.mallory@uclg.on.ca>, "David.firstfin@sympatico.ca" <David.firstfin@sympatico.ca>, "sabbyduthie@gmail.com" <sabbyduthie@gmail.com>, Eric Wemerman <ewemerman@twpec.ca>, Gord Shaw <gshaw@twpec.ca>, Dave Grant <dsgrant@twpec.ca>

Good Morning Mongi,

Please see responses below. As discussed by phone last week, we will review the design report once it is ready with this info.

1- We are planning to propose a factory-made wet made of FRP with submersible pumps Flygt. It comes with 25 year warranty for all parts including the shell. See attached file from the manufacturer (xylem).

The Township prefers Flygt pumps to match all other stations in Cardinal. In regards to the FRP wetwell, could you include a reference (contact info and location) for a municipality that uses this?

2- The control building is not needed except for the generator. If you have any requirements, please let us know. There is a site plan appended to the report.

Please have the pump and flow controls, level transmitter systems, generator and electrical all under one roof.

3- Stand-by generator: natural gas or diesel?

Natural Gas

4- Do you have any particular requirements for the SCADA or control panel, so all Cardinal pumping stations will be harmonized?

SCADA – We have Elpro radios installed at our other stations to transmit level information back to our central SCADA system. The same would be required for the new station.

Control panel- We currently use a Greyline level and pressure transducer system at most stations in Cardinal for pump control. This would be the preferable system. We also use ABB flow meters.

Additional/Early Comments:

Please include more detail regarding the configuration of the valve chamber, perhaps an actual drawing. We would like to see a means of bypass so the wet well could be pumped down by a portable 4" pump directly to the force main, (bypass), to allow internal work in the wet well without disrupting flows or bypassing sewage to the storm system. In section 3.0 Proposed Forcemain, it is indicated that the min size of the forcemain is 100mm and the proposed sizing is 150. It is described latter on as a 150 but we would like to see a commitment to 150mm.

Thankyou WendyVanKeulen

NP 3102 MT 3~ Adaptive 464

Patented self cleaning semi-open channel impeller, ideal for pumping in waste water applications. Modular based design with high adaptation grade.



Technical specification



=		
[m] Head		
14.0-		
13.5		
13.0		
12.5		
12.0		
11.5		
11.0		
10.5		
10.0		
9.5		
9.0		
8.5		
80		
7.5		
7.0	65.8%	
7.0	00.070	
0.0		
6.0		
5.5		
5.0		
4.5		
4.0	`	
3.5		
3.0		
25		
2.0		
1.5-		464 162mm
1.5		
1.0		
0.5		
0.0- 7++++++++++++++++++++++++++++++++++++		
0 5 10 15	20 25 30 35 4	0 45 50 [l/s]
		Curve: ISO 9906

Curves according to: Water, pure Water, pure [100%],277 K,999.9 kg/m³,1.5692 mm²/s

Configuration Motor number Installation type N3102.060 18-11-4AL-W P - Semi permanent, Wet 5hp Discharge diameter 100 mm Impeller diameter 162 mm **Pump information Materials** Impeller diameter Impeller Hard-Iron ™ 162 mm Discharge diameter Stator housing material 100 mm Grey cast iron Inlet diameter 100 mm Maximum operating speed 1745 1/min Number of blades 2 Max. fluid temperature 40 °C Project Created by Eric Mondoux 8/2/2022 Block 8/2/2022 Last update Created on

^{usergroup(s)} ≫**₽age** 356 of 465

NP 3102 MT 3~ Adaptive 464

Phases

Number of poles

Rated voltage

3~

4

600 V

84.4 %

Technical specification

Motor - General

Motor number N3102.060 18-11-4AL-W 5hp ATEX approved

No **Frequency**

60 Hz Version code 060

Motor - Technical

Power factor - 1/1 Load 0.82

Power factor - 3/4 Load 0.76

Power factor - 1/2 Load 0.65 85.2 % Motor efficiency - 3/4 Load 85.8 % Motor efficiency - 1/2 Load

Motor efficiency - 1/1 Load

Total moment of inertia 0.0253 kg m²

Rated speed

. 1745 1/min

Rated current

Insulation class

5.1 A

н

Starting current, direct starting 31 A

Starting current, star-delta 10.3 A

ProjectCreated byEric MondouxBlockCreated on8/2/2022Last update8/2/2022



Rated power

Stator variant

Type of Duty

Starts per hour max.

5 hp

63

S1

30



Data version 7/7/2022 15:55 A7P7

NP 3102 MT 3~ Adaptive 464



Duty Analysis


NP 3102 MT 3~ Adaptive 464





Curves according to: Water, pure , 277 K, 999.9 kg/m³, 1.5692 mm²/s $\,$ [m] Head 14.0 13.5 13.0 12.5 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 65.8% 7.0 6.5 6.0 5.5 5.0 4.5 4.0 3.5 65.8% 3.0 2.5 2.0 `464 162mm 1.5 55 Hz 45 Hz 50 Hz 1.0 0.5 ^[%] Efficiency 60 Overall Efficiency 50-40 30-40 Hz 45 Hz 58 Hz 55 Hz 464 162mm 20-10-[hp] Power input P1 464 162mm (P1) Shaft pow er P2 4.0 464 162mm (P2) -55 Hz -55 Hz 3.0-—50 Hz —50 Hz -45 Hz -45 Hz 2.0 40 Hz 40 Hz 1.0 ₽n¶= NPSHR-values ~464 162mm 8 7-50 6 45 Hz 5 40 Hz 4-3-24 52 [l/s] Curve: ISO 9906 8 12 16 20 28 0 4 32 36 40 48 52 44 Project Created by Eric Mondoux Block Created on 8/2/2022 Last update 8/2/2022



Project	Created by	Eric Mondoux		
Block	Created on	8/2/2022	Last update	8/2/2022



NP 3102 MT 3~ Adaptive 464

Dimensional drawing







TYPICAL SECTION

SIDE VIEW

					PRODU	JCT VARIA	BLES			
		NOMINAL	חו	OD	wт	MASS	MEG	SI	_A	MIN. SLING
r	ANTID	SIZE		00	VVI	(KG)	WI G	SPEC.	f'c (MPa)	ANGLE
PA	A 1050X4	1050	1067	133/	133	3115	GUE	4T 3-1/2	30	60
17		1000	1007	1004	100	0110	OAK	4T 3-1/2 DH	30	60
PA	1200X48	1200	1219	1473	127 BW	3475	OAK	4T 3-1/2 DH	30	60
PA	1200X49	1200	1219	1511	146 CW	3810	GUE	4T 4-1/4	30	60
PA	1350X48	1350	1372	1652	140 BW	4115	OAK	4T 4-1/4 DH	30	60
PA	1350X49	1350	1372	1689	159 CW	4731	GUE	4T 4-3/4	30	60
PA	A 1500X4	1500	1524	1820	152	5180	OAK	4T 4-1/4 DH	30	60
17		1000	1024	1023	102	5100	GUE	4T 4-3/4	35	60
PA	A1650X4	1650	1676	2007	165	6101	GUE	4T 4-3/4	40	60
PA	A1800X4	1800	1829	2184	178	6991	GUE	8T 5-3/4	30	60
PA	A1950X4	1950	1981	2362	191	8110	GUE	8T 5-3/4	40	60
PA	A2100X4	2100	2134	2540	203	9290	GUE	8T 6-1/4	30	60
PA	A2250X4	2250	2286	2718	216	10520	GUE	8T 6-3/4	30	60
PA	A2400X4	2400	2438	2896	229	11880	GUE	8T 7-1/8	30	60
PA	A2550X4	2550	2591	3073	241	12637	GUE	8T 7-1/8	40	60
PA	A2700X4	2700	2743	3251	254	14035	GUE	8T 8-1/4	40	60
PA	A3000X4	3000	3048	3607	279	17185	GUE	20T 10	40	60
	A3000X4	3000	3048 MIN. CONC S	3607	279 0-40 MPa	17185	GUE	20T 10	40 P) STANDA	60
RAWINGS ARE NOT T	TO SCALE		BASED ON C				2 0	= (DOC	
ANDARD CLASS: 65E	D, 100D, 140D		DESIGN. REF	TO CSA 25	7.2-14	USA 207.	2 R			
TING RIGGING CODI	E: S2S-SP -PA02		TOLERANCE	S TO CSA A	257.2-14		REINF	ORCED C	ONCRET	E PIPE
							105	0 - 3000 m	m DIAME	TER
								SIZE (
8 SLA UPDA	TE, RIGGING	REF, CSA A2	57.2 UPDATE	RM	5APR16					

CHECKED BY

CW

DATE

4/JAN/11

1-800-668-7473

FILE

Pipe

RM

SW

ENG.

7/NOV/14

17/SEP/14

DATE

DRAWN BY

SW

SLA UPDATE FOR 2550

REVIEWED, SLA NOTES

DESCRIPTION

7

6

REV.

PAGE

1 OF 2



G:\Engineering\Library\Solidworks\Pipe\Pipe Size Guide\





SH

REV

WINDCHILL VERSION

SH	3/3	REV	С	WINDCHILL VERSION
	0,0		<u> </u>	

4

MODEL	VOLTAGE	WEIGHT	CENTER OF GRAVITY DIM X	CENTER OF GRAVITY DIM Y	CENTER OF GRAVITY DIM Z
SG/MG 120, 150, PG/WG 108, 135	240V, Ø	2,396 kg [5,281 lbs]	1748 [68.8]	706 [27.8]	
SG/MG 120, 150, PG/WG 108, 135	600V	2,439 kg [5,376 lbs]	1732 [68.2]	704 [27.7]	
SG/MG 120, 150, PG/WG 108, 135	208V, 240V, 480V	2,445 kg [5,389 lbs]	1730 [68.1]	704 [27.7]	645 [04 0]
SG/MG 140, 175, PG/WG 126, 158	240V, Ø	2,463 kg [5,429 lbs]	1721 [67.8]	703 [27.7]	015 [24.2]
SG/MG 140, 175, PG/WG 126, 158	600V	2,469 kg [5,442 lbs]	1719 [67.7]	703 [27.7]	
SG/MG 160, 200, PG/WG 144, 180	208V, 240V, 480V	2,477 kg [5,460 lbs]	1716 [67.6]	702 [27.6]	

В

STD ENCLOSURE, STEEL

MODEL	VOLTAGE	WEIGHT	CENTER OF GRAVITY DIM X	CENTER OF GRAVITY DIM Y	CENTER OF GRAVITY DIM Z
SG/MG 120, 150, PG/WG 108, 135	240V, Ø	2,840 kg [6,261 lbs]	1843 [72.6]	777 [30.6]	
SG/MG 120, 150, PG/WG 108, 135	600V	2,883 kg [6,356 lbs]	1828 [72.0]	774 [30.5]	
SG/MG 120, 150, PG/WG 108, 135	208V, 240V, 480V	2,889 kg [6,369 lbs]	1826 [71.9]	773 [30.4]	577 [22 7]
SG/MG 140, 175, PG/WG 126, 158	240V, Ø	2,907 kg [6,409 lbs]	1818 [71.6]	772 [30.4]	577 [22.7]
SG/MG 140, 175, PG/WG 126, 158	600V	2,913 kg [6,422 lbs]	1816 [71.5]	772 [30.4]	
SG/MG 160, 200, PG/WG 144, 180	208V, 240V, 480V	2,921 kg [6,440 lbs]	1814 [71.4]	771 [30.4]	

L1A ENCLOSURE, STEEL

MODEL	VOLTAGE	WEIGHT	CENTER OF GRAVITY DIM X	CENTER OF GRAVITY DIM Y	CENTER OF GRAVITY DIM Z
SG/MG 120, 150, PG/WG 108, 135	240V, Ø	2,978 kg [6,566 lbs]	1771 [69.7]	790 [31.1]	
SG/MG 120, 150, PG/WG 108, 135	600V	3,021 kg [6,660 lbs]	1758 [69.2]	787 [31.0]	
SG/MG 120, 150, PG/WG 108, 135	208V, 240V, 480V	3,027 kg [6,674 lbs]	1757 [69.2]	786 [31.0]	570 [22 0]
SG/MG 140, 175, PG/WG 126, 158	240V, Ø	3,045 kg [6,713 lbs]	1749 [68.9]	785 [30.9]	576 [22.0]
SG/MG 140, 175, PG/WG 126, 158	600V	3,051 kg [6,726 lbs]	1748 [68.8]	785 [30.9]	
SG/MG 160, 200, PG/WG 144, 180	208V, 240V, 480V	3,059 kg [6,744 lbs]	1745 [68.7]	784 [30.9]	

L2A ENCLOSURE, STEEL

MODEL	VOLTAGE	WEIGHT	CENTER OF GRAVITY DIM X	CENTER OF GRAVITY DIM Y	CENTER OF GRAVITY DIM Z
SG/MG 120, 150, PG/WG 108, 135	240V, Ø	3,085 kg [6,801 lbs]	1859 [73.2]	886 [34.9]	
SG/MG 120, 150, PG/WG 108, 135	600V	3,128 kg [6,896 lbs]	1845 [72.6]	881 [34.7]	
SG/MG 120, 150, PG/WG 108, 135	208V, 240V, 480V	3,134 kg [6,909 lbs]	1843 [72.6]	881 [34.7]	E00 [22 0]
SG/MG 140, 175, PG/WG 126, 158	240V, Ø	3,152 kg [6,949 lbs]	1836 [72.3]	879 [34.6]	500 [22.0]
SG/MG 140, 175, PG/WG 126, 158	600V	3,158 kg [6,962 lbs]	1834 [72.2]	878 [34.6]	
SG/MG 160, 200, PG/WG 144, 180	208V, 240V, 480V	3,166 kg [6,980 lbs]	1831 [72.1]	877 [34.5]	

Α

DRAWING CREATED FROM PRO/ENGINEER 3D FILE. ECO MODIFICATION TO BE APPLIED TO SOLID MODEL ONLY.

4

INSTALLATION DRAWING

3

ELECTRONICALLY APPROVED

GENERAC POWER SYSTEMS OWNS THE COPYRIGHT OF THIS DRAWING WHICH IS SUPPLIED IN CONFIDENCE AND MUST NOT BE USED FOR ANY PURPOSE OTHER THAN FOR WHICH IT IS SUPPLIED WITHOUT THE EXPRESS WRITTEN CONSENT OF GENERAC POWER SYSTEMS.

Page 368 of 465

2

©GENERAC POWER SYSTEMS 2013

DIMENSIONS ARE IN MILLIMETERS [INCHES]

INSIDE WINDCHILL

L			
WEIGHT	CENTER OF GRAVITY DIM X	CENTER OF GRAVITY DIM Y	CENTER OF GRAVITY DIM Z
2,688 kg [5,926 lbs]	1808 [71.2]	768 [30.2]	
2,731 kg [6,021 lbs]	1792 [70.6]	765 [30.1]	
2,737 kg [6,034 lbs]	1791 [70.5]	764 [30.1]	570 [22 9]
2,755 kg [6,074 lbs]	1782 [70.2]	763 [30.0]	579 [22.0]
2,761 kg [6,087 lbs]	1780 [70.1]	763 [30.0]	
2,769 kg [6,104 lbs]	1777 [70.0]	762 [30.0]	
_,	[10.0]	[00.0]	1

CENTE WEIGHT 2,734 kg [6,027 lbs] 2,777 kg [6,122 lbs] 2,783 kg [6,135 lbs] 2,801 kg [6,175 lbs] 2,807 kg [6,188 lbs] 2,815 kg [6,206 lbs]

943 lbs]	
956 lbs]	
974 lbs]	

C.1

NOTE:

L		,,	
WEIGHT	CENTER OF GRAVITY DIM X	CENTER OF GRAVITY DIM Y	CENTER OF GRAVITY DIM Z
2,629 kg [5,795 lbs]	1837 [72.3]	757 [29.8]	
2,672 kg [5,890 lbs]	1821 [71.7]	754 [29.7]	
2,678 kg [5,903 lbs]	1819 [71.6]	754 [29.7]	577 [22 7]
2,696 kg [5,943 lbs]	1810 [71.3]	753 [29.6]	577 [22.7]
2,702 kg [5,956 lbs]	1808 [71.2]	752 [29.6]	
2,710 kg [5,974 lbs]	1805 [71.1]	752 [29.6]	

CENTER OF GRAVITY AND WEIGHT MAY CHANGE DUE TO UNIT OPTIONS

STD ENCLOSURE, ALUMINUM

L1A ENCLOSURE, ALUMINUM

L2A ENCLOSURE, ALUMINUM

ER OF GRAVITY DIM X	CENTER OF GRAVITY DIM Y	CENTER OF GRAVITY DIM Z
1855 [73.0]	827 [32.6]	
1839 [72.4]	823 [32.4]	
1837 [72.3]	823 [32.4]	591 [22 0]
1829 [72.0]	821 [32.3]	561 [22.9]
1829 [71.9]	820 [32.3]	
1824 [71.8]	820 [32.3]	



TITL	TITLE								
	WEIGHT AND CENTER OF GRAVITY								
	G14.2L								
	60HZ: SG150/PG135, SG175/PG158, SG200/PG180								
	50HZ: SG12	20/PG	108, SG	6140/PG126,	SG160/PG	144			
ISSU	E DATE:	11/26/	14						
SIZE	E CAGE NO	D\	VG NO	10000	೧೨೧೯೦	5	REV		
В	N/A		1000003936		5	С			
SCA	E 0.016	WT-K	G		SHEET	3 of	3		
				1					

В

Α

LIST OF DRAWINGS

No.	INDEX	TITLE	REV. No.	DATE
1	CS-1	COVER SHEET - LIST OF DRAWINGS & KEY PLAN	2	04-15-2024
2	PS-1	SITE PLAN AND GENERAL NOTES AND SPECIFICATIONS	2	04-15-2024
3	PS-2	PUMPING STATION WET WELL - SECTIONS AND DETAILS	2	04-15-2024
4	PS-3	PUMPING STATION FORCEMAIN BY-PASS CHAMBER	2	04-15-2024
5	PS-4	PUMPING STATION DETAILS	1	11-22-2023
6	A-1	PUMPING STATION GENERATOR BUILDING	1	11-22-2023
7	M-1	PUMPING STATION MECHANICAL PLANS	1	11-22-2023
8	E-1	PUMPING STATION ELECTRICAL PLANS	1	11-22-2023

UNITED COUNTIES OF LEEDS AND GRENVILLE VILLAGE OF CARDINAL

LOCKMASTER' S MEADOW SUBDIVISION PUMPING STATION

PART OF LOT 7, CONCESSION 1 GEOGRAPHIC TOWN OF EDWARDSBURGH TOWNSHIP OF EDWARDSBURGH/CARDINAL COUNTY OF GRENVILLE

> ADDRESS: COUNTY RD No. 22 CARDINAL, ONTARIO

> > APPLICANT: Edwardsburgh Developments Ltd. 434-300 EARL GREY DRIVE KANATA, ON K2T 1C1 613-282-5601

CONSULTANT:

ADVANCE Civil - Municipal - Structural 613-986-170

PROJECT No. 114

APRIL 2024

04-15-2024 04-15-2024 04-15-2024 11-22-2023 11-22-2023 11-22-2023 11-22-2023

RAILWAY CANADIAN NATIONAL STATION RD PUMPING | STATION St. Lawrence River St. Lawrence River KEY PLAN ----Not To Scale

TO \Lambda 🧹

KEMPTVILLE







04/15/24



NUM	VENT

LEVEL CONTROLS GUIDE TO BE SECURED AT 2m INTERVALS STARTING 300mm ABOVE FLOAT LEVEL TYPICAL. POSITIONED SUCH THAT FLOATS DO

TO PROVIDE MAXIMUM PERIMETER

ABOVE PUMPS. OPENING TO BE

LINK-SEAL MODULAR SEALS MANUFACTURED BY PIPELINE	WITH MODEL WS STEEL WALL SLEEVES SEAL & INSULATOR, INC.
	ELASTOMERIC SEAL ELEMENT LS MODEL BOLT PRESSURE PLATE
LS Model Seal Element Bolts/Nuts	CONTINUOUSLY WÉLDED ON BOTH SÍDES
<u>Sleeve Model Description</u> WS Steel Wall Sleeve	<u>Material</u> Steel

<u>NOTES:</u>

- 1. ULTRASONIC AND PRESSURE TRANSDUCERS TO BE PROVIDED AS PRIMARY AND SECONDARY LEVEL CONTROLS INSIDE THE WET WEILL. FLOATS ARE THIRD BACK UP.
- 2. PROVIDE A BASE PLATE WITH ANCHORS FOR PORTABLE DAVIT MOUNT.

2 TOWNSHIP COMMENTS 04/15/24 11/22/23 1 INITIAL ISSUE DATE MM/DD/YY REVISION / ISSUE No. PREPARED BY: Mongi Mabrouk P.Eng. Phone: 613-986-9170 Email: eng.services.ca@gmail.com ROFESSION M. MABROUK 100136017 ADVANCE ENGINEERING 04/15/202A CE OF O PROJECT NAME AND ADDRESS: LOCKMASTER'S MEADOW SUBDIVISION 95 LOTS COUNTY ROAD No. 22 (SHANLY RD), CARDINAL, ONTARIO APPLICANT: Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata 613-282-5601 TITLE: PUMPING STATION **SECTIONS &** DETAILS

SCALE: 1:25

DRAFTED BY:

DATE:

DRAWING No .:

PS-2

04/15/24









NO	TES:
1.	ALL JOINTS, VALVES AND FITTINGS SHALL BE
	FLANGED WITH UNIFLANGE RESTRAINTS.
2.	SIZE OF PIPING, VALVES AND FITTINGS TO BE
	SAME SIZE AS FORCEMAIN EXCEPT WHERE
	OTHERWISE INDICATED.
3.	CONSTRUCTION AND REINFORCEMENT TO OPSD 705.
4.	ALL DIMENSIONS ARE IN mm UNLESS OTHERWISE
_	NOTED.
5.	MINOR VARIATION IN THE CHAMBER DIMENSIONS
	MIGHT BE APPROVED IF THERE ARE BENEFITS TO
	THE CLIENT.







Page 374 of 465





SCHEDULE "J"

STREET SIGNAGE AND LIGHTING

Traffic signage shall be installed as per the Traffic Signage Plan (SIG-1, SIG-2), prepared by Advance Engineering Ltd., stamped and dated September 6, 2023.

STREET SIGNS

Reflectorized aluminum street signs on square perforated steel/galvanized posts shall be installed as set out in clause 16 and at the location(s) specified by the Traffic Signage Plan.

Streets shown in Schedule "B" shall be named as follows:

Street A: Balsam Street Street B: Lockhouse Street Street C: Conifer Lane

STREET LIGHTING

Streets shall be illuminated as per the Photometric Plan prepared by Advance Engineering, dated July 15, 2024.

The Owner agrees to install Street lighting in accordance with the Municipal requirements and in compliance with the Electrical Safety Authority's Guidelines for the Design, Installation, Operation and Maintenance of Street Lighting Assets.

The Owner agrees to provide streetlights where streets intersect with the United Counties Road as close as possible to the intersection of the road allowances, in a location approved by the United Counties. These streetlights shall be designed and installed under the guidance, requirements and to the satisfaction of the United Counties.

Unless otherwise required by the Municipality, street light poles are to be made of composite material.

Attached:

- Traffic Signs and Pavement Markings (SIG1) June 18, 2024
- Existing Signs along County Road (SIG2) June 18, 2024
- Photometric Plan (PH1) July 15, 2024







<u>PHOTO 1</u> TWO SIGNS TO BE RELOCATED TO APPROXIMATELY 30 m NORTH OF CONIFER LN CENTRELINE OR AS DIRECTED BY VILLAGE STAFF. DODGE ST SIGN TO BE INSTALLED ON TOP OF THE EXISTING STOP SIGN AT DODGE ST EDGE. A NEW SIGN POST FOR BALSAM ST TO BE PROVIDED AS SHOWN.





	Ottawa	Riq	ght—of—Way	Light	ing F	oLicy	Septer	nber	9,	2016	
Γ	Table 2	21	Recomment	ded A	verac	ie Roa	dway	liahtir	na	l evel	s

	Table 2.1 Recommended Average Roddway Lighting Levels						
	AREA CLASSIFICATION	LUMINANCE		GLARE	ILLUMINANCE		
CLASSIFICATION		Average Luminance Lavg (Cd/m ²)	Uniformity Ratio L _{avg} / L _{min}	Veiling Luminance Ratio L _{Vmax} / L _{avg}	Minimum Maintained Average E _{avg} (Lux)	Uniformity Ratio E _{avg} / E _{min}	
LOCAL	General Urban Area / Other	0.30	6.0	0.40	4.0	6.0	

Ottawa Right—of—Way l	ighting PoLicy September S	9, 2016			
Table 2.2 Recommende	ed Average Lighting Levels	for Intersections			
	MINIMUM MAINTAINED AVERAGE (Lux) BY AREA CLASSIFICATION / UNIFORMITY RATIO Eavg / Emin				
INTERSECTING ROADWAY CLASSIFICATION	Mixed Use Centre / Central Area High	Employment / Enterprise Area Medium	General Urban Area / Other & Rural Signalized Intersections Low		
ARTERIAL & LOCAL	26.0 / (6.0)	20.0 / (6.0)	13.0 / (6.0)		
LOCAL & LOCAL	18.0 / (6.0)	14.0 / (6.0)	8.0 / (6.0)		

POADWAY	Maintained Illuminance Levels					
CLASSIFICATION	Average Horizontal E _{avg} (Lux)	Uniformity Ratio E _{avg} / E _{min} (Max.)				
Walkways	5.0	10.0				

<u>LEGEND</u> HYDRO POLE TREE HEDGES



			Luminaire	list (Site 1)				
Index	Manufacturer	Article name	Item number	Fitting	Luminous flux	Maintenance factor	Connected load	Quantity
1	Philips	RoadFocus LED Cobra Head - Medium (RFM), 48 LED's, 4000K CCT, TYPE R3S OPTIC,	RFM-55W48LED 4K-G2-R3S	1x (3) LEDgine ARRAY(S) DRIVEN AT 350mA	7882 lm	0.80	55.1 W	6
2	Philips	RoadFocus LED Cobra Head - Small (RFS), 40 LED's, 4000K CCT, TYPE R2M OPTIC,	RFS-35W40LED 4K-G2-R2M	1x (2) LEDgine ARRAY(S) DRIVEN AT 280mA	5471 lm	0.80	35.3 W	38

#	Name	Parameter	Min	Max	Average	Mean/Min	Max/Min
1	INT-1	Perpendicular illuminance (Adaptive)	0.50 lx	25.6 lx	10.6 lx	21.2	51.2
		Luminance (Adaptive)	0.016 cd/m ^a	0.84 cd/m²	0.35 cd/m²	21.9	52.5
2	INT-2	Perpendicular illuminance (Adaptive)	3.27 lx	28.6 lx	16.1 lx	4.92	8.75
		Luminance (Adaptive)	0.11 cd/m²	0.94 cd/m²	0.53 cd/m²	4.82	8.55
3	INT-3	Perpendicular illuminance (Adaptive)	4.55 lx	29.5 ix	15.3 ix	3.36	6.48
		Luminance (Adaptive)	0.15 cd/m²	0.97 cd/m²	0.51 cd/m*	3.40	6.47
4	INT—4	Perpendicular illuminance (Adaptive)	4.45 ix	26.5 ix	12.9 ix	2.90	5.96
		Luminance (Adaptive)	0.15 cd/m²	0.87 cd/m²	0.43 cd/m [*]	2.87	5.80
5	INT—5	Perpendicular illuminance (Adaptive)	3.05 lx	28.7 ix	13.3 lx	4.36	9.41
		Luminance (Adaptive)	0.10 cd/m²	0.95 cd/m²	0.44 cd/m²	4.40	9.50
6	INT—6	Perpendicular illuminance (Adaptive)	6.51 lx	36.0 lx	23.7 lx	3.64	5.53
		Luminance (Adaptive)	0.21 cd/m*	1.19 cd/m*	0.78 cd/m [*]	3.71	5.67
7	A1	Perpendicular illuminance (Adaptive)	3.65 lx	23.8 lx	10.3 lx	2.82	6.52
		Luminance (Adaptive)	0.12 cd/m [*]	0.79 cd/m²	0.34 cd/m²	2.83	6.58
8	сı	Perpendicular illuminance (Adaptive)	3.02 lx	23.9 lx	10.6 lx	3.51	7.91
		Luminance (Adaptive)	0.100 cd/m [*]	0.79 cd/m²	0.35 cd/m²	3.50	7.90
9	A2	Perpendicular illuminance (Adaptive)	4.19 ix	23.8 lx	10.6 lx	2.53	5.68
		Luminance (Adaptive)	0.14 cd/m ²	0.79 cd/m ²	0.35 cd/m²	2.50	5.64
10	C2	Perpendicular illuminance (Adaptive)	1.56 lx	23.9 lx	9.52 lx	6.10	15.3
		Luminance (Adaptive)	0.052 cd/m ^a	0.79 cd/m ²	0.31 cd/m ^a	5.96	15.2
11	B1	Perpendicular illuminance (Adaptive)	3.00 lx	24.8 ix	10.9 lx	3.63	8.27
		Luminance (Adaptive)	0.099 cd/m ²	0.82 cd/m [*]	0.36 cd/m ²	3.64	8.28
12	82	illuminance (Adaptive)	3.55 lx	24.1 lx	10.8 lx	3.04	6.79
		Luminance (Adaptive)	0.12 cd/m ^ª	0.79 cd/m²	0.36 cd/m ²	3.00	6.58
13	83	Perpendicular illuminance (Adaptive)	6.65 lx	25.6 lx	16.0 lx	2.41	3.85
		Luminance (Adaptive)	0.22 cd/m [*]	0.84 cd/m ²	0.53 cd/m ²	2.41	3.82
14	B4	Perpendicular illuminance (Adaptive)	6.24 lx	24.1 lx	12.7 lx	2.04	3.86
		Luminance (Adaptive)	0.21 cd/m ²	0.80 cd/m ²	0.42 cd/m ²	2.00	3.81
15	B5	Perpendicular illuminance (Adaptive)	7.99 lx	25.0 lx	15.2 lx	1.90	3.13
		Luminance (Adaptive)	0.26 cd/m ²	0.83 cd/m²	0.50 cd/m ²	1.92	3.19
16	B6	Perpendicular illuminance (Adaptive)	4.30 lx	24.2 ix	10.9 lx	2.53	5.63
		Luminance (Adaptive)	0.14 cd/m ²	0.80 cd/m [*]	0.36 cd/m*	2.57	5.71
17	B7	Perpendicular illuminance (Adaptive)	4.88 lx	23.9 lx	10.9 lx	2.23	4.90
		Luminance (Adaptive)	0.16 cd/m ²	0.79 cd/m*	0.36 cd/m ²	2.25	4.94
18	P1	Perpendicular Illuminance (Adaptive)	1.04 lx	97.5 lx	21.1 lx	20.3	93.8
		Luminance (Adaptive)	0.034 cd/m²	3.22 cd/m ²	0.70 cd/m ²	20.6	94.7

7. LUMINAIRE FOR WALKWAY SHALL BE

FULL CUT OFF TYPE.

INITIAL SUBMISSION

Mongi Mabrouk P.Eng.

Email: eng.services.ca@gmail.com

ADVANCE ENGINEERING

PROJECT NAME AND ADDRESS:

Edwardsburgh Developments Ltd.

434-300 Earl Grey Drive

APPLICANT:

Kanata, ON

TITLE:

SCALE:

DRAFTED BY:

613-282-5601

No. | REVISION / ISSUE

Phone: 613-896-9170

PREPARED BY:

- 6. LED SQUARE LANTERN LUMINAIRE -SIDE MOUNT AS PER LLD002B.

- 3.5m. OTTAWA STD. LLD004A.
- 5. LED WING STYLE LUMINAIRE. HEIGHT
- INTERSECTIONS.
- 4. LED LUMINAIRE SHALL BE TYP II FOR STREET SEGMENTS AND TYPE IV FOR

- LBD001A.
- 3. BRACKET AS PER OTTAWA STD.
- 2. CONCRETE POLE HANDLING AND INSTALLATION AS PER OTTAWA STD. LID003A.
- DATED SEPTEMBER 9, 2019.
- CONFORM TO THE CITY OF OTTAWA "RIGHT-OF-WAY LIGHTING POLICY",
- <u>NOTES</u>
- 1. STREET LIGHTS EQUIPMENTS SHALL

PROJECT No.: 0114 DATE: 07-15-2024

1:600



SCHEDULE "K"

LANDSCAPING

For the lands set out in Schedule "A", the Owner agrees to implement the objectives and criteria of the Landscape Plan (LS-1), prepared by Advance Engineering Ltd., stamped and dated June 18, 2024.

EARTH BERM (ACOUSTIC BARRIER)

The Owner shall ensure that an earth berm is installed as shown on the Landscape Plan (LS-1). The earth berm shall be 2.5 meters above grade at the property line, with side slopes not steeper than 2.5 to 1. Coniferous trees shall be planted on the North side of the earth berm, at a minimum height of 2.0m.

FENCING

The Owner shall install that a chain-link fence of minimum 1.83 meter height along the municipal property line as shown on the Landscape Plan (LS-1).

The Owner shall install a chain link fence along the walkway shown on Block H of the Landscape Plan (LS-1). Bollards shall be erected on the walkway in accordance with the detail shown on D-5, ensuring a minimum separation distance between the bollards of 1.2m.

CARE AND MAINTENANCE OF PLANTINGS

The Owner shall provide necessary care for all plantings in the Landscape Plan during the course of developing the lands in accordance with this Agreement.

The following language shall be included in all Lease and Purchase and Sale Agreements for lots 13-20, inclusive:

The plantings along the eastern property boundary are for screening purposes and shall not be removed. The care and maintenance of the plantings is the responsibility of the property owner.

Attached:

• Landscape Plan (LS-1) June 18, 2024



7. CONTRACTOR/DEVELOPER SHALL PROVIDE NECESSARY CARE FOR PLANTED TREES. 8. REFER TO EROSION AND SEDIMENT CONTROL PLAN FOR REQUIREMENTS PERTAINING TO LANDSCAPING AND SEQUENCING OF WORK.

PROPOSED CONIFEROUS TREE

PROPOSED SHRUBS

₩

0

- FROM ANOTHER TREE: 6 m.

8. REFER TO SITE SERVICING PLAN AND DETAILS FOR REQUIREMENTS AND LOCATIONS RELATED TO SERVICE CONNECTIONS. 9. ROAD ALLOWANCES SHALL BE FINISHED WITH GRASS SEED OR SOD.

₩ SCALE: 1:250 TOP OF BERM : 83.5

 \star

TOTAL 227 UNITS

LANDSCAPE PLAN DRAWING No .: PROJECT No.: 0114 06-18-2024

TREE TO BE REMOVED/RELOCATED



SCHEDULE "L"

COMPOSITE UTILITY PLAN

For the lands set out in Schedule "A", the Owner agrees to implement the objectives and criteria of the Composite Utility Plan (CUP-1 to 3 inclusive), prepared by Advance Engineering Ltd., stamped and dated February 6, 2024; and the Utility Crossing Plans (CR-1, CR-2), prepared by Advance Engineering Ltd., stamped and dated February 6, 2024.

UTILITY SPECIFICATIONS

Wiring for public utilities, to be installed in the area of the Plan of Subdivision herein shall be underground and shall be installed in accordance with specifications approved by the Municipal Official and the applicable utility. Secondary power to the house shall be supplied underground.

Attached:

- Composite Utility Plans (CUP1 to CUP3 inclusive) February 6, 2024
- Utility Crossings (CR1, CR2) June 18, 2024
- KINBG_Lockmaster Mead PH1 (Enbridge) April 8, 2024



9. THE MINIMUM DEPTH OF COVER SHALL BE 0.7 m FOR UNDERGROUND UTILITIES

D, OR TOP	LEGEND:		
	PROPERTY BOUNDARY	DRIVEWAY	
1L	PHASING LIMITS	FENCE	-0
AS	LOT LINE	PROPOSED GAS MAIN	C C
	SETBACK LINE	PROPOSED BELL LINE	——— B ———— B ————
		EXISTING 150mmø PERFORATED SUBDRAIN	SD SD
CTION		EXISTING ROAD DITCH LINE	D
	EXISTING SANITARY SEWER	PROPOSED HANDHOLE FOR TELECOM	B
ERIALS	EXISTING HYDRO LINE	PROPOSED BELL PEDESTAL	•
	EXISTING GAS MAIN GAS GAS GAS GAS	CROSSING – CONCRETE ENCAISED	
EIERMINED	EXISTING BELL LINE	PROPOSED GAS SERVICE	2>>
ITE IS A	PROPOSED WATERMAIN	JOINT UTILITY TRENCH (HYDRO, BELL, CABLE)	
L	PROPOSED FORCEMAIN ── ─ ───── FM ─────	DENOTES NUMBER OF UTILITY DUCTS	2H, 1B, 1C
1.2 m, THE	PROPOSED SANITARY SEWER	1 PHASE PAD-MOUNTED TRANSFORMER 16 KV (10) U) 🔺
	PROPOSED STORM SEWER ———————————————————————————————————	SERVICE ENTRANCE HYDRO BELL CABLE	
	PROPOSED SANITARY MANHOLE 1200mm (S)	3 PHASE KIOSK (2 11)	
PROVIDED	EXISTING SANITARY MANHOLE	J FHASE RIUSK (2 U)	
S, THE	PROPOSED STORM MANHOLE $\overline{\mathbb{O}}$	3 PHASE PAD–MOUNTED TRANSFORMER (1 U)	
ANDARD	EXISTING STORM (DRAINAGE) MANHOLE		
ITILITY	PROPOSED CATCH BASIN 600 x 600	END WALL BOX	
	PROPOSED REAR YARD CATCH BASIN	HYDRO POLE	HPO
AND	EXISTING CULVERT	HYDRU POLE C/W GUY WIRE	(HP)
	PROPOSED TREE .	STREET LIGHT CABLE	SL
ON AND		STREET LIGHT DISCONNECT	SD "
	PROPOSED WATER VALVE & BOX	STREET LIGHT POLE & GROUND WIRE	×
	EXISTING WATER VALVE	COMMUNITY MAILBOX	
	PROPOSED FIRE HYDRANT 🛛 🎯		



DIRECT BURIED, OR TOP			·····]
LOCATED IN THE			
	PHASING LIMITS	FENCE — —	-00
ID OPSD AND AS	LOT LINE	PROPOSED GAS MAIN	G G
MENTS.	SETBACK LINE	PROPOSED BELL LINE	—— В ——— В ——
NCE WITH THE	EASEMENT	EXISTING 150mmø PERFORATED SUBDRAIN –	
1 AS WELL AS	EXISTING WATERMAIN EX WM	EXISTING ROAD DITCH LINE	D
	EXISTING SANITARY SEWER ———————————————————————————————————	PROPOSED HANDHOLE FOR TELECOM	🛛 🖪
ND COVER MATERIALS	EXISTING HYDRO LINE	PROPOSED BELL PEDESTAL	
ND MECHANICALLY	EXISTING GAS MAIN ————————————————————————————————————	CROSSING – CONCRETE ENCAISED	
DENSITI AS DETERMINED	EXISTING BELL LINE	PROPOSED GAS SERVICE	2>>
UGHOUT THE SITE IS A	PROPOSED WATERMAIN	JOINT UTILITY TRENCH (HYDRO, BELL, CABLE)	
SUCH, NORMAL	PROPOSED FORCEMAIN	DENOTES NUMBER OF UTILITY DUCTS	2H, 1B, 1C
E.	PROPOSED SANITARY SEWER ———————————————————————————————————	1 PHASE PAD-MOUNTED TRANSFORMER 16 KV (10 U	J)
50 mm OF GRANULAR	PROPOSED STORM SEWER ── ► ───── stm ─────	SERVICE ENTRANCE HYDRO, BELL, CABLE	
	PROPOSED SANITARY MANHOLE 1200mm	3 PHASE KIOSK (2 U)	
HE TRENCHES, PROVIDED	EXISTING SANITARY MANHOLE		
THE ROADWAYS, THE TS TO 95% STANDARD	PROPOSED STORM MANHOLE	3 PHASE PAD-MOUNTED TRANSFORMER (1 U)	
	EXISTING STORM (DRAINAGE) MANHOLE		Л
SO THAT THE UTILITY	PROPOSED CATCH BASIN 600 x 600		
ACED.	PROPOSED REAR YARD CATCH BASIN		
VERT ACCESS AND	EXISTING CULVERT	HIDRO FOLE C/W GUT WIRE	C HP
	PROPOSED TREE	STREET LIGHT CABLE -	SL
THE EXCAVATION AND	\/ 9 -D	STREET LIGHT DISCONNECT	SD Ű
	PROPOSED WATER VALVE & BOX	STREET LIGHT POLE & GROUND WIRE	×—×
	EXISTING WATER VALVE		

5	TOWNSHIP COMMENTS
4	TOWNSHIP COMMENTS JUNE 30, 2
3	TOWNSHIP COMMENTS
2	TOWNSHIP COMMENTS
1	INITIAL SUBMISSION
No.	REVISION / ISSUE
PREP	ARED BY:
Mo Pho Ema	ngi Mabrouk P.Eng. one: 613-896-9170 ail: eng.services.ca@gmail.com
	ENGINEERING
PRO	JECT NAME AND ADDRESS:
M	LOCKMASTE IEADOW SUBE 95 LOTS
CO	UNTY ROAD No. 22 (S

APPLICANT:

Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata, ON 613-282-5601



DATE 02-06-2024





REVISED: JUNE 2021



UNDERGROUND DISTRIBUTION STANDARDS - INTERIM.... 3D - DESIGN GUIDE SINGLE-PHASE DISTRIBUTION

R04 🍉

Hydro One ..

B	MII etween HONI Dis	NIMUM HC stribution E	Table 1 DRIZONT quipment	B AL CLEA (<50 kV) &	RANCES & Other Pl	ant/Struct	ures
	Separation (mm)						
		U	nderground	•		Overhead	
		Primary & Secondary Cables/Ducts	Pad-mounted Equipment (Foundation)			Conductor	Conductor
Other 2	Plant/Structures		Access side	Non-access Sides	Pole (below grade)	0-0.75kV (note 3)	0.751-50kV (note 3)
	Water Line	300	300	300	600	-	-
Water Plant	Valve Box / Chamber	300	300 ¹	300 ¹	600	-	_
	Hydrant	300	3000	1000	1000	-	-
	Sewer Line	300	300	300	600	-	-
Sewer Plant	Catch Basin	300	300 ¹	300 ¹	600	-	-
	Manhole	300	300 ¹	300 ¹	600	-	-
Gas	Gas Line	300 ⁴	300	300	600	-	-
	Pole/Mast/Pillar	600	3000	1000	3000	1000	1000
Troffic /	Cable or Duct	300	300	300	600	-	-
Street	Joint Use Pole	600	3000	1000	3000	1000	1000
Lighting	U/G Vault / Hand- hole	300	300 ¹	300 ¹	1000	-	-
	Control Pedestal	300	3000	150 ⁵	1000	-	-
	Pedestal	300	3000	150 ⁵	1000	-	-
Comm.	Cable (Direct Buried / Joint- Use Trench)	300 / 0 ²	300	300	600	-	-
	U/G Vault / Hand- hole	300	300 ¹	300 ¹	1000	-	-
Miso	Tree (Direct Buried / Duct)	1000 / 300	3000	3000	3000	10	1000
141150.	Building/Structure Foundation ⁶	300	3000	1000	5000	-	-

¹ The specified clearance is to the outside of the ground grid of the pad-mounted equipment. ²Only applicable in a joint-use trench when there is 300 mm of vertical separation between the communication and supply cables.

³ Overhead conductors are in full position of horizontal swing as calculated in DL6-109. ⁴Zero horizontal separation is allowed during cable crossing if there is 300 mm vertical clearance.

⁵ Communication pedestals located within 3 m of pad-mounted supply equipment shall be bonded to the ground grid. See DU-03-214 for details.

^b Measured from the nearest extent of the structure including footings and any associated drainage components. Note: The clearances are measured from the surface of the listed equipment to the closest surface of the other.

- 8 -

...2011 Edition



02-06-2024



UTILITY CROSSING TABLE					
POINT #	TOP NETWORK	BOTTOM NETWORK	TOP ELVATION	BOTTOM ELEVATION	ELEVATION DIFFERENCE
1	114-2-STM-1	114-2-SAN	82.71	82.23	0.482 m
2	114-2-STM-1	114-2-WM	82.69	82.33	0.361 m
3	114-2-SAN	114-2-WM	82.88	82.45	0.435 m
4	114-2-STM-1	114-2-SAN	82.55	82.00	0.555 m
5	114-2-STM-1	114-2-WM	82.60	81.94	0.663 m
6	114-2-WM	114-2-STM-1	82.16	82.07	0.096 m
7	114-2-WM	114-2-SAN	82.17	81.34	0.830 m
8	114-2-STM-1	114-2-SAN	82.01	81.26	0.756 m
9	114-2-STM-1	114-2-WM	82.05	81.55	0.496 m
10	114-2-WM	114-2-STM-1	81.83	81.87	-0.039 m
11	114-2-WM	114-2-SAN	81.84	80.81	1.035 m
12	114-2-STM-1	114-2-SAN	81.26	80.42	0.833 m
13	114-2-STM-1	114-2-WM	81.29	80.52	0.762 m
14	114-2-STM-1	114-2-FM	81.05	80.42	0.636 m
15	114-2-STM-1	114-2-SAN	81.15	79.92	1.232 m
16	114-2-STM-1	114-2-WM	81.18	79.91	1.271 m
17	114-2-STM-1	114-2-WM	80.10	79.48	0.618 m
18	114-2-WM	114-2-SAN	79.27	79.24	0.031 m
19	114-2-FM	114-2-WM	79.81	79.49	0.320 m
20	114-2-STM-1	114-2-FM	80.40	79.93	0.468 m
21	114-2-STM-1	114-2-FM	79.87	79.72	0.147 m
22	114-2-STM-1	114-2-SAN	80.12	79.14	0.979 m

UTILITY CROSSING TABLE					
POINT #	TOP NETWORK	BOTTOM NETWORK	TOP ELVATION	BOTTOM ELEVATION	ELEVATION DIFFERENCE
23	114-2-WM	114-2-SAN	80.57	80.42	0.153 m
24	114-2-STM-1	114-2-WM	81.24	80.69	0.550 m
25	114-2-STM-1	114-2-SAN	81.23	80.31	0.917 m
26	114-2-WM	114-2-SAN	79.73	79.68	0.048 m
27	114-2-STM-1	114-2-WM	80.48	79.93	0.545 m



NOTES:

- 1. VERTICAL CLEARANCES: 0.5 m BARREL TO BARREL WHEN WATERMAIN IS UNDER SEWER AND 0.25 m WHEN WATERMAIN IS ABOVE.
- 2. FOR WATERMAIN, THE MINIMUM DISTANCE FROM PIPE JOINTS TO THE INTERSECTION SHALL BE 3 m.
- 3. WHEN CROSSING EXISTING PIPES, THE NEW PIPE SHALL BE POSITIONED SO THAT ITS JOINTS ARE AT EQUAL DISTANCES FROM THE CROSSED PIPE.
- 4. FOR NEW CROSSINGS, BOTH PIPES SHALL BE INTERSECTED AT THEIR MID-LENGTHS AT THE CROSSING POINT.
- 5. PROVIDE THRUST BLOCKS FOR WATERMAIN AS SPECIFIED.

PIPE CROSSING DETAIL - JOINTS

SCALE: 1:50

PROJECT NAME AND ADDRESS: LOCKMASTER'S MEADOW SUBDIVISION	DRAWING TITLE
CARDINAL	

NOTES:

1- FOR CROSSINGS INVOLVING WATERMAIN, FOLLOW WATERMAIN TOP ELEVATIONS IN PROFILE VIEWS AS THE VALUES SHOWN IN THE CROSSING TABLE CONSIDER THE WATERMAIN A STRAIGHT LINE. 2- JOINT UTILITY TRENCH IS GENERALLY CONSTRUCTED ABOVE SEWER AND WATERMAIN PIPES. 3- SERVICE LATERALS ARE TO BE ADJUSTED ON FIELD. CONTRACTOR SHALL RECORD ALL SERVICE ELEVATIONS AT PROPERTY LINES. 4- CATCHBASIN LEADS ARE TO BE INSTALLED ABOVE WATERMAIN AND SEWER MAIN. 5- CROSSINGS OVER EXISTING PIPES TO BE AS PER OPSD.

114-2-WM: PROPOSED WATERMAIN 114-2-STM-1: PROPOSED STORM SEWER 114-2-SAN: PROPOSED SANITARY SEWER 114-2-FM: PROPOSED FORCE MAIN

<u>:</u>	SCALE:	DRAWING No .:
ITY CROSSINGS	N/A	(D)
	DATE:	
	06-18-2024	
	00-10-2024	









SCHEDULE "M"

RAIL NOISE ASSESSMENT

For the lands set out in Schedule "A", the Owner agrees to implement the objectives and criteria of the Rail Noise Assessment, prepared by Gradient Wind, stamped and dated November 23, 2024.

Attached:

• Rail Noise Assessment November 24, 2023

ENGINEERS & SCIENTISTS





GRADIENT WIND REPORT: 21-139 – Rail Noise R2

November 24th, 2023

PREPARED FOR Edwardsburgh Developments Ltd. 434-300 Earl Grey Drive Kanata, ON K2T 1C1

PREPARED BY

Adam Bonello, B.Eng., Junior Environmental Scientist Joshua Foster, P.Eng., Lead Engineer

127 WALGREEN ROAD, OTTAWA, ON, CANADA KOA 1L0 | 613 836 0934 GRADIENTWIND.COM Page 391 of 465

EXECUTIVE SUMMARY

This report describes a rail noise assessment performed for a proposed residential development located off Shanly Road in Cardinal, Ontario. The development comprises of 95 lots for single-family households. A CN railway corridor approximately 175m Northwest is the major noise source for the development. Figure 1 illustrates a complete site plan with surrounding context.

The assessment is based on (i) theoretical noise prediction methods that conform to the Ministry of the Environment, Conservation and Parks (MECP); (ii) noise level criteria as specified by the MECP NPC-300 guidelines; (iii) rail traffic volumes corresponding to data obtained from CN; and (iv) site and grading plans received October 2023.

This report revision was issued to address the comments from the peer reviewer Jade Acoustics and is based on the grading package in October 2023. This report replaces Gradient Wind's previous submission (GW21-139 Rail Noise Assessment, dated October 10th, 2022)

The results of the current analysis indicate that noise levels will range between 53 and 60 dBA during the daytime period (07:00-23:00) and the nighttime period (23:00-07:00). The highest noise level (i.e., 60 dBA) occurs at the North façade of the development's Northernmost row of houses, which are nearest and most exposed to the CN railway.

The noise levels predicted due to railway traffic exceed the criteria listed in Section 4.2 for building components at certain houses, therefore, upgraded building components will be required as illustrated in Figure 4. Noise levels at the outdoor living areas (OLA) reach up to 59 dBA, since they fall below 60 dBA no further mitigation is required for these areas. Additionally, a Type A Warning Clause will be required on Lease, Purchase and Sale Agreements as specified in Figure 4 and Table 4.

Results of the calculations indicate that some buildings in the development experience noise levels at the Pane of Window which exceed 55 dBA. These buildings will require forced air heating with provisions for central air conditioning which will allow occupants to keep windows closed and maintain a comfortable living environment at their discretion. Additionally, Type C Warning Clauses will also be required in all



Lease, Purchase and Sale Agreements as summarized in Section 6. A CN specific Warning Clause is also required on all buildings within 300 m of the CN railway as seen in Figure 5.

With respect to stationary noise impacts from the buildings on the surroundings and the building itself, since the development comprises of single-family homes no rooftop HVAC equipment is expected therefore no stationary noise impacts are expected. The surroundings of the site include residential buildings and farm fields. As such, there are no significant existing stationary noise sources impacting the site.

Since all buildings in the development have a setback distance from the rail tracks greater than 75m, a vibration analysis is not required.

TABLE OF CONTENTS

1. INTRODUCTION
2. TERMS OF REFERENCE
3. OBJECTIVES
4. METHODOLOGY2
4.1 Background2
4.2 Rail Noise2
4.2.1 Criteria for Rail Traffic Noise2
4.2.2 Theoretical Railway Noise Predictions4
4.2.3 Railway Traffic Volumes4
4.3 Indoor Noise Calculations
5. ENVIRONMENTAL NOISE RESULTS
5.1 Railway Traffic Noise Levels
5.2 Noise Control Measures7
5.3 Noise Barrier Calculation9
6. DISCUSSION, CONCLUSIONS AND RECOMMENDATIONS
FIGURES APPENDICES

Appendix A – Rail Traffic Data Appendix B – STAMSON 5.04 Input and Output Data and Supporting Information Appendix C – BPN 56 Window STC Calculations



1. INTRODUCTION

Gradient Wind Engineering Inc. (Gradient Wind) was retained by Edwardsburgh Developments Inc. to undertake a rail noise assessment for the proposed residential development located off Shanly Road in Cardinal, Ontario. This report summarizes the methodology, results, and recommendations related to the assessment of exterior noise levels generated by local train traffic. This report has been updated to address peer reviewer comments prepared by Jade Acoustics in their memo dated October 27th, 2023.

This assessment is based on theoretical noise calculation methods conforming to the Ministry of the Environment, Conservation and Parks (MECP)¹ guidelines. Noise calculations were based on draft site plans dated November 2020, grading drawings received November 2023, with future rail traffic volumes corresponding to data obtained from CN.

2. TERMS OF REFERENCE

The focus of this rail noise assessment is a proposed residential development located off Shanly Road in Cardinal, ON. The development is directly south of an existing CN railway. The development will comprise of 95, two-storey, single-family homes, and an earth berm along the north side of the proposed lots, obstructing the line-of-sight to the railway. On the far north of the site is a storm water management pond which will buffer the development from the railway. Figure 1 illustrates a complete site plan with surrounding context.

The source of rail noise is the CN railway directly North of the proposed development. Shanly Road is located directly east of the proposed development, however, traffic volumes on this roadway are low enough to neglect it as a noise source. Since the proposed buildings are greater than 75 m from the CN railway, a vibration assessment is not required as per *Guidelines for New Development in Proximity to Railway Operations*².



¹ Ontario Ministry of the Environment and Climate Change – Environmental Noise Guidelines, Publication NPC-300, Queens Pri nter for Ontario, Toronto, 2013

² Dialog and J.E. Coulter Associates Limited, prepared for The Federation of Canadian Municipalities and The Railway Association of Canada, May 2013
3. **OBJECTIVES**

The principal objectives of this study are to (i) calculate the future noise levels on the study building produced by rail traffic, and (ii) determine whether exterior noise levels exceed the allowable limits specified by the MECP Noise Control Guidelines – NPC-300 as outlined in Section 4.2 of this report.

4. METHODOLOGY

4.1 Background

Noise can be defined as any obtrusive sound. It is created at a source, transmitted through a medium, such as air, and intercepted by a receiver. Noise may be characterized in terms of the power of the source or the sound pressure at a specific distance. While the power of a source is characteristic of that particular source, the sound pressure depends on the location of the receiver and the path that the noise takes to reach the receiver. Measurement of noise is based on the decibel unit, dBA, which is a logarithmic ratio referenced to a standard noise level (2*10⁻⁵ Pascals). The 'A' suffix refers to a weighting scale, which better represents how the noise is perceived by the human ear. With this scale, a doubling of power results in a 3 dBA increase in measured noise levels and is just perceptible to most people. An increase of 10 dBA is often perceived to be twice as loud.

4.2 Rail Noise

4.2.1 Criteria for Rail Traffic Noise

For rail traffic, the equivalent sound energy level, L_{eq} , provides a measure of the time varying noise levels, which is well correlated with the annoyance of sound. It is defined as the continuous sound level, which has the same energy as a time varying noise level over a period of time. For railway noise, the L_{eq} is commonly calculated on the basis of a 16-hour (L_{eq16}) daytime (07:00-23:00) / 8-hour (L_{eq8}) nighttime (23:00-07:00) split to assess its impact on residential buildings. The NPC-300 guidelines specify that the recommended indoor noise limit ranges (that are relevant to this study) are 40 and 35 dBA for living rooms, and sleeping quarters, respectively, as listed in Table 1.

TABLE 1: INDOOR SOUND LEVEL CRITERIA (RAIL)³

Type of Space	Time Period	L _{eq} (dBA)
General offices, reception areas, retail stores, etc.	07:00 - 23:00	45
Living/dining/den areas of residences, hospitals, schools , nursing/retirement homes, day-care centres, theatres, places of worship, libraries, individual or semi-private offices, conference rooms, etc.	07:00 – 23:00	40
Sleeping quarters of hotels/motels	23:00 - 07:00	40
Sleeping quarters of residences, hospitals, nursing/retirement homes, etc.	23:00 - 07:00	35

Predicted noise levels at the plane of window (POW) dictate the action required to achieve the recommended sound levels. An open window is considered to provide a 10 dBA reduction in noise, while a standard closed window is capable of providing a minimum 20 dBA noise reduction⁴. A closed window due to a ventilation requirement will bring noise levels down to achieve an acceptable indoor environment⁵. If the nighttime sound level outside the bedroom or living/dining room windows exceeds 55 dBA or the daytime sound level outside the bedroom or living/dining area windows exceeds 60 dBA, building components including windows, walls and doors, where applicable, need to be designed so that the indoor sound levels comply with the sound level limits in Table 1.

The sound level criterion for outdoor living areas (OLA) is 55 dBA, which applies during the daytime (07:00 to 23:00). When noise levels exceed 55 dBA, mitigation should be provided to reduce noise levels where technically and administratively feasible to acceptable levels at or below the criterion. When noise levels at the OLA exceed 60 dBA mitigation must be provided.



³ Adapted from ENCG 2016 – Tables 2.2b and 2.2c

⁴ Burberry, P.B. (2014). Mitchell's Environment and Services. Routledge, Page 125

⁵ MECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.8

4.2.2 Theoretical Railway Noise Predictions

Calculations were performed in MECP's STAMSON software using STEAM (Sound from Trains Environmental Analysis Method) to determine railway noise impact on the study site. Calculations were performed by treating the rail segment as a linear source of noise, and by using existing building locations as noise barriers. In addition to the railway traffic volumes summarized in Table 2, theoretical noise predictions were based on the following parameters:

- The ground surface was modelled as absorptive where grass and foliage (soft ground) are present, and as reflective where pavement and concrete are present (hard ground).
- Noise receptors were strategically placed at five (5) locations at the façades as Plane of Window (POW) receptors at the highest levels of the buildings.
- Buildings were assumed to be 2-storeys tall with a height of 6 m.
- Three (3) receptor location were chosen as OLA receptors located in backyards.
- The location of the receptors are illustrated in Figure 2.
- Rail lines were taken as welded.
- Earth Berm will be 2.5m tall (above local grade). Initial calculations were made which did not consider the benefit of the berm.
- Railway is assumed to be 1.7m above local grade.

The rail bed is approximately the same height as the base of the utility poles with have an average grade of 81.3m as shown on the grading plan. The top of rail is to be confirmed by survey during the design phase of the subdivision. Top of rail expected to be \approx 0.3m higher than rail bed at 81.6m.

4.2.3 Railway Traffic Volumes

The CN Railway line is located to the North of the development, as shown in Figure 1. This railway line serves 3 train types: freight, way freight, and passenger trains. NPC-300 dictates that noise calculations should consider future sound levels based on a railway's classification at the mature state of development. As a result, the ultimate AADT volumes are based on train count data provided by CN Railway (dated July of 2021), with a 2.5% growth rate applied for 10 years from the date of the project (2023). Table 2

summarizes the railway traffic values used for each railway segment, the number of cars, the maximum speed and the number of locomotives included in this assessment. CN Railway data can be found in Appendix A.

Train Type	Projected 2031 Traffic Volumes	Speed Limit (km/h)	Number of Locomotives	Number of Cars
Freight	16/9*	89	4	140
Way Freight	1/0*	89	4	25
Passenger	15/0*	105	2	10

TABLE 2: EXTERIOR NOISE LEVELS DUE TO TRANSPORTATION SOURCES

* Projected 2033 AADT daytime/nighttime rail traffic volumes

4.3 Indoor Noise Calculations

The difference between outdoor and indoor noise levels is the noise attenuation provided by the building envelope. According to common industry practice, complete walls and individual wall elements are rated according to the Sound Transmission Class (STC). The STC ratings of common residential walls built in conformance with the Ontario Building Code (2020) typically exceed STC 35, depending on exterior cladding, thickness and interior finish details. For example, brick veneer walls can achieve STC 50 or more. Standard commercially sided exterior metal stud walls have around STC 45. Standard good quality double-glazed non-operable windows can have STC ratings ranging from 25 to 40, depending on the window manufacturer, pane thickness and inter-pane spacing. The windows are usually the known weak point in a partition.

As per Section 4.2, when daytime noise levels (from rail sources) at the plane of the window exceed 60 dBA daytime and 55 dBA nighttime, calculations must be performed to evaluate the sound transmission quality of the building components to ensure acceptable indoor noise levels. The calculation procedure⁶ considers:

• Window type and total area as a percentage of total room floor area



⁶ EN 12354-3:2000 "Building Acoustics - Estimation of acoustic performance of buildings from the performance of elements - Part 3: Airborne sound insulation against outdoor sound"

- Exterior wall type and total area as a percentage of the total room floor area
- Acoustic absorption characteristics of the room
- Outdoor noise source type and approach geometry
- Indoor sound level criteria, which varies according to the intended use of a space.

Based on published research⁷, exterior walls possess specific sound attenuation characteristics that are used as a basis for calculating the required STC ratings of windows in the same partition. Window STC calculations have therefore been based on the following assumptions:

- Bedrooms are assumed to be very absorptive (1.25 absorption coefficient), while living rooms are assumed to have an intermediate level of absorption (0.8 absorption coefficient).
- Exterior walls will have a minimum STC 45
- Room, window, and wall dimensions are based on the following assumptions, as detailed floor plans are not yet available:
 - Typical bedroom window is 3 m x 3 m and typical living rom is 3 m x 4 m.
 - Window will be 70% of the wall area.

STC calculations were performed based on the method developed by the National Research Council in their Building Practice Note # 56⁸.

5. ENVIRONMENTAL NOISE RESULTS

5.1 Railway Traffic Noise Levels

The results of the current analysis indicate that noise levels will range between 53 and 60 dBA during the daytime period (07:00-23:00) and the nighttime period (23:00-07:00). The highest noise level (i.e., 60 dBA) occurs at the North façade of the development's Northernmost row of houses, which are nearest and most exposed to the CN railway. Noise levels in the OLA are taken without the benefit of the berm. Details of the STAMSON calculations can be found in Appendix B.



⁷ CMHC, Road & Rail Noise: Effects on Housing

⁸ Quirt, J.D. Controlling Sound Transmission into Buildings, National Research Council of Canada, Ottawa September 1985

Receptor	Receptor Height Above	eceptor Height Above Receptor Location		loise Level BA)
Number	Grade (m)		Day	Night
1	4.5	POW – North Façade – Lot 68	53	53
2	4.5	POW – North Façade – Lot 46	57	56
3	4.5	POW – North Façade – 47	60	60
4	4.5	POW – East Façade – Lot 52	57	56
5	4.5	POW – North Façade – Lot 1	57	57
6	1.5	OLA – Backyard – Lot 46	56	N/A*
7	1.5	OLA – Backyard – Lot 49	59	N/A*
8	1.5	OLA – Backyard – Lot 52	59	N/A*

TABLE 3: EXTERIOR NOISE LEVELS DUE TO TRANSPORTATION SOURCES

*Nighttime noise levels at OLA receptors are not considered as per NPC-300.

5.2 Noise Control Measures

The noise levels predicted due to railway traffic exceed the criteria listed in Section 4.2 for building components. As discussed, the STC requirements for windows have been determined based on preliminary STC calculations, utilizing the methodology described in the NRC Building Practice Note #56. Details of these calculations, can be found in Appendix C. The STC requirements for the windows are summarized below for various lots within the development (see Figure 4), façades not listed do not require upgraded building components. Furthermore, the North facing facades where noise levels do not exceed the criteria listed in Section 4.2, standard building components combined with Ontario Building Code (OBC) requirements will be sufficient. The STC requirements for the windows are summarized below for various units within the development (see Figure 4):

Bedroom Windows

- (i) Bedroom windows facing North, East, West for lots 47-52 will require a minimum STC of 30.
- (ii) Bedroom windows facing North for lots 46 and 1 will require a minimum STC of 30.
- (iii) All other bedroom windows are to satisfy Ontario Building Code (OBC 2020) requirements.



• Living Room Windows

- (i) Bedroom windows facing North, East, West for lots 47-52 will require a minimum STC of 30.
- (ii) Bedroom windows facing North for lots 46 and 1 will require a minimum STC of 30.
- (iii) All living room windows are to satisfy Ontario Building Code (OBC 2020) requirements.
- Exterior Walls
- (i) Exterior wall components on North façades will require a minimum STC of 45, which will be achieved with brick cladding or an acoustical equivalent according to NRC test data⁹.

The STC requirements apply to windows, doors, and window wall elements. A review of window supplier literature indicates that the specified STC ratings can be achieved by a variety of window systems having a combination of glass thickness and inter-pane spacing will offer the necessary sound attenuation rating. It is the responsibility of the manufacturer to ensure that the specified window achieves the required STC. This can only be assured by using window configurations that have been certified by laboratory testing. The requirements for STC ratings assume that the remaining components of the building are constructed and installed according to the minimum standards of the Ontario Building Code (OBC). The specified STC requirements also apply to swinging and/or sliding patio doors.

Results of the calculations also indicate that the development will require forced air heating with provisions for central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment at their discretion. In addition to ventilation requirements, Warning Clauses will also be required in all Lease, Purchase and Sale Agreements, as summarized in Section 6. Table 4 summarizes the required Warning Clause and mitigation measures for each lot.



⁹ J.S. Bradley and J.A. Birta. Laboratory Measurements of the Sound Insulation of Building Façade Elements, National Research Council October 2000.

TABLE 4: NOISE CONTROL MEASURES

	Minimum STC requirements				
Lot #	Window	Wall	Warning Clause	Ventilation	
1, 47-52	30	45	Type C, Type A, & CN	Forced Air Heating with AC provisions	
46	30	45	Type C, & CN	Forced Air Heating with AC provisions	
2-6, 41-45, 53-56, 62-70	OBC	OBC	CN	N/A	

5.3 Noise Barrier Calculation

A noise barrier investigation was carried out to find the benefit of noise level reduction of applying a 2.5m tall earth berm located between the north sides of lots 47-52. The table below outlines the resultant noise levels with the berm.

Receptor	Receptor Height	Receptor Location	Daytime L _{eq} Nois	e Levels (dBA)
Number	Above Grade (m)		Without berm	With berm
6	1.5	OLA – Backyard – Lot 46	56	55
7	1.5	OLA – Backyard – Lot 49	59	56
8	1.5	OLA – Backyard – Lot 52	59	59

TABLE 5: NOISE BARRIER INVESTIGATION

Through analysis of the earth berm, the berm will reduce noise levels in the backyard areas of lots 47-51 to more acceptable levels. However, the end lot 52 will not notice any change from the presence of the berm. Due to noise levels exceeding 55 dBA, lots 47-52 and 1 will require a warning clause type A on Lease, Purchase and Sale Agreements, as summarized in Section 6.



6. DISCUSSION, CONCLUSIONS AND RECOMMENDATIONS

The results of the noise study indicate that noise levels at certain houses exceed 55 dBA during the nighttime period (23:00-7:00), therefore, building components with a higher Sound Transmission Class (STC) rating will be required. Noise levels at certain outdoor living areas (OLA) exceed 55 dBA which will require a Warning Clause on all Lease, Purchase and Sale Agreements, as specified in Figure 4.

Results of the calculations also indicate that certain buildings in the development will require forced air heating with provisions for central air conditioning which will allow occupants to keep windows closed and maintain a comfortable living environment at the occupant's discretion, as specified in Figure 4. The following Warning Clauses will also be required to be placed on Lease, Purchase and Sale Agreements, as summarized in Table 4 and Figure 4:

Type C

"This dwelling unit has been designed with the provision for adding central air conditioning at the occupant's discretion. Installation of central air conditioning by the occupant in low and medium density developments will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."

Туре А

"Purchasers/tenants are advised that sound levels due to increasing rail traffic may occasionally interfere with some outdoor activities as the sound levels may exceed the sound level limits of the City and the Ministry of the Environment"

In addition to NPC-300 Warning Clauses the following CN Railway Warning Clause will be required in Lease, Purchase and Sale Agreements for lots within 300m of the railway:

CN Warning Clause:

"Warning: Canadian National Railway Company or its assigns or successors in interest has or have a rights-of-way within 300 metres from the land the subject hereof. There may be alterations to or expansions of the railway facilities on such rights-of-way in the future including the possibility



that the railway or its assigns or successors as aforesaid may expand its operations, which expansion may affect the living environment of the residents in the vicinity, notwithstanding the inclusion of any noise and vibration attenuating measures in the design of the development and individual dwelling(s). CNR will not be responsible for any complaints or claims arising from use of such facilities and/or operations on, over or under the aforesaid rights-of-way."

Off-site stationary noise impacts are not expected to be an issue since houses in the proposed development will not have rooftop HVAC equipment. The immediate surroundings of the site include residential buildings and farm fields. As such, there are no significant existing stationary noise sources impacting the site.

Since all buildings in the development have a setback distance from the rail tracks greater than 75m, a vibration analysis is not required.

Please be advised that prior to issuance of a building permit, a detailed review of the mechanical and architectural building design will be required. Additionally, an inspection of the mitigation measures, such as the earth berm, will be required prior to occupancy.

This concludes rail noise assessment and report. If you have any questions or wish to discuss our findings, please advise us. In the interim, we thank you for the opportunity to be of service.

Sincerely,

Gradient Wind Engineering Inc.

the Belly

Adam Bonello, B.Eng. Junior Environmental Scientist

Gradient Wind Report #21-139 - Rail Noise R2



Joshua Foster, P.Eng. Lead Engineer















APPENDIX A

RAIL TRAFFIC DATA

127 WALGREEN ROAD, OTTAWA, ON, CANADA KOA 1LO [613 836 0934 GRADIENTWIND.COM Page 411 of 465

System Engineering Engineering Services 1 Administration Road Concord, GN, L48 189 Tr. 905 649, 2054 Fr. 905 760, 3406 **Train Count Data** TRANSMITTAL GRADIENTWIND Tb^+_i Project . KNG - 104.96- County Road 22, United Counties Destinatoire | Engineers and of Leeds and Greenville ON Scientists 127 Walgreen Road Ottawa ON KoA 1Lo Caleb Alexander Routing: All he caleb.alexander@gradientwind.com Michael Vallins From: Date: 2021/07/06 Expéditeur ; Adjacent Development Ce: CN via e-mail Urgent 🗌 For Your Use 🗋 For Review 🗋 For Your Information 🗋 Confidential Train Traffic Data - CN Kingston Subdivision near County Road 22 Ren in United Counties of Leeds and Greenville, ON Please find attached the requested Train Traffic Data. The application fee in the amount of \$500.00 +HST will be invoiced. Should you have any questions, please do not hesitate to contact the undersigned at permits.gld@cn.ca.

Sincerely,

Michael Vallins P.Eng Manager, Public Works- Easter Canada Pemits.gld@cn.ca

Train Count Data

Page 1

 ${\bf Date:}\ 2021/07/06 \quad$ Project Number: KNG - 104.96 - County Road 22, UC of Leeds and Greenville ON

Dear Caleb:

Re: Train Traffic Data – CN Kingston Subdivision near County Road 22 in United Counties of Leeds and Greenville, ON

The following is provided in response to Caleb's 2021/06/18 request for information regarding rail traffic in the vicinity of County Road 22 in United Counties of Leeds and Grenville ON at approximately Mile 104.96 on CN's Kingston Subdivision.

Typical daily traffic volumes are recorded below. However, traffic volumes may fluctuate due to overall economic conditions, varying traffic demands, weather conditions, track maintenance programs, statutory holidays and traffic detours that when required may be heavy although temporary. For the purpose of noise and vibration reports, train volumes must be escalated by 2.5% per annum for a 10-year period.

Typical daily traffic volumes at this site location are as follows:

	0700-2300			
Type of Train	Volumes	Max.Consist	Max. Speed	Max. Power
Freight	12	140	55	4
Way Freight	1	25	55	4
Passenger	11	10	65	2

*Maximum train speed is given in Miles per Hour

	2300-0700			
Type of Train	Volumes	Max.Consist	Max. Speed	Max. Power
Freight	7	140	55	4
Way Freight	0	25	55	4
Passenger	0	10	65	2

The volumes recorded reflect westbound and eastbound freight and passenger operations on CN's Kingston Subdivision.

Except where anti-whistling bylaws are in effect, engine-warning whistles and bells are normally sounded at all at-grade crossings. There are two (2) at-grade crossings in the immediate vicinity of the study area at Mile 103.86 Marine Station Road and Mile 105.75 Farm Xing. Anti-Whistling Bylaws are not in effect at these locations. Please note that engine-warning whistles may be sounded in cases of emergency, as a safety and or warning precaution at station locations and pedestrian crossings and occasionally for operating requirements.

With respect to equipment restrictions, the gross weight of the heaviest permissible car is 286,000 lbs.

Page 2

The double mainline track is considered to be continuously welded rail throughout the study area.

The Canadian National Railway continues to be strongly opposed to locating developments near railway facilities and rights-of-way due to potential salety and environmental conflicts. Development adjacent to the Railway Right-of-Way is not appropriate without sound impact mitigation measures to reduce the incompatibility. For confirmation of the applicable rail noise, vibration and safety standards, Adjacent Development, Canadian National Railway Properties at <u>Proximity@cn.ca</u> should be contacted directly.

I trust the above information will satisfy your current request.

Sincerely,

Michael Vallins P.Eng Manager, Public Works- Easter Canada Pemits.gld@en.ca



APPENDIX B

STAMSON INPUT-OUTPUT DATA

127 WALGREEN ROAD, OTTAWA, ON, CANADA KOA 1LO [613 836 0934 GRADIENTWIND.COM Page 415 of 465

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:14:31 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r1.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) _____ Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld _ _ * 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 0.00 ! 0.00 ! 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) -----------Angle1 Angle2 : -90.00 deg 90.00 deg : 0 Wood depth (No woods.) : No of house rows 1 / 1 House density : 80 % : (Absorptive ground surface) Surface 1 Receiver source distance : 226.00 / 226.00 m Receiver height : 4.50 / 4.50 m : 1 (Flat/gentle slope; no barrier) : -82 deg Track 1 Topography Whistle Angle Reference angle : 0.00 Results segment # 1: KNG (day) _____ LOCOMOTIVE (0.00 + 52.38 + 0.00) = 52.38 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.50 76.49 -17.61 -1.17 0.00 -5.34 0.00 52.38 _____ WHEEL (0.00 + 44.02 + 0.00) = 44.02 dBAAnglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

ENGINEERS & SCIENTISTS

90 0.60 69.56 -18.85 -1.35 0.00 -5.34 0.00 44.02 -90 _____ LEFT WHISTLE (0.00 + 25.91 + 0.00) = 25.91 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 0.50 73.89 -17.61 -25.03 0.00 -5.34 0.00 25.91 -84 _____ RIGHT WHISTLE (0.00 + 28.61 + 0.00) = 28.61 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 -79 0.50 73.89 -17.61 -22.33 0.00 -5.34 0.00 28.61 _____ Segment Leg : 53.00 dBA Total Leq All Segments: 53.00 dBA Results segment # 1: KNG (night) _____ LOCOMOTIVE (0.00 + 51.99 + 0.00) = 51.99 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.50 76.10 -17.61 -1.17 0.00 -5.34 0.00 51.99 _____ WHEEL (0.00 + 44.06 + 0.00) = 44.06 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq . _ _ _ _ _ _ _ _ _ _ _ _ _ _____ 90 0.60 69.60 -18.85 -1.35 0.00 -5.34 0.00 44.06 -90 _____ LEFT WHISTLE (0.00 + 23.73 + 0.00) = 23.73 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -84 -82 0.50 71.71 -17.61 -25.03 0.00 -5.34 0.00 23.73 _____ RIGHT WHISTLE (0.00 + 26.43 + 0.00) = 26.43 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _____ -79 0.50 71.71 -17.61 -22.33 0.00 -5.34 0.00 26.43 -82 _____ Segment Leq : 52.65 dBA Total Leg All Segments: 52.65 dBA TOTAL Leg FROM ALL SOURCES (DAY): 53.00 (NIGHT): 52.65

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:15:44 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r2.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) _____ Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ Angle1 Angle2 : -90.00 deg 20.00 deg Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 223.00 / 223.00 m Receiver height:4.50 / 4.50 mTopography:1 (Flat 1 (Flat/gentle slope; no barrier) -82 deg Track 1 : Whistle Angle : 0.00 Reference angle Results segment # 1: KNG (day) LOCOMOTIVE (0.00 + 55.89 + 0.00) = 55.89 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 20 0.50 76.49 -17.52 -3.08 0.00 0.00 0.00 55.89 _____ WHEEL (0.00 + 47.58 + 0.00) = 47.58 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 20 0.60 69.56 -18.76 -3.23 0.00 0.00 0.00 47.58

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 418 of 465

LEFT WHISTLE (0.00 + 31.37 + 0.00) = 31.37 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 0.50 73.89 -17.52 -24.99 0.00 0.00 0.00 31.37 -84 _____ RIGHT WHISTLE (0.00 + 34.11 + 0.00) = 34.11 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 -79 0.50 73.89 -17.52 -22.25 0.00 0.00 0.00 34.11 _____ Segment Leg : 56.53 dBA Total Leq All Segments: 56.53 dBA Results segment # 1: KNG (night) _____ LOCOMOTIVE (0.00 + 55.50 + 0.00) = 55.50 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 20 0.50 76.10 -17.52 -3.08 0.00 0.00 0.00 55.50 WHEEL (0.00 + 47.62 + 0.00) = 47.62 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _____ -90 20 0.60 69.60 -18.76 -3.23 0.00 0.00 0.00 47.62 _____ LEFT WHISTLE (0.00 + 29.20 + 0.00) = 29.20 dBA Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg _____ -84 -82 0.50 71.71 -17.52 -24.99 0.00 0.00 0.00 29.20 _____ RIGHT WHISTLE (0.00 + 31.94 + 0.00) = 31.94 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq ------82 -79 0.50 71.71 -17.52 -22.25 0.00 0.00 0.00 31.94 _____ Segment Leq : 56.18 dBA Total Leg All Segments: 56.18 dBA TOTAL Leq FROM ALL SOURCES (DAY): 56.53 (NIGHT): 56.18

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:17:39 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r3.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) _____ Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 174.00 / 174.00 m Receiver height:4.50 / 4.50 mTopography:1 (Flat 1 (Flat/gentle slope; no barrier) -82 deg Track 1 Whistle Angle : : 0.00 Reference angle Results segment # 1: KNG (day) LOCOMOTIVE (0.00 + 59.41 + 0.00) = 59.41 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.50 76.49 -15.91 -1.17 0.00 0.00 0.00 59.41 _____ WHEEL (0.00 + 51.17 + 0.00) = 51.17 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.60 69.56 -17.03 -1.35 0.00 0.00 0.00 51.17

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 420 of 465

_____ LEFT WHISTLE (0.00 + 33.77 + 0.00) = 33.77 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 0.50 73.89 -15.91 -24.20 0.00 0.00 0.00 33.77 -84 _____ RIGHT WHISTLE (0.00 + 37.34 + 0.00) = 37.34 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 -78 0.50 73.89 -15.91 -20.64 0.00 0.00 0.00 37.34 _____ Segment Leg : 60.05 dBA Total Leq All Segments: 60.05 dBA Results segment # 1: KNG (night) _____ LOCOMOTIVE (0.00 + 59.02 + 0.00) = 59.02 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.50 76.10 -15.91 -1.17 0.00 0.00 0.00 59.02 WHEEL (0.00 + 51.22 + 0.00) = 51.22 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ ----_ _ _ _ _ _ _ _ _ _ _ _ _ _ _____ -90 90 0.60 69.60 -17.03 -1.35 0.00 0.00 0.00 51.22 _____ LEFT WHISTLE (0.00 + 31.59 + 0.00) = 31.59 dBA Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg _____ -82 0.50 71.71 -15.91 -24.20 0.00 0.00 0.00 31.59 -84 _____ RIGHT WHISTLE (0.00 + 35.16 + 0.00) = 35.16 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq ------82 -78 0.50 71.71 -15.91 -20.64 0.00 0.00 0.00 35.16 _____ Segment Leq : 59.71 dBA Total Leg All Segments: 59.71 dBA TOTAL Leg FROM ALL SOURCES (DAY): 60.05 (NIGHT): 59.71



ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:18:32 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r4.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) _____ Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ : 0.00 deg 90.00 deg Angle1 Angle2 0 (No woods.) Wood depth : No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 179.00 / 179.00 m Receiver height:4.50 / 4.50 mTopography:1 (Flat 1 (Flat/gentle slope; no barrier) -82 deg Track 1 : Whistle Angle : 0.00 Reference angle Results segment # 1: KNG (day) LOCOMOTIVE (0.00 + 56.22 + 0.00) = 56.22 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ 0 90 0.50 76.49 -16.10 -4.18 0.00 0.00 0.00 56.22 _____ WHEEL (0.00 + 47.97 + 0.00) = 47.97 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ 0 90 0.60 69.56 -17.23 -4.37 0.00 0.00 0.00 47.97

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 422 of 465

ENGINEERS & SCIENTISTS

LEFT WHISTLE (0.00 + 31.59 + 0.00) = 0.00 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq -82 0.00 73.89 0.00 -24.20 0.00 0.00 0.00 31.59 0 _____ Segment Leq : 56.83 dBA Total Leg All Segments: 56.83 dBA Results segment # 1: KNG (night) _____ LOCOMOTIVE (0.00 + 55.83 + 0.00) = 55.83 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _____ _____ 90 0.50 76.10 -16.10 -4.18 0.00 0.00 0.00 55.83 0 _____ WHEEL (0.00 + 48.01 + 0.00) = 48.01 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ 90 0.60 69.60 -17.23 -4.37 0.00 0.00 0.00 48.01 0 _____ LEFT WHISTLE (0.00 + 31.59 + 0.00) = 0.00 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ 0 -82 0.00 71.71 0.00 -24.20 0.00 0.00 0.00 31.59 _____ Segment Leq : 56.49 dBA Total Leq All Segments: 56.49 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 56.83 (NIGHT): 56.49



ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:19:18 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r5.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) _____ Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ Angle1 Angle2 : -42.00 deg 90.00 deg Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 223.00 / 223.00 m Receiver height:4.50 / 4.50 mTopography:1 (Flat 1 (Flat/gentle slope; no barrier) -82 deg Track 1 Whistle Angle : : 0.00 Reference angle Results segment # 1: KNG (day) LOCOMOTIVE (0.00 + 56.79 + 0.00) = 56.79 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -42 90 0.50 76.49 -17.52 -2.18 0.00 0.00 0.00 56.79 _____ WHEEL (0.00 + 48.49 + 0.00) = 48.49 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -42 90 0.60 69.56 -18.76 -2.32 0.00 0.00 0.00 48.49

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 424 of 465

ENGINEERS & SCIENTISTS

LEFT WHISTLE (0.00 + 31.59 + 0.00) = 0.00 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq -42 -82 0.00 73.89 0.00 -24.20 0.00 0.00 0.00 31.59 _____ Segment Leq : 57.39 dBA Total Leg All Segments: 57.39 dBA Results segment # 1: KNG (night) _____ LOCOMOTIVE (0.00 + 56.39 + 0.00) = 56.39 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _____ _____ 90 0.50 76.10 -17.52 -2.18 0.00 0.00 0.00 56.39 -42 _____ WHEEL (0.00 + 48.53 + 0.00) = 48.53 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ 90 0.60 69.60 -18.76 -2.32 0.00 0.00 0.00 48.53 -42 _____ LEFT WHISTLE (0.00 + 31.59 + 0.00) = 0.00 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ -42 -82 0.00 71.71 0.00 -24.20 0.00 0.00 0.00 31.59 _____ Segment Leq : 57.05 dBA Total Leq All Segments: 57.05 dBA TOTAL Leg FROM ALL SOURCES (DAY): 57.39

(NIGHT): 57.05



ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:29:21 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r6.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) _____ Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ Angle1 Angle2 : -90.00 deg 43.00 deg Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 228.00 / 228.00 m Receiver height:1.50 / 1.50 mTopography:1 1 (Flat/gentle slope; no barrier) -82 deg Track 1 : Whistle Angle : 0.00 Reference angle Results segment # 1: KNG (day) LOCOMOTIVE (0.00 + 55.50 + 0.00) = 55.50 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 43 0.58 76.49 -18.73 -2.26 0.00 0.00 0.00 55.50 _____ WHEEL (0.00 + 47.59 + 0.00) = 47.59 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 43 0.66 69.56 -19.62 -2.35 0.00 0.00 0.00 47.59

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 426 of 465

_____ LEFT WHISTLE (0.00 + 29.28 + 0.00) = 29.28 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 0.58 73.89 -18.73 -25.87 0.00 0.00 0.00 29.28 -84 _____ RIGHT WHISTLE (0.00 + 32.06 + 0.00) = 32.06 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 -79 0.58 73.89 -18.73 -23.10 0.00 0.00 0.00 32.06 _____ Segment Leg : 56.18 dBA Total Leq All Segments: 56.18 dBA Results segment # 1: KNG (night) _____ LOCOMOTIVE (0.00 + 55.11 + 0.00) = 55.11 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 43 0.58 76.10 -18.73 -2.26 0.00 0.00 0.00 55.11 WHEEL (0.00 + 47.63 + 0.00) = 47.63 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 43 0.66 69.60 -19.62 -2.35 0.00 0.00 0.00 47.63 _____ LEFT WHISTLE (0.00 + 27.10 + 0.00) = 27.10 dBA Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg _____ -82 0.58 71.71 -18.73 -25.87 0.00 0.00 0.00 27.10 -84 _____ RIGHT WHISTLE (0.00 + 29.88 + 0.00) = 29.88 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq ------82 -79 0.58 71.71 -18.73 -23.10 0.00 0.00 0.00 29.88 _____ Segment Leq : 55.84 dBA Total Leg All Segments: 55.84 dBA TOTAL Leq FROM ALL SOURCES (DAY): 56.18 (NIGHT): 55.84

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:25:48 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r6b.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) -----Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld _ _ 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ Angle1 Angle2 : -90.00 deg 43.00 deg Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 228.00 / 228.00 m Receiver height:1.50 / 1.50 mTopography:2 (Flat : 2 (Flat/gentle slope; with barrier) : -82 deg Track 1 : 0.00 deg Angle2 : 43.00 deg : 2.50 m Whistle Angle Barrier angle1 Barrier height Barrier receiver distance : 109.00 / 109.00 m Source elevation : 81.60 m : 82.67 m Barrier elevation Reference angle Receiver elevation : 82.50 m : 0.00 Results segment # 1: KNG (day) _____ Barrier height for grazing incidence _____ Source ! Receiver ! Barrier ! Elevation of Height (m) ! Height (m) ! Height (m) ! Barrier Top (m) A13

+	+	- – – – + – – – – – – – –				
4.00 ! 1. 0.50 ! 1.	.50 ! 2 .50 ! 0	2.35 !).68 !	84.85 83.18			
1000000000000000000000000000000000000	12 + 0 00) =	54 54 dBA				
Anglel Angle2 Alpha Re	efLeq D.Adj	F.Adj W.Adj	H.Adj E	3.Adj	SubLeq	
-90 0 0.58	76.49 -18.73	-4.34 0.00	0.00	0.00	53.42	
0 43 0.44	76.49 -16.96	-6.40 0.00	0.00 -	-5.01	48.12	
WHEEL (45.47 + 38.65 + Anglel Angle2 Alpha Re	0.00) = 46.29 efLeq D.Adj) dBA F.Adj W.Adj	H.Adj E	3.Adj	SubLeq	
-90 0 0.66 6	59.56 -19.62	-4.47 0.00	0.00	0.00	45.47	
0 43 0.54 6	59.56 -18.20	-6.45 0.00	0.00 -	-6.26	38.65	
LEFT WHISTLE (0.00 + 29 Anglel Angle2 Alpha Re	9.28 + 0.00) = efLeq D.Adj	= 29.28 dBA F.Adj W.Adj	H.Adj E	3.Adj	SubLeq	
-84 -82 0.58	73.89 -18.73 -	-25.87 0.00	0.00	0.00	29.28	
RIGHT WHISTLE (0.00 + 3 Anglel Angle2 Alpha Re	32.06 + 0.00) efLeq D.Adj	= 32.06 dBA F.Adj W.Adj	H.Adj E	3.Adj	SubLeq	
-82 -79 0.58	73.89 -18.73 -	-23.10 0.00	0.00	0.00	32.06	
Segment Leq : 55.18 dBA Total Leq All Segments: 55.18 dBA Results segment # 1: KNG (night)						
Barrier height for graz	zing incidence	2				
Source ! Receiver Height (m) ! Height (! Barrier (m) ! Height	! Elevat: (m) ! Barrier	ion of Top (m)			
4.00 ! 1. 0.50 ! 1.	.50 ! 2 .50 ! 0	2.35 !).68 !	84.85 83.18			
LOCOMOTIVE (53.03 + 47. Angle1 Angle2 Alpha Re	.73 + 0.00) = efLeq D.Adj	54.15 dBA F.Adj W.Adj	H.Adj E	3.Adj	SubLeq	
-90 0 0.58	76.10 -18.73	-4.34 0.00	0.00	0.00	53.03	
0 43 0.44	76.10 -16.96	-6.40 0.00	0.00 -	-5.01	47.73	

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 429 of 465

ENGINEERS & SCIENTISTS

WHEEL (45.52 + 38.70 + 0.00) = 46.34 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _ _ _ _ _ _ _ ------90 0 0.66 69.60 -19.62 -4.47 0.00 0.00 0.00 45.52 _____ 0 43 0.54 69.60 -18.20 -6.45 0.00 0.00 -6.26 38.70 _____ LEFT WHISTLE (0.00 + 27.10 + 0.00) = 27.10 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -84 -82 0.58 71.71 -18.73 -25.87 0.00 0.00 0.00 27.10 _____ RIGHT WHISTLE (0.00 + 29.88 + 0.00) = 29.88 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -79 0.58 71.71 -18.73 -23.10 0.00 0.00 0.00 29.88 -82 _____ Segment Leq : 54.84 dBA Total Leq All Segments: 54.84 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 55.18 (NIGHT): 54.84



ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:34:38 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r7.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) _____ Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 169.00 / 169.00 m Receiver height:1.50 / 1.50 mTopography:1 1 (Flat/gentle slope; no barrier) -82 deg Track 1 : Whistle Angle : 0.00 Reference angle Results segment # 1: KNG (day) LOCOMOTIVE (0.00 + 58.49 + 0.00) = 58.49 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.58 76.49 -16.67 -1.33 0.00 0.00 0.00 58.49 _____ WHEEL (0.00 + 50.64 + 0.00) = 50.64 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.66 69.56 -17.46 -1.46 0.00 0.00 0.00 50.64

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 431 of 465
_____ LEFT WHISTLE (0.00 + 32.28 + 0.00) = 32.28 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 0.58 73.89 -16.67 -24.93 0.00 0.00 0.00 32.28 -84 _____ RIGHT WHISTLE (0.00 + 36.10 + 0.00) = 36.10 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 -78 0.58 73.89 -16.67 -21.12 0.00 0.00 0.00 36.10 _____ Segment Leg : 59.18 dBA Total Leq All Segments: 59.18 dBA Results segment # 1: KNG (night) _____ LOCOMOTIVE (0.00 + 58.10 + 0.00) = 58.10 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.58 76.10 -16.67 -1.33 0.00 0.00 0.00 58.10 WHEEL (0.00 + 50.69 + 0.00) = 50.69 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _ _ _ _ _ _ _____ -90 90 0.66 69.60 -17.46 -1.46 0.00 0.00 0.00 50.69 _____ LEFT WHISTLE (0.00 + 30.10 + 0.00) = 30.10 dBA Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg _____ -84 -82 0.58 71.71 -16.67 -24.93 0.00 0.00 0.00 30.10 _____ RIGHT WHISTLE (0.00 + 33.92 + 0.00) = 33.92 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq ------82 -78 0.58 71.71 -16.67 -21.12 0.00 0.00 0.00 33.92 _____ Segment Leq : 58.84 dBA Total Leg All Segments: 58.84 dBA TOTAL Leq FROM ALL SOURCES (DAY): 59.18 (NIGHT): 58.84

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:35:31 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r7b.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) -----Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld _ _ 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ : -90.00 deg 90.00 deg Angle1 Angle2 Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 169.00 / 169.00 m Receiver height:1.50 / 1.50 mTopography:2 (Flat : 2 (Flat/gentle slope; with barrier) : -82 deg Track 1 : -90.00 deg Angle2 : 72.00 deg : 2.50 m Whistle Angle Barrier angle1 Barrier height Barrier receiver distance : 37.00 / 37.00 m Source elevation : 81.60 m Barrier elevation : 81.40 m Reference angle Results segment # 1: KNG (day) _____ Barrier height for grazing incidence _____ Source ! Receiver ! Barrier ! Elevation of Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)

+		+	+-					
4.00 ! 0.50 !	1.50 1.50	! 2	2.49 ! 1.72 !		83.49 82.72			
LOCOMOTIVE (0	0.00 + 55.11 +	44.86) =	55.50	dba				
Angle1 Angle2	Alpha RefLe	q D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	
-90 72	0.44 76.4	9 -15.09	-1.29	0.00	0.00	-5.00	55.11	
72 90	0.58 76.4	9 -16.67 -	-14.96	0.00	0.00	0.00	44.86	
WHEEL (0.00 + Angle1 Angle2	46.54 + 36.5 Alpha RefLe	6) = 46.90 q D.Adj	6 dBA F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	
-90 72	0.54 69.5	6 -16.20	-1.45	0.00	0.00	-5.37	46.54	
72 90	0.66 69.5	6 -17.46 -	-15.54	0.00	0.00	0.00	36.56	
LEFT WHISTLE Angle1 Angle2	(0.00 + 30.23 2 Alpha RefLe	+ 0.00) = q D.Adj	= 30.23 F.Adj	3 dBA W.Adj	H.Adj	B.Adj	SubLeq	
-84 -82	0.44 73.8	9 -15.09 -	-23.56	0.00	0.00	-5.00	30.23	
RIGHT WHISTLE Anglel Angle2	2 (0.00 + 33.8 2 Alpha RefLe	2 + 0.00) q D.Adj	= 33.8 F.Adj	32 dBA W.Adj	H.Adj	B.Adj	SubLeq	
-82 -78	0.44 73.8	9 -15.09 -	-19.98	0.00	0.00	-5.00	33.82	
Segment Leq : 56.11 dBA Total Leq All Segments: 56.11 dBA								
Results segme	ent # 1: KNG (:	night)						
Barrier height for grazing incidence								
Source ! Height (m) !	Receiver Height (m)	! Barrier ! Height	! (m) !	Elevati Barrier	on of Top ((m)		
4.00 ! 0.50 !	1.50 1.50	! 2	2.49 ! 1.72 !		83.49 82.72			
LOCOMOTIVE (0 Angle1 Angle2	0.00 + 54.72 + 2 Alpha RefLe	44.47) = q D.Adj	55.11 F.Adj	dBA W.Adj	H.Adj	B.Adj	SubLeq	
-90 72	0.44 76.1	0 -15.09	-1.29	0.00	0.00	-5.00	54.72	
72 90	0.58 76.1	0 -16.67 -	-14.96	0.00	0.00	0.00	44.47	

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 434 of 465

WHEEL (0.00 + 46.59 + 36.60) = 47.00 dBAAnglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ - - - - - - -_____ -90 72 0.54 69.60 -16.20 -1.45 0.00 0.00 -5.37 46.59 _____ 72 90 0.66 69.60 -17.46 -15.54 0.00 0.00 0.00 36.60 _____ LEFT WHISTLE (0.00 + 28.05 + 0.00) = 28.05 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -84 -82 0.44 71.71 -15.09 -23.56 0.00 0.00 -5.00 28.05 _____ RIGHT WHISTLE (0.00 + 31.64 + 0.00) = 31.64 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -78 0.44 71.71 -15.09 -19.98 0.00 0.00 -5.00 31.64 -82 _____ Segment Leq : 55.76 dBA Total Leq All Segments: 55.76 dBA

(NIGHT): 55.76



TOTAL Leg FROM ALL SOURCES (DAY): 56.11



ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:39:47 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r8.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) _____ Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 169.00 / 169.00 m Receiver height:1.50 / 1.50 mTopography:1 1 (Flat/gentle slope; no barrier) -82 deg Track 1 : Whistle Angle : 0.00 Reference angle Results segment # 1: KNG (day) LOCOMOTIVE (0.00 + 58.49 + 0.00) = 58.49 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.58 76.49 -16.67 -1.33 0.00 0.00 0.00 58.49 _____ WHEEL (0.00 + 50.64 + 0.00) = 50.64 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.66 69.56 -17.46 -1.46 0.00 0.00 0.00 50.64

Edwardsburgh Developments Ltd. LOCKMASTERS MEADOW, CARDINAL: RAIL NOISE ASSESSMENT Page 436 of 465

_____ LEFT WHISTLE (0.00 + 32.28 + 0.00) = 32.28 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 0.58 73.89 -16.67 -24.93 0.00 0.00 0.00 32.28 -84 _____ RIGHT WHISTLE (0.00 + 36.10 + 0.00) = 36.10 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -82 -78 0.58 73.89 -16.67 -21.12 0.00 0.00 0.00 36.10 _____ Segment Leg : 59.18 dBA Total Leq All Segments: 59.18 dBA Results segment # 1: KNG (night) _____ LOCOMOTIVE (0.00 + 58.10 + 0.00) = 58.10 dBA Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.58 76.10 -16.67 -1.33 0.00 0.00 0.00 58.10 WHEEL (0.00 + 50.69 + 0.00) = 50.69 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _____ _ _ _ _ _ _ _____ -90 90 0.66 69.60 -17.46 -1.46 0.00 0.00 0.00 50.69 _____ LEFT WHISTLE (0.00 + 30.10 + 0.00) = 30.10 dBA Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg _____ -84 -82 0.58 71.71 -16.67 -24.93 0.00 0.00 0.00 30.10 _____ RIGHT WHISTLE (0.00 + 33.92 + 0.00) = 33.92 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq ------82 -78 0.58 71.71 -16.67 -21.12 0.00 0.00 0.00 33.92 _____ Segment Leq : 58.84 dBA Total Leg All Segments: 58.84 dBA TOTAL Leq FROM ALL SOURCES (DAY): 59.18 (NIGHT): 58.84

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 24-11-2023 12:40:42 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: r8b.te Time Period: Day/Night 16/8 hours Description: Rail data, segment # 1: KNG (day/night) -----Train ! Trains ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (Left) ! (Right) !(km/h) !/Train!/Train! type Type !weld _ _ 1. Freight ! 8.0/4.5 ! 8.0/4.5 ! 89.0 ! 4.0 !140.0 !Diesel! Yes * 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 89.0 ! 4.0 ! 25.0 !Diesel! Yes 3. Passenger ! 7.5/0.0 ! 7.5/0.0 ! 105.0 ! 2.0 ! 10.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters: Train type:! Unadj. Trains ! Annual % ! Years of !NoName! Left ! Right ! Increase ! Growth ! Train type: _____+ 2. W Freight ! 0.5/0.0 ! 0.5/0.0 ! 0.00 ! 0.00 ! Data for Segment # 1: KNG (day/night) _____ : -90.00 deg 90.00 deg Angle1 Angle2 Wood depth : 0 (No woods.) No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver source distance : 169.00 / 169.00 m Receiver height:1.50 / 1.50 mTopography:2 (Flat : 2 (Flat/gentle slope; with barrier) : -82 deg Track 1 : -90.00 deg Angle2 : 0.00 deg : 2.50 m Whistle Angle Barrier angle1 Barrier height Barrier receiver distance : 24.00 / 24.00 m Source elevation : 81.60 m Barrier elevation : 81.75 m Reference angle Results segment # 1: KNG (day) _____ Barrier height for grazing incidence _____ Source ! Receiver ! Barrier ! Elevation of Height (m) ! Height (m) ! Height (m) ! Barrier Top (m) A23

 4	4.00 !		1.50 !		+- 2.68 !		83.58		
LOCOMOTI Angle1 A	IVE (0. Angle2	.00 + 55 Alpha	5.48 + 5 RefLeq	55.48) = D.Adj	58.49 F.Adj	dBA W.Adj	H.Adj	B.Adj	SubLeq
 -90 -90	0 0	0.44 0.58	76.49 76.49	-15.09 -16.67	-4.06 -4.34	0.00 0.00	0.00	-4.97 0.00	52.37* 55.48
0	90	0.58	76.49	-16.67	-4.34	0.00	0.00	0.00	55.48
* Brigh	nt Zone	e !							
WHEEL ((Anglel <i>P</i>).00 + Angle2	44.02 - Alpha	+ 47.63 RefLeq) = 49.2 D.Adj	0 dBA F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	0	0.54	69.56	-16.20	-4.26	0.00	0.00	-5.08	44.02
0	90	0.66	69.56	-17.46	-4.47	0.00	0.00	0.00	47.63
LEFT WHI Anglel A	ISTLE	(0.00 + Alpha	32.28 - RefLeq	+ 0.00) D.Adj	= 32.28 F.Adj	3 dBA W.Adj	H.Adj	B.Adj	SubLeq
-84 -84	-82 -82	0.44 0.58	73.89 73.89	-15.09 -16.67	-23.56 -24.93	0.00 0.00	0.00 0.00	-4.99 0.00	30.23* 32.28
* Brigh	nt Zone	 e !							
RIGHT WH Anglel A	HISTLE Angle2	(0.00 - Alpha	⊦ 36.10 RefLeq	+ 0.00) D.Adj	= 36.1 F.Adj	LO dBA W.Adj	H.Adj	B.Adj	SubLeq
-82 -82	-78 -78	0.44 0.58	73.89 73.89	-15.09 -16.67	-19.98 -21.12	0.00 0.00	0.00 0.00	-4.99 0.00	33.83* 36.10
* Bright Zone ! Segment Leq : 59.01 dBA									
Total Le	eq All	Segment	:s: 59.0)1 dBA					
Results	segmer	nt # 1:	KNG (n:	ight)					
Barrier height for grazing incidence									
Source Height	! (m) !	Receive Height	er ! (m) !	Barrier Height	- (m) !	Elevati Barrier	on of Top	(m)	
	1.00 !		1.50 !		2.68 !		83.58		





ENGINEERS & SCIENTISTS

0 50 1	1 50 I	2 19 1	83 09
0.30 .	T .20 .	2.1/.	0.0.00

LOCOMO Angle1	FIVE (0 Angle2	.00 + 55 Alpha	5.09 + 5 RefLeq	55.09) = D.Adj	= 58.10 F.Adj	dBA W.Adj	H.Adj	B.Adj	SubLeq
-90 -90	0 0	0.44 0.58	76.10 76.10	-15.09 -16.67	-4.06 -4.34	0.00 0.00	0.00 0.00	-4.97 0.00	51.97* 55.09
0	90	0.58	76.10	-16.67	-4.34	0.00	0.00	0.00	55.09
* Brig	ght Zone	e !							
WHEEL Anglel	(0.00 + Angle2	44.07 - Alpha	+ 47.68 RefLeq) = 49.2 D.Adj	25 dBA F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	0	0.54	69.60	-16.20	-4.26	0.00	0.00	-5.08	44.07
0	90	0.66	69.60	-17.46	-4.47	0.00	0.00	0.00	47.68
LEFT WI Anglel	HISTLE Angle2	(0.00 + Alpha	30.10 - RefLeq	+ 0.00) D.Adj	= 30.10 F.Adj	dBA W.Adj	H.Adj	B.Adj	SubLeq
-84 -84	-82 -82	0.44 0.58	71.71 71.71	-15.09 -16.67	-23.56 -24.93	0.00	0.00 0.00	-4.99 0.00	28.06* 30.10
* Brig	ght Zone	e !							
RIGHT N Anglel	WHISTLE Angle2	(0.00 - Alpha	⊦ 33.92 RefLeq	+ 0.00) D.Adj	= 33.9 F.Adj	2 dBA W.Adj	H.Adj	B.Adj	SubLeq
-82 -82	-78 -78	0.44 0.58	71.71 71.71	-15.09 -16.67	-19.98 -21.12	0.00	0.00 0.00	-4.99 0.00	31.65* 33.92
* Brig	ght Zone	e !							
Segment Leq : 58.65 dBA									
Total 1	Total Leq All Segments: 58.65 dBA								

TOTAL Leq FROM ALL SOURCES (DAY): 59.01 (NIGHT): 58.65





APPENDIX C

BPN 56 WINDOW STC CALCULATIONS

127 WALGREEN ROAD, OTTAWA, ON, CANADA KOA 1LO [613 836 0934 GRADIENTWIND.COM Page 441 of 465

CALCULATIONS TO REDUCE INTERIOR RAIL TRAFFIC NOISE LOCKMASTER'S MEADOW - BEDROOM

	Ra	uil	
Outdoor Sound Level	=	60	
Source Geometry Correction:	=	0	
Correction For Surface Reflection:	=	3	
Target Indoor Noise Level:	=	35	
Required Noise Reduction:	=	28	

	Rail				
COMPONENT: Wall A - Spandral			STC Is:	45	
Noise Spectrum Type	F				
Component Category	d	Correction: (Table 5)	10		
Room Floor Area:	9 m ²			-10	dBA
Component Area:	2.43 m ²				
Component / Floor (%):	27 %				
Room Absorption Category:	Very Absorptive	Correction: (Table 4 Equation)	-7		dBA
				7	
Noise Reduction If Only This Compone	ent Transmits Sound Ene	ergy:		42	dBA
		Required Noise R	eduction:	28	dBA
Surplus noise reduction for comparison	to Table 3			14	
Component Transmits	4 % Of Sound				

COMPONENT: Surface A Window		Req	uired Noise Reduction Is:	28	dBA
Percentage Of Sound Energy Transmitted	1: 96	i %	Correction: (Table 3 Equation)	0	
Room Floor Area:	9	m²			
Component Area:	5.67	m²			
Component / Floor (%):	63	9/6			
Room Absortion Category:	Very Absorptive		Correction: (Table 4 Equation)	-3	dBA
Noise Spectrum	F				
Component Category	b		Correction: (Table 5)	3	dBA
			Required STC Is:	28	







SCHEDULE "N"

EASEMENTS AND LAND DEDICATIONS

LAND DEDICATIONS

The Owner shall ensure that the Municipality receives a valid conveyance, free of any encumbrances, of the following lands at the Owner's expense:

- 1. Block A: Open space and stormwater control facility
- 2. Block B: Sanitary pumping station
- 3. Block E: Right-of-way for future road (south)
- 4. Block F: Parkland Dedication
- 5. Block G: Right-of-way for future road (west)
- 6. Block H: 6m-wide walkway and passage for utilities and servicing

The Owner shall ensure that the United Counties of Leeds and Grenville receives a valid conveyance, free of any encumbrances, of the following lands at the Owner's expense:

- 1. Block C: 0.30m reserve on County Road
- 2. Blocks D and Da: 0.30m reserve on County Road
- 3. Road widening lands: Lands along the entire frontage of County Road 22 for future road purpose, sufficient to provide 13.1 m from the centreline of the Counties road.

EASEMENTS

In addition, the Owner shall ensure that the Municipality is granted 2.4m wide easements over all proposed swales; and 4.5m wide easement over all proposed ditches and culverts as shown in the Grading and Drainage Plans (GR-1 to GR-3 inclusive).

The Owner shall ensure deeds for lots 45 and 46 shall include a note that no changes in grading are allowed and that an easement is granted to the Municipality as shown in the Grading and Drainage Plan (GR-1 to GR-3 inclusive) to allow for maintenance.

The owner shall ensure that an easement for operational noise and vibration emissions is registered against any lots within 300m of the CN right of way.

The Owner shall ensure that the Municipality is granted easement(s) over that portion of County Rd 22 wherein the water and sewer works cross through the County Road allowance. The survey and easement shall be to the satisfaction of the Counties and the Municipality and shall be at the cost of the applicant.

SCHEDULE "O"

PARKLAND DEVELOPMENT SPECIFICATIONS

The Owner agrees that Block F, as shown on the Plan, shall be conveyed to the Municipality as part of Parkland Dedication.

No building permits will be issued for phase 2 until the following owner obligations associated with Block F have been completed to the satisfaction of the Township:

It is the responsibility of the Owner to fill with clean earth fill, compact and level Block F accordingly, providing for positive surface drainage to the satisfaction of the Municipality.

The Owner shall grade areas of parkland where necessary to the satisfaction of the Municipality, so as to provide a uniform surface, free of debris, necessary to establish a safe clean and maintainable surface.

Block F shall be graded in accordance with the approved Grading Plan for the Plan of Subdivision. No storage of building materials, including granular or topsoil will be permitted on Block F.

SCHEDULE "P"

ENGINEERING CONSULTANT(S)

The following Consultant(s) will be engaged by the Owner to provide the professional engineering services for the Subdivision on the lands described under Schedule "A":

Mongi Mabrouk P.Eng.

ADVANCE ENGINEERING LTD. 527-840 SPRINGLAND DR OTTAWA ON K1V 6L6

SCHEDULE "Q"

ADDITIONAL REQUIREMENTS OF THE UNITED COUNTIES OF LEEDS AND GRENVILLE

The Owner shall design and construct the intersection of all roads within the Plan of Subdivision that intersect the County Road to the satisfaction of the United Counties of Leeds and Grenville.

The Owner agrees to pay all expenses including those for drawing preparation, utility relocations, fees, security, road work, construction supervision, engineering and administrative costs for the modification of any intersection.

The Owner shall obtain an entrance permit and/or enter into an agreement with the United Counties of Leeds and Grenville, to the satisfaction of the United Counties of Leeds and Grenville respecting the conditions of accessing the Counties road/road allowance prior to undertaking any work within the Counties road allowance. Only one construction access shall be active at one time. If multiple accesses are to be active during construction, approval must be obtained by the road authority.

Prior to any site or earth work activity and during site work and construction on the lands or within the Counties road allowance (including but not limited to entrance construction, topsoil removal, tree removal, digging, site pre-grading, curb works, model home construction) the Owner shall:

- 1. Arrange an onsite (pre-construction) meeting with United Counties engineering staff with a minimum of 72 hours' notice for such meeting to review matters of Counties interests, including establishing the limits of required works
- 2. Arrange a video inspection of the United Counties road allowance with the United Counties staff in attendance in order to document the condition of the surface infrastructure before site works and construction. The Owner will immediately provide a copy of the preconstruction video survey to the United Counties
- Install and maintain, to the satisfaction of the Counties, mud mats and dust control suppressants on the subdivision lands to reduce the impact of mud tracking onto the Counties road network. Mud mats shall be according to the Counties specifications and what is shown on the Erosion and Sediment Control Plan
- 4. Immediately sweep and clean the County Road in the case of any dirt, mud, granular or other materials being deposited on the roadway to the satisfaction of the United Counties

SCHEDULE "R"

WORK SCHEDULE

The Works shall be constructed, installed or otherwise provided in general conformance with the work schedule set out in this Schedule. If the Work is not performed in accordance with the schedule for each portion of the Works to be constructed, installed or otherwise provided, the Owner shall be considered to have failed to proceed with reasonable speed, provided however that if any portion of the Work is delayed by an unavoidable delay, and such delay is reasonable, in the opinion of the Municipality, the completion date shall be extended by the period of such delay.

No work shall be commenced on any of the Works until the designs for all the Works and soil tests have been approved by the Municipality and the Municipality may stop any work that is commenced without its approval.

Any work undertaken by the Owner prior to this Agreement coming into force shall not be approved or Assumed by the Municipality as a municipal service until such time as the Owner's Professional Engineer has advised the Municipality, in writing, that such work has been carried out in accordance with the applicable specifications, and that all requirements for Assumption have been met to the Municipality's satisfaction and the Owner has paid the Municipality all costs in its review and processing of a request to approve, Accept or Assume such Works. The Owner shall provide all the information and expose or reconstruct any portion of the Works which the Municipality may in its sole and absolute discretion require. The Municipality is under no obligation to approve, Accept or Assume any portion of the Works undertaken by the Owner prior to this Agreement coming into force or unsatisfactory in the Municipality's sole and unfettered discretion, following this Agreement coming into force.

CONTRACTOR FOR CONSTRUCTION OF WORKS

The Owner covenants and agrees not to enter into any contract for the performance of any of the Works unless the contractor has first been approved by the Municipality, which approval shall not be unreasonably withheld. The contract(s) shall provide that the Municipality may inspect the construction of all Works and shall have authority to instruct the contractor(s) or subcontractor(s) to stop work should any construction be undertaken contrary to the provisions of this Agreement or the Municipality's design criteria, standards and specifications.

COMMENCEMENT OF CONSTRUCTION

The Owner covenants and agrees, prior to the construction of any Works, including the installation of public utilities, to give to the Municipality ten (10) days advance written notice of the date upon which construction of any Works is scheduled to commence.

[Include Schedule of Works]

Meadows subdivison

#	Activity Name	Remaining Duration	Start	Finish	Units
1	늘 Meadows subdivison	154	15-Jan-24	22-Aug-24	
2		46	15-Jan-24	19-Mar-24	
3	Rough site grading	25	13-Feb-24	19-Mar-24	
4		16	22-Jan-24	12-Feb-24	
5	Sit fence Install	5	15-Jan-24	19-Jan-24	
6		19	13-Feb-24	11-Mar-24	
7	Connect to existing watermain	2	08-Mar-24	11-Mar-24	1
8	Waterman Testing	3	05-Mar-24	07-Mar-24	
9	Waterservices	7	23-Feb-24	04-Mar-24	
10	250mm PVC DR 18 Watermain	2	23-Feb-24	26-Feb-24	
11	□ 150mm PVC DR 18 Watermain	10	23-Feb-24	07-Mar-24	
12	a 200 PVC PVC DR 18 Watermain	7	13-Feb-24	22-Feb-24	
13	🗧 Storm Sewer	34	22-Apr-24	07-Jun-24	
14	Storm Sewer - CCTV Inspection	2	06-Jun-24	07-Jun-24	,
15	200mm PVC DR35 Storm Sewer - CB Lead	5	30-May-24	05-Jun-24	
16	100mm PVC DR28 Storm Service (Subdivision)	7	24-May-24	03-Jun-24	
17	Rear yard catch basins	8	24-May-24	04-Jun-24	
18	StormCeptor EFO 12	3	21-May-24	23-May-24	
19	🚍 600mm x 600mm Catchbasin	7	21-May-24	29-May-24	
20	900mm Concrete Storm Sewer	2	16-May-24	17-May-24	
21	675mm Concrete Storm Sewer	5	09-May-24	15-May-24	
22	= 450mm Concrete Storm Sewer	3	09-May-24	13-May-24	
23	375mm PVC DR35 Storm Sewer	3	06-May-24	08-May-24	
24	300mm PVC DR35 Storm Sewer	1	06-May-24	06-May-24	
25	600mm Concrete Storm Sewer	5	02-May-24	08-May-24	
20		2	02-May-24	03-IVIay-24	
21	■ 525mm Concrete Storm Sewer	2	30-Api-24	01-May-24	
20	= 1200mm Storm MH	2	30-Api-24 22-Δpr-24	01-10/ay-24 29-Apr-24	
30	Sanitary source	32	08-Mar-24	23-Apr-24	
31			22 Apr 24	23 Apr 24	<u> </u>
32	Sanitary Sewer - CCTV Inspection	2	22-Api-24 17-Apr-21	20-Api-24 10-Apr-24	
33	125mm PV/C DR28 Sanitary Service (Subdivision)	7	08-Apr-24	16-Apr-24	
34	 1200mm Sanitary MH 	4	02-Apr-24	05-Apr-24	
35	200mm PVC DR35 Sanitary Sewer	16	08-Mar-24	01-Apr-24	
36	F Roads	39	10-Jun-24	02-Aug-24	
37	County road 22 reinstatement	4	30-Jul-24	02-Aug-24	
38	Place 40mm SP 12.5 B 58-34	3	30-Jul-24	01-Aug-24	
39	Place 40mm SP19 B 58-34	3	25-Jul-24	29-Jul-24	
40	🔲 3M Subdrain	4	11-Jul-24	16-Jul-24	
41	Concrete Curbs	5	11-Jul-24	17-Jul-24	
42	📼 Granular A	10	11-Jul-24	24-Jul-24	
43	🔲 Granular B placement	11	25-Jun-24	10-Jul-24	
44	Prep road subgrade	11	10-Jun-24	24-Jun-24	
45	🖕 Subcontract work	30	11-Jul-24	22-Aug-24	
46	Ence work	15	01-Aug-24	22-Aug-24	
47	Electrical subcontractor	25	11-Jul-24	15-Aug-24	
48	Concrete Elat work	15	11- luL24	31- lul-24	
40		16	11 Jul 24		
49		10		-01-Aug-24	
50		4	29-Jul-24	01-Aug-24	
52		2	25-JUI-24	20-JUE24	
52		2	20-JUI-24	∠4-JUF∠4 22 Jul 24	
- 33		Ø	II-JUF24	∠∠-JUF24	

SCHEDULE "S"

CERTIFICATE OF ASSUMPTION

[date]

THE CORPORATION OF THE TOWNSHIP OF EDWARDSBURGH/CARDINAL 18 Center Street, P.O. Box 129 Spencerville, ON K0E 1X0

- Attention: David Simpson Edwardsburgh Development Inc.
- Re: Certificate of Assumption PT LT 7 CON 1 Edwardsburgh; Edwardsburgh/Cardinal Lockmaster's Meadow Subdivision Subdivision Application No. [**no**]

This letter certifies that I, [name of Municipal Official], being the [title] and employed by the Corporation of the Township of Edwardsburgh/Cardinal ("the Municipality") have reviewed the terms of the Subdivision Agreement dated [date] and inspected the Works as defined therein.

I hereby verify and confirm that the Works appear to have been executed in accordance with the subdivision agreement including the schedules and approved plans attached thereto. Further, I am satisfied that all Municipal accounts have been paid and all maintenance requirements met.

Accordingly, I hereby recommend to council that it assume the said Works by way of resolution or assumption by-law such that ownership of the Works vest in the Municipality.

Yours truly,

[Name] [Title]



TOWNSHIP OF EDWARDSBURGH CARDINAL INFORMATION ITEM

Committee: Committee of the Whole - Community Development

Date: October 7, 2024

Department: Recreation

Topic: Summer Day Camp Year End Report

Background:

This year's summer camp was another success, with both the Cardinal and Johnstown locations hosting well-attended sessions. Each location offered four two-week sessions, providing a total of eight weeks of engaging activities for local children. In Johnstown, all four sessions had high numbers, accommodating 39 campers per session, for a total of 156 campers and 63 different families. Cardinal also saw strong participation, with 40 campers in sessions 1, 3, and 4 and 20 campers in session 2, bringing Cardinal's total to 120 campers and 49 different families.

Successes

Overall, this summer's camp was a great success. The themed sessions (Sports, Survivor, Arts and Crafts, and Everyday Hero) were well received by both campers and staff, featuring a variety of engaging games, activities, and creative projects. The Survivor theme during Session 2 was particularly popular, with campers enjoying daily team challenges that promoted teamwork and friendly competition.

Campers also benefited from swimming lessons, free swim sessions, and the Johnstown Junior Lifeguarding program at the Johnstown pool. Johnstown campers enjoyed using the new pickleball courts, new basketball net and baseball fields. Cardinal campers made excellent use of the arena, baseball field and basketball court throughout all eight weeks. Additionally, the Fire Department visited both camps in the final week to provide fire safety education. A standout moment was when the campers had the opportunity to be sprayed by the fire hose, which was a fun and memorable experience.

Camp Challenges

A notable challenge this summer was the camper demographic. At the Johnstown camp, the majority of participants were aged 5 to 7, making up 51.87% of the camp population. Children aged 8 to 10 comprised 38.13%, while those aged 11 to 12 made up just 10%. Similarly, at the Cardinal camp, the 5 to 7 age group was the largest, representing 54.28% of the campers. The 8 to 10 age group accounted for 40%, and the 11 to 12 age group represented only 5.72%.

Given this distribution, it is recommended to adjust the camp age range to focus on children aged 5 to 10. This change would better align with the demographics and allow for a more targeted and engaging camp experience. Resources could be reallocated to enhance programs for this core age group, ensuring the camp meets the needs and interests of the majority of participants.

Staff

Staff were hired in early spring to ensure all required training could be completed before summer began. Each team member underwent training in customer service excellence, allergy awareness, concussion awareness, and WHMIS. Staff also participated in two collaborative training sessions with the pool staff: one full-day and one evening session. The evening session included hands-on scenarios with the Fire Department to enhance preparedness.

Staff Successes: The Township employed 16 camp staff members this summer, including 10 full-time and 6 part-time. This staffing structure proved beneficial, providing flexibility to cover the more than half of our staff who required over 7 days off. The additional part-time staff also offered crucial support in managing campers with behavioral challenges, leading to smoother operations and better individual attention.

Staffing Challenges: Once the summer began, one challenge was that not all staff were able to commit to a full 40-hour workweek for the entire 8-week duration.

Leaders in Training

Leaders in Training (LITs) are volunteer students that were a valuable component of this year's summer camp. They played a key role during free swim sessions, helping to meet pool admission standards. LITs also assisted in leading camp activities for those who chose not to participate in free swim, ensuring a well-rounded and engaging experience for all campers.

Considerations for Summer 2025

Staffing: Continue hiring 16 camp staff, keeping in mind that not all staff will be available for a full 40-hour workweek.

Training: Provide additional training for managing children with behavioral challenges.

Equipment: Invest in more outdoor equipment.

Age Range: Adjust the camp age range to 5 to 10 or 11 years old to better align with the younger camper demographic.

ast

Recreation Coordinator

Facilities Manager



TOWNSHIP OF EDWARDSBURGH CARDINAL INFORMATION ITEM

Committee: Committee of the Whole - Community Development

Date: October 7, 2024

Department: Recreation

Topic: Aquatic Program Year End Report

Background:

The Township continues to deliver strong and engaging summer programming and experienced another successful summer of programming for 2024. This year's program attracted significant participation, reflecting the community's enthusiasm and the effectiveness of our offerings. The high attendance and participation rates are evident throughout the various activities, as outlined in this report.

The program included a wide range of activities catering to different age groups and interests. From swimming lessons, aquafit, swim team, Jr. Lifeguard program to lifeguarding courses and the public swim offerings. The commitment to programming was key to drawing families and ensuring that all community members could find appropriate times that suited their needs and preferences. Attendance across all programs was impressive, with many programs reaching or exceeding capacity. This high level of participation underscores the program's success and the community's desire for engaging summer activities.

Spring Courses

Course	Total	TWPEC Staff	Spring of 2023
	Participants for	Participants	
	2024	for 2024	
		-	
Safeguard	16	9	14
Standard First Aid and CPR-C	7	3	9

Aquatic	6	1	Not offered
Managers NEW			

Staff training and course offerings started in early spring; this is to ensure all courses can be taught. The Safeguard course, which is geared to Camp Counsellors and LIT's, focuses on supervision of campers while in the pool. This program was also marketed to any youth 12 years or older who may have a backyard pool or have an interest in working with kids who may be around water.

June Programming

The early opening of Johnstown Pool allowed the pool to extend its programming into the evenings, since the township was offering leadership programs to staff, the township was able to offer public swimming, aquafit and swimming lessons to the community.

June Lessons

June lessons were offered for the first time this year and ran simultaneously with the Lifeguarding courses. A total of 13 swimmers took advantage of this opportunity. This worked well with organization and teamwork of staff and zoning of the pool. This can only work if you have majority of college or university staff.

Johnstown Pool	June 10 th to 30th
Johnstown Weekend	The pool was opened for 4 weekends in June with an average of 19 swimmers using the pool. One of those days was the opening of the pool, which had 45 swimmers that day. If you removed that day the average was 15.7 swimmers per day.
Johnstown Evening Swim	The pool was open on June 10 th , and while lifeguarding courses were being taught public swimming was being offered and on average 10 swimmers participated per night.
Johnstown Aquafit (2 nights)	Offered 5 times in June with one night cancelled due to weather, and an average of 10 Aqua fitters.

June Johnstown Only

School

The extended availability also enabled the township to form a valuable partnership with South Edwardsburg Public School. Through this collaboration, students, excluding junior and senior kindergarten, received three swimming lessons focused on basic skills such as putting their faces in the water, kicking, and beginning strokes, along with essential water safety training. Jr/ Sr Kindergarten students received one lesson, and received some instructions in water safety as well as getting in and out of the pool, wearing PFD's, floats etc. Students also enjoyed free swim time, making the overall experience highly positive. Both the school and staff worked hard to meet all safety ratios, which ensured we had a minimum of 6 to 8 staff depending on the group or number. This initiative gave children who might not have accessed swimming lessons to gain these critical life skills. It is hoped that this partnership can continue, and the program offering can continue to grow as it has proven to be highly beneficial for both the school and the students. It is important to note that this partnership worked because we had college and university students to support the program.

Leadership Program

The township continues to build on providing leadership courses for our own employees and to local municipalities. As you can see by the township offering these courses to our own staff, the township is also helping other local municipalities with current staffing shortages. The new course the township offered this June was the Examiners course. The Examiners course is the first step to allowing Candidates to evaluate and certify candidates in the Life Saving Society's training programs. We had 5 employees attend this course; two staff have completed their apprenticeship and can examine the Bronze Courses.

It is worth noting that ALL spring and June Leadership courses are taught and examined by the Aquatics Director.

Course	Number of Participants 2024	Current Staff	Summer of 2023
Lifesaving Assistant Instructor NEW	2	2	Not offered
Lifesaving Society Swim Instructors	17	12	16
Lifesaving Society Instructors	9	3	7
Aquatic Supervisor Course	0	0	8

Examiners NEW	7	5	0

Bronze Program

Course	Number of Participants 2024	Current Staff	Summer of 2023
Bronze Star	1	0	2
Basic First Aid	0	0	2
Bronze Medallion	7	2	11
Emergency First Aid	6	1	9
Bronze Cross	7	4	6
Standard First Aid	13	8	7
National Lifeguarding Course	8	5	13
National Lifeguarding Recert	13	5	11

Aquatic Team

This year's aquatic team consisted of 23 different individuals working a variety of different hours to operate both pools with full programing this summer of approximately 60 hours per week.

Profile of The Aquatic Team

The community pools are operated by hard-working part-time team members with a variety of experiences and range of ages.

First Year Lifeguard/Instructors	7 (15 years of age)
First Year Lifeguard/Instructors	4 (16 and 17 years of age)
First Year Lifeguard/Instructors	1 (18 years of age)

Second Year Lifeguard/Instructor	4 (16 and 17 years of age)
Second Year Lifeguard/Instructor	1 (18 years of age or older)
Third Year Lifeguard/Instructor	4 (18 years of age or older)
Adults	2 Adults

This summer, we added two additional staff members this season compared to last year, though there were four fewer adult participants. Additionally, we have twelve new staff, with an increase of five new lifeguards/instructors and exceeding last summer's numbers.

We provided approximately 20 hours of in-service training to staff during June and July. These sessions were not only led by the Aquatic's Director and Recreation Director but were also conducted in partnership with Chief Moore and the fire department. The Deck Supervisors also assisted in suggesting and delivering parts of the in-service training. They also ensured that staff participated fully and met the established expectations by modelling.

Hours of Operations

Programming	Number of Staff	Rational
Adult Lane Swim (2	2 staff	
days a week at each		
pool)		
Morning Lessons	4 to7 staff, and deck	Keeping our ratio down to an
9.00am to 12.00pm	supervisor	average of 1:4 ratio throughout
0.00001110 12.000011		most of our classes.
1:00pm to 3:00pm	7 staff	To meet both the public swim ratios,
Public Swim		as well as the camp ratio
3:00pm to 4:30pm	Depending on the night it	
Public Swim	would be either 4 or 6 for	
	Cardinal or 4 or 3 for	
	Johnstown depending on	
	lessons	

4:30pm to 5:30pm Swim Team	3 staff needed	2 coaching and 1 guarding (Cardinal) 2 guards (Johnstown, as the team is coached by a SERA volunteer)
5:30pm to 7:00pm Lessons Two nights a week	6 staff in cardinal and 4 staff in Johnstown	We need to add a deck supervisor to evening lessons
6:00pm to 7:00pm Aquafit	3 Staff	1 Instructing and 2 guarding through rotation
7:00pm to 8:00pm Public Swim	2 Staff	2 guards going through rotation

This summer, the hours of operation at each pool were reduced by 6.5 hours. These adjustments did not impact the overall programming at either location, evening lessons and public swimming were still available. The changes were implemented as follows:

Friday night: Reduced by 2.5hours, from 8:00am to 5:30pm.

Saturday and Sunday: Reduced by 1 hour each day, with new hours of 12:00pm to 4:00pm instead of 12:00pm to 5:00pm.

Evening public swim: Reduced by 2 hours, with the elimination of the 7:00pm to 8:00pm swim time at each pool.

Success

- 12 new staff members were mentored and had the opportunity to build confidence and skills and were able to deliver a successful summer program for children and families.
- The township met its ratios of 25:1 for public swimming and the daycare policy for ratio set out by the Ontario Regulations. The ratio is 2:1 for children 5 years and under (this ratio cannot be combined with any other ratio) 4:1 when campers cannot pass the swim test and are ages 6 to 9, 8:1 when campers can pass the swim test. Campers over the age of 10 who cannot pass the swim team must be in a 4:1 ratio. Both pools used pool staff to help with these ratios.

Challenges

- Every Lifeguard/Instructor took 7 to 10 days off in some fashion whether it be consecutively or in request for evening and/or weekends off, which were at an all-time high (for either sports or family time)
- Many of our student staff members struggled with taking direction. Where this is their first job, some are still working to build conflict resolution skills. It takes some extra time and clear communication to supervise this team

Swimming Lessons

Basic swimming ability is a fundamental requirement in any meaningful attempt to eliminate drowning in Canada. There are 5 modules in the Lifesaving Society Swim for Life Program

- Parent & Tot for 3 to 5 years of age
- Preschool for children 3 to 5 years of age
- Swimmer for children 5 years or older
- Adult lessons for people over 16 years
- Fitness Swimmer for people of any age who want to improve their overall physical fitness.

This summer we ran four of these programs along with the Swim Patrol Program. Our lessons were run at both pools, with the options of day or evening lessons. Saturday lessons were only offered in Johnstown.

Table 1: Swim for Life Program and Swim Patrol								
	Overall Day Lessons 2023	Overall Day Lessons 2024	Evening Lessons 2023	Evening Lessons 2024	Saturday Lessons 2023	Saturday Lessons 2024	Total for 2024	Total for 2023
Cardinal	246	275	102	110	Not offered	Not Offered	385	348
Johnstown	225	242	63	50	16	20	312	304

From the table you can see an overall increase in our numbers this summer, this is mostly due to the day camp and the success of its programs. Evening lessons continue to be a success in Cardinal with the numbers increasing slightly.

Considerations for 2025 season

- Daily Morning lessons at both pools from 9:00am to 12:00pm
- Evening lessons to be taught ONLY at the Cardinal pool from 5:00pm to 7:00pm
- Saturday Lessons to be taught in Johnstown 10:00am to 12:00pm

The Township is excited to try these new changes for the 2025 swimming season. They will enable more effective programming and maximize the utilization of pool space. By implementing these adjustments, we can enhance the overall experience of participants and ensure a more efficient use of staff. These improvements will create a more engaging and well-organized swimming environment allowing everyone to benefit from more dynamic and enjoyable swimming lessons.

Deck Supervisor

As recommended by the Lifesaving Society, the Township implemented a full-time deck supervisor for all lesson blocks. The deck supervisor was responsible for ensuring lessons started and stopped on time, assisting parents when needed, supporting instructors (behaviors, injuries of swimmers, crying of swimmers). Deck supervisors are an integral part of a successful lesson block. Ensuring the lessons are taught within their zones and within the aquatic director's expectations are also important deck supervisor roles.

Pool Attendance

	2024 Total #	2023 Total #	2022 Total #	2021 Total #
	Of Swimmers	of Swimmers	of Swimmer	of Swimmer
Cardinal Pool Public Swim/Lane	3200	2673	2481	1859
Swim				
Cardinal Aquafit (2 nights)	270	247	84	

Johnstown Pool Public Swim/Lane	3140	2921	2935	2578
Swim				
Johnstown Aquafit (2 nights)	210	160	55	

Observations of the usage of the two Facilities

- It is important to note that the Cardinal facility had an overall increased use of the wading pool this summer by young families.
- Cardinal afternoon public swims were well attended from 2:30pm to 4:30pm
- Johnstown pool had an increase of public swimmers during the evening public swim times, as opposed to the smaller group during the day 2:00pm to 4:30pm
- It is also important to note that because the ball diamonds in Johnstown were busier this summer, attendance increased during our Saturday Public swim times, having to add an extra staff member.

Aquafit

The aquafit program was ran four times a week over a seven-week period. Each pool had 2 evenings from 6:00pm to 7:00pm. This time slot is well liked by participants. Despite being canceled, on average, once a week due to weather, the sessions saw an average attendance of 18 participants with numbers reaching up to 35 on some occasions. Participation was highly weather-dependent, with fluctuations in attendance largely influenced by the day's condition. The instructor continues to build positive relationships with participants.

Swim Team

Swim team ran out of both pools this summer. Johnstown Bear Paws saw a registration of about 35 swimmers where Cardinal Sea Sharks saw a registration of about 8 swimmers. Johnstown attended all swim meets this summer where Cardinal only attended their own and Johnstown's meet where 4 swimmers attended and competed in individual events only.

Johnstown Bear Paws practiced from 4:30pm to 5:25pm Monday to Friday with a volunteer coach. Cardinal Swimmers practiced Monday to Friday 12:00pm to 1:00pm. In Cardinal, July practices were well attended by 8 swimmers, however, in August participation was extremely limited.

It is my recommendation based on numbers the last two years in Cardinal, that staff reallocate this pool time in Cardinal to private lessons and a NEW program called "Make a splash for All-Sensory Friendly Swimming" This program would meet the needs of some of our most vulnerable children.

Johnstown would become the home of a recreational swim team for the summer.

Jr. Lifeguard Club

Jr. Lifeguard club ran out of the Johnstown pool only this summer. It ran 2 times a week on Monday and Wednesday. This program saw 11 kids register for it, and some of the older campers took advantage of it. This program was instructed by two of our senior staff, who reinforced basic lifeguarding skills and made it fun. It is the hope that these individuals will keep their interest and participate in the bronze courses and gain a passion for the sport.

Conclusion

The 2024 Summer Program was a success, marked by high participation, diverse offerings, and positive community feedback. The strong attendance figures across all activities reflect the program's effectiveness in meeting the needs and interests of our residents. Moving forward, we aim to build on this success, addressing any challenges and continuing to offer enriching and engaging programming for our community.

It is recommended that program offerings become the driving force behind what is potentially offered at each pool rather than trying to offer the same programing at each facility. With Staffing allocation, it is recommended that evening lessons be offered only at one pool being Cardinal, and Johnstown be left open for public /lane swim.

Two NEW opportunities for the 2025 summer

Making a Splash for All- Sensory Friendly Swimming

This program would be a valuable addition to our offerings, specifically designed for children with sensory sensitivities, autism, and other neurological differences, making water safety accessible and more enjoyable for all. We understand that some children find regular lessons very overwhelming due to the number of participants, splashing, general noise and activity on the deck. This program will help develop water safety skills and foster a love for swimming in a more supportive environment. Our staff will receive specialize training by the Aquatic Director and an experienced educator who works directly with children with sensory sensitivities.

Private Swimming lessons

This summer, private lesson requests were made by numerous families throughout the township. Feedback from parents indicates a strong preference for private lessons, as they can be customized to meet their child's specific learning needs. Several reasons have been identified for this increased demand: Some swimmers may be behind their peers and prefer not to be placed in lessons with younger children and other swimmers may have had negative experiences in group settings and require additional support to build confidence and skills.

To address this demand, we recommend making private lessons more widely available to interested families. This would target a new group of swimmers while expanding the options within our program. These lessons could be offered concurrently with current lessons using a one-to-one instructor-to-student ratio or scheduled during less busy times, depending on the needs of the participants. By implementing these changes, we can better accommodate diverse learning needs, enhance the overall experience, and attract more participants to our swimming program.

Finally, this summer was a summer for change, growth and learning for all. Our programs overall saw growth and as a staff we continued to educate and bring drowning prevention awareness to our community.

Additional Recommendations for the 2025 Aquatic Season

- Maintain working relationship with South Edwardsburgh Public School and continue providing a swim program for the month of June.
- Host a Jr. Lifeguard competition day.
- Continue our work with drowning prevention with a greater focus on Drowning Prevention week.

Wish list for supplies.

- Fins, of different sizes.
- Pool noodles





Recreation Coordinator

Facility Manager